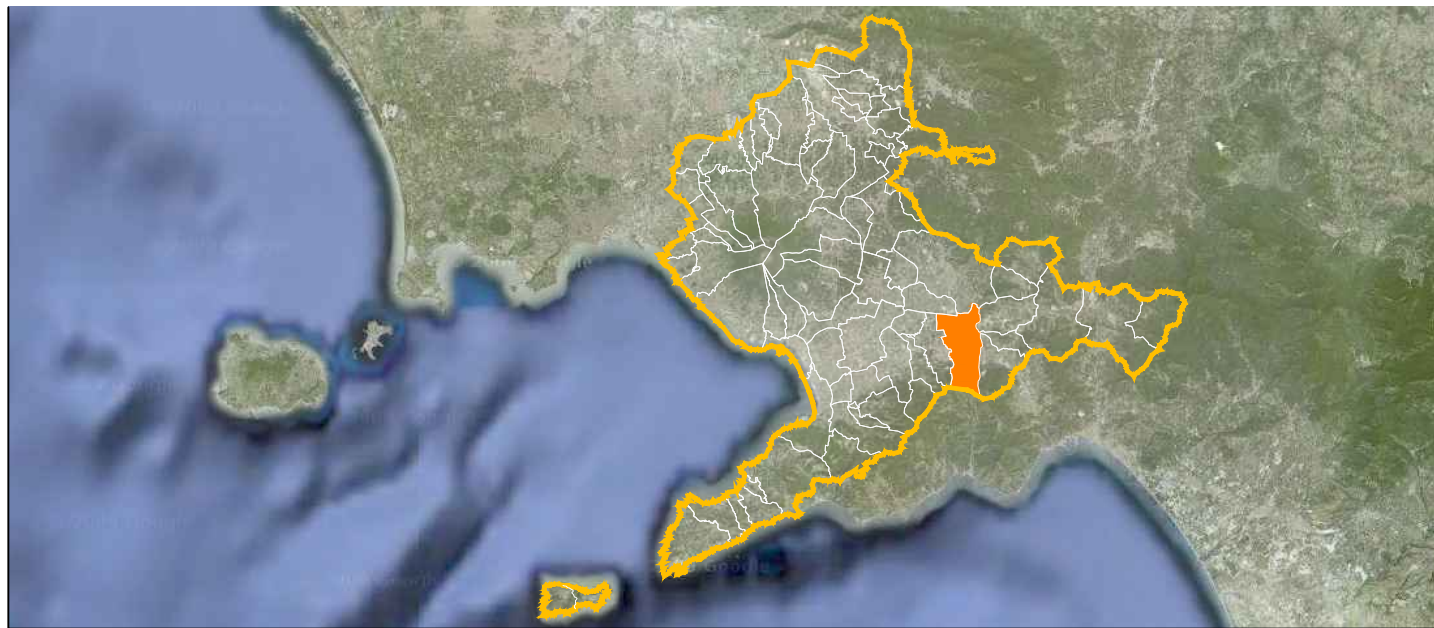




Ambito Distrettuale Sarnese Vesuviano
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PROTOCOLLO D'INTESA REGIONE CAMPANIA, COMUNE DI NOCERA INFERIORE,
ENTE D'AMBITO SARNESE-VESUVIANO, GORI SpA
PROT. N. 17853 DEL 19/04/2018



**COMUNE DI NOCERA INFERIORE
COMPLETAMENTO DELLA RETE FOGNARIA
1° LOTTO - STRALCIO A**



INT 7308

PROGETTO ESECUTIVO

INGEGNERIA

Il Responsabile
ing. Domenico Cesare

Elaborato:

G2.2

Titolo:

**SCARICATORE VIA PUCCI
Relazione di calcolo strutturale**

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//

COLLABORATORI

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ing. Fabio Iasevoli

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ing. Domenico Cesare

IL RUP



**REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA
NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO - STRALCIO A
CODICE INTERVENTO – INT 7308
SCARICATORE IN VIA PUCCI**



Relazione di Calcolo Strutturale

Il progettista strutturale

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RELAZIONE DI CALCOLO STRUTTURALE

PREMESSA

La presente relazione di calcolo strutturale, in conformità al §10.1 del DM 17/01/18, è comprensiva di una descrizione generale dell'opera e dei criteri generali di analisi e verifica. Segue inoltre le indicazioni fornite al §10.2 del DM stesso per quanto concerne analisi e verifiche svolte con l'ausilio di codici di calcolo. Il presente documento riassume i principali aspetti connessi alla progettazione strutturale delle opere a completamento della rete fognaria del comune di Nocera Inferiore.

In particolare le opere di seguito descritte sono atte alla realizzazione di una struttura scatolare in conglomerato cementizio armato per l'alloggiamento di un impianto di scarico delle acque reflue. La struttura sarà posta in via Pucci.

DESCRIZIONE GENERALE DELL'OPERA

Il presente documento riassume i principali aspetti connessi alla progettazione strutturale di un impianto scatolare atto a ospitare un impianto di scarico delle acque reflue. La struttura, interamente in c.c.a., ha forma rettangolare di dimensioni in pianta pari a circa 4.60x3.50m, affiancata con continuità strutturale a un altro corpo quadrato di dimensioni 1.50x1.50m.

La vasca è costituita da pareti di spessore di 20 cm; i due corpi sono posti a quote leggermente sfalsate, circa -3.35m e -3.00m. I gusci di fondazione sono di spessore 50cm. La scelta del loro piano di posa della fondazione è dettata esigenze di tipo idraulico, verificate con la resistenza meccanica dei primi strati di terreno e dalle caratteristiche di rigidità e resistenza della struttura. La piastra di copertura ha spessore 30cm.

I dati di progetto di riferimento, localizzazione e tipo di costruzione sono riportati nelle seguenti tabelle.

Parametri della struttura			
Classe d'uso	Vita V_n [anni]	Coeff. Uso	Periodo V_r [anni]
III	50.0	1.5	75.0

VALUTAZIONE DEL FATTORE DI STRUTTURA SECONDO IL D.M. 17/01/2018

Classe di duttilità media (CD"B").

Parametri fattore in direzione x e y

Sistema costruttivo: calcestruzzo

Tipologia strutturale: altre tipologie

Valore base fattore $q_0 = 1.500$

Fattore di regolarità $K_R = 1.0$

Fattore dissipativo $q_D = q_0 \cdot K_R = 1.500$

Fattori di comportamento utilizzati

Dissipativi

q SLU x: 1.500

q SLU y: 1.500

q SLU z: 1.500

Quadro normativo di riferimento adottato

Le norme ed i documenti assunti quale riferimento per la progettazione strutturale vengono indicati di seguito. Nel capitolo “normativa di riferimento” è comunque presente l’elenco completo delle normative disponibili.

Progetto-verifica degli elementi	
Progetto cemento armato	D.M. 17-01-2018
Progetto acciaio	D.M. 17-01-2018
Progetto legno	D.M. 17-01-2018
Progetto muratura	D.M. 17-01-2018
Azione sismica	
Norma applicata per l’azione sismica	D.M. 17-01-2018

Azioni di progetto sulla costruzione

Nei capitoli “modellazione delle azioni” e “schematizzazione dei casi di carico” sono indicate le azioni sulle costruzioni. Nel prosieguo si indicano tipo di analisi strutturale condotta (statico, dinamico, lineare o non lineare) e il metodo adottato per la risoluzione del problema strutturale nonché le metodologie seguite per la verifica o per il progetto-verifica delle sezioni. Si riportano le combinazioni di carico adottate e, nel caso di calcoli non lineari, i percorsi di carico seguiti; le configurazioni studiate per la struttura in esame *sono risultate effettivamente esaustive per la progettazione-verifica*. La verifica della sicurezza degli elementi strutturali avviene con i metodi della scienza delle costruzioni. L’analisi strutturale è condotta con il metodo degli spostamenti per la valutazione dello stato tensodeformativo indotto da carichi statici. L’analisi strutturale è condotta con il metodo dell’analisi modale e dello spettro di risposta in termini di accelerazione per la valutazione dello stato tensodeformativo indotto da carichi dinamici (tra cui quelli di tipo sismico). L’analisi strutturale viene effettuata con il metodo degli elementi finiti. Il metodo sopraindicato si basa sulla schematizzazione della struttura in elementi connessi solo in corrispondenza di un numero prefissato di punti denominati nodi. I nodi sono definiti dalle tre coordinate cartesiane in un sistema di riferimento globale. Le incognite del problema (nell’ambito del metodo degli spostamenti) sono le componenti di spostamento dei nodi riferite al sistema di riferimento globale (traslazioni secondo X, Y, Z, rotazioni attorno X, Y, Z). La soluzione del problema si ottiene con un sistema di equazioni algebriche lineari i cui termini noti sono costituiti dai carichi agenti sulla struttura opportunamente concentrati ai nodi:

$$\mathbf{K} \cdot \mathbf{u} = \mathbf{F} \quad \text{dove} \quad \mathbf{K} = \text{matrice di rigidezza}$$

$$\mathbf{u} = \text{vettore spostamenti nodali}$$

$$\mathbf{F} = \text{vettore forze nodali}$$

Dagli spostamenti ottenuti con la risoluzione del sistema vengono quindi dedotte le sollecitazioni e/o le tensioni di ogni elemento, riferite generalmente ad una terna locale all’elemento stesso.

Il sistema di riferimento utilizzato è costituito da una terna cartesiana destrorsa XYZ. Si assume l’asse Z verticale ed orientato verso l’alto.

Gli elementi utilizzati per la modellazione dello schema statico della struttura sono i seguenti:

Elemento tipo TRUSS	(biella-D2)
Elemento tipo BEAM	(trave-D2)
Elemento tipo MEMBRANE	(membrana-D3)
Elemento tipo PLATE	(piastra-guscio-D3)
Elemento tipo BOUNDARY	(molla)
Elemento tipo STIFFNESS	(matrice di rigidezza)
Elemento tipo BRICK	(elemento solido)
Elemento tipo SOLAIO	(macro elemento composto da più membrane)

Modello numerico

In questa parte viene descritto il modello numerico utilizzato (o i modelli numerici utilizzati) per l'analisi della struttura. La presentazione delle informazioni deve essere, coerentemente con le prescrizioni del paragrafo 10.2 e relativi sottoparagrafi delle NTC-18, tale da garantirne la leggibilità, la corretta interpretazione e la riproducibilità

Tipo di analisi strutturale	
Statica lineare	SI
Statica non lineare	NO
Sismica statica lineare	NO
Sismica dinamica lineare	SI
Sismica statica non lineare (prop. masse)	NO
Sismica statica non lineare (prop. modo)	NO
Sismica statica non lineare (triangolare)	NO
Non linearità geometriche (fattore P delta)	NO

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Informazioni sul codice di calcolo	
Titolo:	PRO_SAP PROfessional Structural Analysis Program
Versione:	PROFESSIONAL (build 2018-06-182)
Produttore-Distributore:	2S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara
Dati utente finale:	Ing. Iasevoli Fabio
Codice utente	Ing. Iasevoli Fabio
Codice Licenza:	Licenza dsi3773

Un attento esame preliminare della documentazione a corredo del software **ha consentito di valutarne l'affidabilità e soprattutto l'idoneità al caso specifico**. La documentazione, fornita dal produttore e distributore del software, contiene una esauriente descrizione delle basi teoriche e degli algoritmi impiegati, l'individuazione dei campi d'impiego, nonché casi prova interamente risolti e commentati, corredati dei file di input necessari a riprodurre l'elaborazione:

Affidabilità dei codici utilizzati

2S.I. ha verificato l'affidabilità e la robustezza del codice di calcolo attraverso un numero significativo di casi prova in cui i risultati dell'analisi numerica sono stati confrontati con soluzioni teoriche. E' possibile reperire la documentazione contenente alcuni dei più significativi casi trattati al seguente link:
<http://www.2si.it/Software/Affidabilità.htm>

Modellazione della geometria e proprietà meccaniche:

nodi	777
elementi D2 (per aste, travi, pilastri...)	0
elementi D3 (per pareti, platee, gusci...)	784
elementi solaio	0
elementi solidi	0

Dimensione del modello strutturale [cm]:

X min =	0.00
Xmax =	465.00
Ymin =	0.00
Ymax =	442.50
Zmin =	-305.00
Zmax =	-40.00

Strutture verticali:

Elementi di tipo asta	NO
Pilastri	NO
Pareti	SI
Setti (a comportamento membranale)	NO

Strutture non verticali:

Elementi di tipo asta	NO
Travi	NO
Gusci	SI
Membrane	NO

Orizzontamenti:

Solai con la proprietà piano rigido	NO
Solai senza la proprietà piano rigido	NO

Tipo di vincoli:

Nodi vincolati rigidamente	NO
Nodi vincolati elasticamente	NO
Nodi con isolatori sismici	NO
Fondazioni puntuali (plinti/plinti su palo)	NO
Fondazioni di tipo trave	NO
Fondazioni di tipo platea	SI
Fondazioni con elementi solidi	NO

Modellazione della geometria e proprietà meccaniche:

nodi	1166
elementi D2 (per aste, travi, pilastri...)	0
elementi D3 (per pareti, platee, gusci...)	1143
elementi solaio	0
elementi solidi	0

Dimensione del modello strutturale [cm]:

X min =	-0.00
---------	-------

Xmax =	500.00
Ymin =	0.00
Ymax =	310.00
Zmin =	-470.00
Zmax =	-50.00
Strutture verticali:	
Elementi di tipo asta	NO
Pilastrati	NO
Pareti	SI
Setti (a comportamento membranale)	NO
Strutture non verticali:	
Elementi di tipo asta	NO
Travi	NO
Gusci	SI
Membrane	NO
Orizzontamenti:	
Solai con la proprietà piano rigido	NO
Solai senza la proprietà piano rigido	NO
Tipo di vincoli:	
Nodi vincolati rigidamente	NO
Nodi vincolati elasticamente	NO
Nodi con isolatori sismici	NO
Fondazioni puntuali (plinti/plinti su palo)	NO
Fondazioni di tipo trave	NO
Fondazioni di tipo platea	SI
Fondazioni con elementi solidi	NO

Modellazione delle azioni

Si veda il capitolo “**Schematizzazione dei casi di carico**” per le informazioni necessarie alla comprensione ed alla ricostruzione delle azioni applicate al modello numerico, coerentemente con quanto indicato nella parte “2.6. Azioni di progetto sulla costruzione”.

Combinazioni e/o percorsi di carico

Si veda il capitolo “**Definizione delle combinazioni**” in cui sono indicate le combinazioni di carico adottate e, nel caso di calcoli non lineari, i percorsi di carico seguiti.

Combinazioni dei casi di carico	
APPROCCIO PROGETTUALE	Approccio 2
Tensioni ammissibili	NO
SLU	SI
SLV (SLU con sisma)	SI
SLC	NO
SLD	SI
SLO	NO
SLU GEO A2 (per approccio 1)	NO

SLU EQU	NO
Combinazione caratteristica (rara)	SI
Combinazione frequente	NO
Combinazione quasi permanente (SLE)	NO
SLA (accidentale quale incendio)	NO

Principali risultati

I risultati devono costituire una sintesi completa ed efficace, presentata in modo da riassumere il comportamento della struttura, per ogni tipo di analisi svolta.

2.8.1. Risultati dell'analisi modale

Viene riportato il tipo di analisi modale condotta, restituiti i risultati della stessa e valutate le informazioni desumibili in merito al comportamento della struttura.

2.8.2. Deformate e sollecitazioni per condizioni di carico

Vengono riportati i principali risultati atti a descrivere il comportamento della struttura, in termini di stati di sollecitazione e di deformazione generalizzata, distinti per condizione elementare di carico o per combinazioni omogenee delle stesse.

2.8.3. Involuppo delle sollecitazioni maggiormente significative. L'analisi e la restituzione degli involuppi (nelle combinazioni considerate agli SLU e agli SLE) delle caratteristiche di sollecitazione devono essere finalizzate alla valutazione dello stato di sollecitazione nei diversi elementi della struttura.

2.8.4. Reazioni vincolari

Vengono riportate le reazioni dei vincoli nelle singole condizioni di carico e/o nelle combinazioni considerate.

2.8.5. Altri risultati significativi

Nella presente parte vengono riportati tutti gli altri risultati che il progettista ritiene di interesse per la descrizione e la comprensione del/i modello/i e del comportamento della struttura.

La presente relazione, oltre ad illustrare in modo esaustivo i dati in ingresso ed i risultati delle analisi in forma tabellare, riporta una serie di immagini:

per i dati in ingresso:

- modello solido della struttura
- numerazione di nodi e ed elementi
- configurazioni di carico statiche
- configurazioni di carico sismiche con baricentri delle masse e eccentricità

per le combinazioni più significative (statisticamente più gravose per la struttura):

- configurazioni deformate
- diagrammi e involuppi delle azioni interne
- mappe delle tensioni
- reazioni vincolari
- mappe delle pressioni sul terreno

per il progetto-verifica degli elementi:

- diagrammi di armatura
- percentuali di sfruttamento
- mappe delle verifiche più significative per i vari stati limite

Informazioni generali sull'elaborazione e giudizio motivato di accettabilità dei risultati.

Il programma prevede una serie di controlli automatici (check) che consentono l'individuazione di errori di modellazione. Al termine dell'analisi un controllo automatico identifica la presenza di spostamenti o rotazioni abnormi. Si può pertanto asserire che l'elaborazione sia corretta e completa. I risultati delle elaborazioni sono stati sottoposti a controlli che ne comprovano l'attendibilità. Tale valutazione ha compreso il confronto con i risultati di semplici calcoli, eseguiti con metodi tradizionali e adottati, anche in fase di primo proporzionamento della struttura. Inoltre, sulla base di considerazioni riguardanti gli stati tensionali e deformativi determinati, si è valutata la validità delle scelte operate in sede di schematizzazione e di modellazione della struttura e delle azioni. Si allega al termine della presente relazione elenco sintetico dei controlli svolti (verifiche di equilibrio tra reazioni vincolari e carichi applicati, comparazioni tra i risultati delle analisi e quelli di valutazioni semplificate, etc.).

Verifiche agli stati limite ultimi

Nel capitolo relativo alla progettazione degli elementi strutturali agli SLU vengono indicate, con riferimento alla normativa adottata, le modalità ed i criteri seguiti per valutare la sicurezza della struttura nei confronti delle possibili situazioni di crisi ed i risultati delle valutazioni svolte. In via generale, oltre alle verifiche di resistenza e di spostamento, devono essere prese in considerazione verifiche nei confronti dei fenomeni di instabilità, locale e globale, di fatica, di duttilità, di degrado.

Verifiche agli stati limite di esercizio

Nel capitolo relativo alla progettazione degli elementi strutturali agli SLU vengono indicate, con riferimento alla normativa adottata, le modalità seguite per valutare l'affidabilità della struttura nei confronti delle possibili situazioni di perdita di funzionalità (per eccessive deformazioni, fessurazioni, vibrazioni, etc.) ed i risultati delle valutazioni svolte.

RELAZIONE SUI MATERIALI

Il capitolo Materiali riporta informazioni esaustive relative all'elenco dei materiali impiegati e loro modalità di posa in opera e ai valori di calcolo. Ulteriori informazioni sono riportate nella relazione generale nel capitolo inerente la caratterizzazione dei materiali impiegati.

NORMATIVA DI RIFERIMENTO

D.Min. Infrastrutture Min. Interni e Prot. Civile 17 Gennaio 2018 e allegate "Norme tecniche per le costruzioni".

D.Min.Infrastrutture Min. Interni e Prot. Civile 14 Gennaio 2008 e allegate "Norme tecniche per le costruzioni".

D.Min.Infrastrutture e trasporti 14 Settembre 2005 e allegate "Norme tecniche per le costruzioni".

D.M.LL.PP. 9 Gennaio 1996 "Norme tecniche per il calcolo, l'esecuzione ed il collaudo delle strutture in cemento armato, normale e precompresso e per le strutture metalliche".

D.M.LL.PP. 16 Gennaio 1996 "Norme tecniche relative ai <<Criteri generali per la verifica di sicurezza delle costruzioni e dei carichi e sovraccarichi>>".

D.M.LL.PP. 16 Gennaio 1996 "Norme tecniche per le costruzioni in zone sismiche".

Circolare 4/07/96, n.156AA.GG./STC. istruzioni per l'applicazione delle "Norme tecniche relative ai <<Criteri generali per la verifica di sicurezza delle costruzioni e dei carichi e sovraccarichi>>" di cui al D.M. 16/01/96.

Circolare 10/04/97, n.65AA.GG. istruzioni per l'applicazione delle "Norme tecniche per le costruzioni in zone sismiche" di cui al D.M. 16/01/96.

D.M. LL.PP. 20 Novembre 1987 "Norme tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento".

Circolare 4 Gennaio 1989 n. 30787 "Istruzioni in merito alle norme tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento".

D.M. LL.PP. 11 Marzo 1988 "Norme tecniche riguardanti le indagini sui terreni e sulle rocce, la stabilità dei pendii naturali e delle scarpate, i criteri generali e le prescrizioni per la progettazione, l'esecuzione e il collaudo delle opere di sostegno delle terre e delle opere di fondazione".

D.M. LL.PP. 3 Dicembre 1987 "Norme tecniche per la progettazione, esecuzione e collaudo delle costruzioni prefabbricate".

UNI 9502 -Procedimento analitico per valutare la resistenza al fuoco degli elementi costruttivi di conglomerato cementizio armato, normale e precompresso - edizione maggio 2001

Ordinanza del Presidente del Consiglio dei Ministri. 3274 del 20 marzo 2003 "Primi elementi in materia di criteri generali per la classificazione sismica del territorio nazionale e di normative tecniche per le costruzioni in zona sismica" e successive modificazioni e integrazioni.

UNI EN 1990:2006 13/04/2006 Eurocodice 0 - Criteri generali di progettazione strutturale.

UNI EN 1991-1-1:2004 01/08/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-1: Azioni in generale - Pesi per unità di volume, pesi propri e sovraccarichi per gli edifici.

UNI EN 1991-2:2005 01/03/2005 Eurocodice 1 - Azioni sulle strutture - Parte 2: Carichi da traffico sui ponti.

UNI EN 1991-1-3:2004 01/10/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-3: Azioni in generale - Carichi da neve.

UNI EN 1991-1-4:2005 01/07/2005 Eurocodice 1 - Azioni sulle strutture - Parte 1-4: Azioni in generale
- Azioni del vento.

UNI EN 1991-1-5:2004 01/10/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-5: Azioni in generale
- Azioni termiche.

UNI EN 1992-1-1:2005 24/11/2005 Eurocodice 2 - Progettazione delle strutture di calcestruzzo - Parte
1-1: Regole generali e regole per gli edifici.

UNI EN 1992-1-2:2005 01/04/2005 Eurocodice 2 - Progettazione delle strutture di calcestruzzo - Parte
1-2: Regole generali -Progettazione strutturale contro l'incendio.

UNI EN 1993-1-1:2005 01/08/2005 Eurocodice 3 - Progettazione delle strutture di acciaio - Parte 1-1:
Regole generali e regole per gli edifici.

UNI EN 1993-1-8:2005 01/08/2005 Eurocodice 3 - Progettazione delle strutture di acciaio - Parte 1-8:
Progettazione dei collegamenti.

UNI EN 1994-1-1:2005 01/03/2005 Eurocodice 4 - Progettazione delle strutture composte acciaio-
calcestruzzo - Parte 1-1:Regole generali e regole per gli edifici.

UNI EN 1994-2:2006 12/01/2006 Eurocodice 4 - Progettazione delle strutture composte acciaio-
calcestruzzo - Parte 2: Regole generali e regole per i ponti.

UNI EN 1995-1-1:2005 01/02/2005 Eurocodice 5 - Progettazione delle strutture di legno - Parte 1-1:
Regole generali – Regole comuni e regole per gli edifici.

UNI EN 1995-2:2005 01/01/2005 Eurocodice 5 - Progettazione delle strutture di legno - Parte 2: Ponti.

UNI EN 1996-1-1:2006 26/01/2006 Eurocodice 6 - Progettazione delle strutture di muratura - Parte 1-
1: Regole generali per strutture di muratura armata e non armata.

UNI EN 1996-3:2006 09/03/2006 Eurocodice 6 - Progettazione delle strutture di muratura - Parte 3:
Metodi di calcolo semplificato per strutture di muratura non armata.

UNI EN 1997-1:2005 01/02/2005 Eurocodice 7 - Progettazione geotecnica - Parte 1: Regole generali.

UNI EN 1998-1:2005 01/03/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica
- Parte 1: Regole generali, azioni sismiche e regole per gli edifici.

UNI EN 1998-3:2005 01/08/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica
- Parte 3: Valutazione e adeguamento degli edifici.

UNI EN 1998-5:2005 01/01/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica
- Parte 5: Fondazioni, strutture di contenimento ed aspetti geotecnici.

CIRCOLARE esplicativa n. 7 del 19 gennaio 2019.

CARATTERISTICHE MATERIALI UTILIZZATI

LEGENDA TABELLA DATI MATERIALI

Il programma consente l'uso di materiali diversi. Sono previsti i seguenti tipi di materiale:

1	materiale tipo cemento armato
2	materiale tipo acciaio
3	materiale tipo muratura
4	materiale tipo legno
5	materiale tipo generico

I materiali utilizzati nella modellazione sono individuati da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni materiale vengono riportati in tabella i seguenti dati:

Young	modulo di elasticità normale
Poisson	coefficiente di contrazione trasversale
G	modulo di elasticità tangenziale
Gamma	peso specifico
Alfa	coefficiente di dilatazione termica

I dati soprariportati vengono utilizzati per la modellazione dello schema statico e per la determinazione dei carichi inerziali e termici. In relazione al tipo di materiale vengono riportati inoltre:

1	cemento armato	Rck	resistenza caratteristica cubica
		Fctm	resistenza media a trazione semplice
2	acciaio	Ft	tensione di rottura a trazione
		Fy	tensione di snervamento
		Fd	resistenza di calcolo
		Fdt	resistenza di calcolo per spess. t>40 mm
		Sadm	tensione ammissibile
		Sadmt	tensione ammissibile per spess. t>40 mm

Vengono inoltre riportate le tabelle contenenti il riassunto delle Informazioni assegnate nei criteri di progetto in uso.

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Maggio 2011, disponibile per il download sul sito **www.2si.it**, si segnalano i seguenti esempi applicativi:

Modellazione di strutture in c.a.

Test N°	Titolo
41	GERARCHIA DELLE RESISTENZE PER TRAVI IN C.A.
42	GERARCHIA DELLE RESISTENZE PER PILASTRI IN C.A.
43	VERIFICA ALLE TA DI STRUTTURE IN C.A.
44	VERIFICA AGLI SLU DI STRUTTURE IN C.A.
45	VERIFICA A PUNZONAMENTO ALLO SLU DI PIASTRE IN C.A.
46	VERIFICA A PUNZONAMENTO ALLO SLU DI TRAVI IN C.A.
47	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 9/1/96

48	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 14/1/2008
49	VERIFICA ALLO SLE (TENSIONI E FESSURAZIONE) DI STRUTTURE IN C.A.
50	VERIFICA ALLO SLE (DEFORMAZIONE) DI STRUTTURE IN C.A.
51	FATTORE DI STRUTTURA
52	SOVRARESISTENZE
53	DETTAGLI COSTRUTTIVI C.A.: LIMITI D'ARMATURA PILASTRI E NODI TRAVE-PILASTRO
54	PARETI IN C.A. SNELLE IN ZONA SISMICA
80	ANALISI PUSHOVER DI UN EDIFICIO IN C.A.
120	PROGETTO E VERIFICA DI TRAVI PREM

Id	Tipo / Note	V. caratt.	V. medio	Young	Poisson	G	Gamma	Alfa	Altri
		daN/cm2	daN/cm2	daN/cm2		daN/cm2	daN/cm3		
3	Calcestruzzo Classe C28/35			3.260e+05	0.20	1.358e+05	2.50e-03	1.00e-05	
	Resistenza Rc	350.0							
	Resistenza fctm		28.4						
	Coefficiente ksb								0.85
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05

Pareti c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Progetto armatura	Parete sismica	Singolo elemento FONDAZIONE	Singolo elemento	Parete sismica		
Armatura						
Inclinazione Av [gradi]	90.00	90.00	90.00	90.00		
Angolo Av-Ao [gradi]	90.00	90.00	90.00	90.00		
Minima tesa	0.25	0.25	0.25	0.25		
Massima tesa	4.00	4.00	4.00	4.00		
Maglia unica centrale	No	No	No	No		
Unico strato verticale	No	No	No	No		
Unico strato orizzontale	No	No	No	No		
Copriferro [cm]	5.00	3.00	2.50	2.50		
Maglia V						
diametro	14	12	16	16		
passo	20	25	15	15		
diametro aggiuntivi	14	12	16	16		
Maglia O						
diametro	14	8	16	16		
passo	30	25	15	15		
diametro aggiuntivi	14	8	16	16		
Stati limite ultimi						
Tensione fy [daN/cm2]	4500.00	4500.00	4500.00	4500.00		
Tipo acciaio	tipo C	tipo C	tipo C	tipo C		
Coefficiente gamma s	1.15	1.15	1.15	1.15		
Coefficiente gamma c	1.50	1.50	1.50	1.50		
Fattore di confidenza FC	0.0	0.0	0.0	0.0		
Verifiche con N costante	Si	Si	Si	Si		
Tensioni ammissibili						
Tensione amm. cls [daN/cm2]	97.50	97.50	97.50	97.50		
Tensione amm. acciaio [daN/cm2]	2600.00	2600.00	2600.00	2600.00		
Rapporto omogeneizzazione N	15.00	15.00	15.00	15.00		
Massimo rapporto area compressa/tesa	1.00	1.00	1.00	1.00		
Parete estesa debolmente armata						
Fattore amplificazione taglio V	0.0	1.50	0.0	0.0		
Hcrit. par. 7.4.4.5.1 [cm]	250.00	0.0	0.0	250.00		
Hcrit. par. 7.4.6.1.4 [cm]	0.0	0.0	0.0	0.0		
Diagramma inviluppo taglio	Si	No	No	Si		
Vincolo lati	nessun lato	nessun lato	nessun lato	nessun lato		
Verifica come fascia	No	No	No	No		
Diametro di estremità	0	0	0	0		
Zona confinata						
Minima tesa	1.00	1.00	1.00	1.00		
Massima tesa	4.00	4.00	4.00	4.00		
Distanza barre [cm]	2.00	2.00	2.00	2.00		
Interferro	2	2	2	2		
Armatura inclinata						
Area barre [cm2]	0.0	0.0	0.0	0.0		
Angolo orizzontale [gradi]	0.0	0.0	0.0	0.0		
Distanza di base [cm]	0.0	0.0	0.0	0.0		
Resistenza al fuoco						

Pareti c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
3- intradosso	No	No	No	No		
3+ estradosso	No	No	No	No		
Tempo di esposizione R	15	15	15	15		

Gusci c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Armatura						
Inclinazione Ax [gradi]	0.0	0.0	0.0	0.0		
Angolo Ax-Ay [gradi]	90.00	90.00	90.00	90.00		
Minima tesa	0.10	0.10	0.31	0.10		
Massima tesa	0.78	0.78	0.78	0.78		
Maglia unica centrale	No	No	No	No		
Copriferro [cm]	5.00	3.00	2.00	5.00		
Maglia x						
diametro	14	16	16	16		
passo	20	20	20	20		
diametro aggiuntivi	14	16	16	16		
Maglia y						
diametro	14	16	16	16		
passo	20	20	20	20		
diametro aggiuntivi	14	16	16	16		
Stati limite ultimi						
Tensione fy [daN/cm2]	4500.00	4500.00	4500.00	4500.00		
Tipo acciaio	tipo C	tipo C	tipo C	tipo C		
Coefficiente gamma s	1.15	1.15	1.15	1.15		
Coefficiente gamma c	1.50	1.50	1.50	1.50		
Fattore di confidenza FC	0.0	0.0	0.0	0.0		
Verifiche con N costante	Si	Si	Si	Si		
Applica SLU da DIN	No	No	No	No		
Tensioni ammissibili						
Tensione amm. cls [daN/cm2]	97.50	97.50	97.50	97.50		
Tensione amm. acciaio [daN/cm2]	2600.00	2600.00	2600.00	2600.00		
Rapporto omogeneizzazione N	15.00	15.00	15.00	15.00		
Massimo rapporto area compressa/tesa	1.00	1.00	1.00	1.00		
Resistenza al fuoco						
3- intradosso	No	No	No	No		
3+ estradosso	No	No	No	No		
Tempo di esposizione R	15	15	15	15		

MODELLAZIONE DELLE SEZIONI

LEGENDA TABELLA DATI SEZIONI

Il programma consente l'uso di sezioni diverse. Sono previsti i seguenti tipi di sezione:

1. sezione di tipo generico
2. profilati semplici
3. profilati accoppiati e speciali

Le sezioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni sezione vengono riportati in tabella i seguenti dati:

Area	area della sezione
A V2	area della sezione/fattore di taglio (per il taglio in direzione 2)
A V3	area della sezione/fattore di taglio (per il taglio in direzione 3)
Jt	fattore torsionale di rigidezza
J2-2	momento d'inerzia della sezione riferito all'asse 2
J3-3	momento d'inerzia della sezione riferito all'asse 3
W2-2	modulo di resistenza della sezione riferito all'asse 2
W3-3	modulo di resistenza della sezione riferito all'asse 3
Wp2-2	modulo di resistenza plastico della sezione riferito all'asse 2
Wp3-3	modulo di resistenza plastico della sezione riferito all'asse 3

I dati sopra riportati vengono utilizzati per la determinazione dei carichi inerziali e per la definizione delle rigidezze degli elementi strutturali; qualora il valore di Area V2 (e/o Area V3) sia nullo la deformabilità

per taglio V2 (e/o V3) è trascurata. La valutazione delle caratteristiche inerziali delle sezioni è condotta nel riferimento 2-3 dell'elemento.

rettangolare	a T	a T rovescia	a T di colmo	a L	a L specchiata
a L specchiata rovescia	a L rovescia	a L di colmo	a doppio T	a quattro specchiata	a quattro
a U	a C	a croce	circolare	rettangolare cava	circolare cava

Per quanto concerne i profilati semplici ed accoppiati l'asse 2 del riferimento coincide con l'asse x riportato nei più diffusi profilati.

Per quanto concerne le sezioni di tipo generico (tipo 1.):

i valori dimensionali con prefisso B sono riferiti all'asse 2

i valori dimensionali con prefisso H sono riferiti all'asse 3

Con riferimento al Documento di Affidabilità "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Settembre 2014, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
1	CARATTERISTICHE GEOMETRICHE E INERZIALI
45	VERIFICA AGLI SLU DI STRUTTURE IN C.A.
48	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 9/1/96
49	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 14/1/2008
50	VERIFICA ALLO SLE (TENSIONI E FESSURAZIONE) DI STRUTTURE IN C.A.
51	VERIFICA ALLO SLE (DEFORMAZIONE) DI STRUTTURE IN C.A.
104	ANALISI DI RESISTENZA AL FUOCO

MODELLAZIONE STRUTTURA: NODI

LEGENDA TABELLA DATI NODI

Il programma utilizza per la modellazione nodi strutturali.

Ogni nodo è individuato dalle coordinate cartesiane nel sistema di riferimento globale (X Y Z).

Ad ogni nodo è eventualmente associato un codice di vincolamento rigido, un codice di fondazione speciale, ed un set di sei molle (tre per le traslazioni, tre per le rotazioni). Le tabelle sottoriportate riflettono le succitate possibilità. In particolare per ogni nodo viene indicato in tabella:

Nodo	numero del nodo.
X	valore della coordinata X
Y	valore della coordinata Y
Z	valore della coordinata Z

Per i nodi ai quali sia associato un codice di vincolamento rigido, un codice di fondazione speciale o un set di molle viene indicato in tabella:

Nodo	numero del nodo.
X	valore della coordinata X
Y	valore della coordinata Y
Z	valore della coordinata Z
Note	eventuale codice di vincolo (es. v=110010 sei valori relativi ai sei gradi di libertà previsti per il nodo TxTyTzRxRyRz, il valore 1 indica che lo spostamento o rotazione relativo è impedito, il valore 0 indica che lo spostamento o rotazione relativo è libero).
Note	(FS = 1, 2,...) eventuale codice del tipo di fondazione speciale (1, 2,... fanno riferimento alle tipologie: plinto, palo, plinto su pali,...) che è collegato al nodo. (ISO = "id SIGLA") indice e sigla identificativa dell' eventuale isolatore sismico assegnato al nodo
Rig. TX	valore della rigidezza dei vincoli elastici eventualmente applicati al nodo, nello specifico TX (idem per TY, TZ, RX, RY, RZ).

Per strutture sismicamente isolate viene inoltre inserita la tabella delle caratteristiche per gli isolatori utilizzati; le caratteristiche sono indicate in conformità al cap. 7.10 del D.M. 17/01/18

TABELLA DATI NODI

Nodo	X	Y	Z	Nodo	X	Y	Z	Nodo	X	Y	Z
	cm	cm	cm		cm	cm	cm		cm	cm	cm
1	280.0	325.0	-305.0	2	292.5	325.0	-305.0	3	306.7	325.0	-305.0
4	346.3	325.0	-305.0	5	372.5	325.0	-305.0	6	385.8	325.0	-305.0
7	410.0	325.0	-305.0	8	280.0	337.5	-305.0	9	292.5	337.5	-305.0
10	308.1	337.5	-305.0	11	349.0	337.5	-305.0	12	369.0	337.5	-305.0
13	375.7	337.5	-305.0	14	385.8	337.5	-305.0	15	410.0	337.5	-305.0
16	280.0	377.5	-305.0	17	292.5	377.5	-305.0	18	312.6	377.5	-305.0
19	358.0	377.5	-305.0	20	385.8	377.5	-305.0	21	410.0	377.5	-305.0
22	280.0	417.5	-305.0	23	292.5	417.5	-305.0	24	317.2	417.5	-305.0
25	366.9	417.5	-305.0	26	385.8	417.5	-305.0	27	410.0	417.5	-305.0
28	280.0	442.5	-305.0	29	292.5	442.5	-305.0	30	320.0	442.5	-305.0
31	372.5	442.5	-305.0	32	385.8	442.5	-305.0	33	410.0	442.5	-305.0
34	0.0	0.0	-270.0	35	37.9	0.0	-270.0	36	75.8	0.0	-270.0
37	113.8	0.0	-270.0	38	151.7	0.0	-270.0	39	189.6	0.0	-270.0
40	227.5	0.0	-270.0	41	267.1	0.0	-270.0	42	292.5	0.0	-270.0
43	306.7	0.0	-270.0	44	346.3	0.0	-270.0	45	372.5	0.0	-270.0
46	385.8	0.0	-270.0	47	410.0	0.0	-270.0	48	425.4	0.0	-270.0
49	465.0	0.0	-270.0	50	0.0	33.8	-270.0	51	37.9	33.8	-270.0
52	75.8	33.8	-270.0	53	113.8	33.8	-270.0	54	151.7	33.8	-270.0
55	189.6	33.8	-270.0	56	227.5	33.8	-270.0	57	267.1	33.8	-270.0
58	292.5	33.8	-270.0	59	306.7	33.8	-270.0	60	346.3	33.8	-270.0
61	372.5	33.8	-270.0	62	385.8	33.8	-270.0	63	410.0	33.8	-270.0
64	425.4	33.8	-270.0	65	465.0	33.8	-270.0	66	0.0	67.5	-270.0
67	37.9	67.5	-270.0	68	75.8	67.5	-270.0	69	113.8	67.5	-270.0
70	151.7	67.5	-270.0	71	189.6	67.5	-270.0	72	227.5	67.5	-270.0
73	267.1	67.5	-270.0	74	292.5	67.5	-270.0	75	306.7	67.5	-270.0
76	346.3	67.5	-270.0	77	372.5	67.5	-270.0	78	385.8	67.5	-270.0
79	410.0	67.5	-270.0	80	425.4	67.5	-270.0	81	465.0	67.5	-270.0
82	0.0	108.8	-270.0	83	37.9	108.8	-270.0	84	75.8	108.8	-270.0
85	113.8	108.8	-270.0	86	151.7	108.8	-270.0	87	189.6	108.8	-270.0
88	227.5	108.8	-270.0	89	267.1	108.8	-270.0	90	292.5	108.8	-270.0
91	306.7	108.8	-270.0	92	346.3	108.8	-270.0	93	372.5	108.8	-270.0
94	385.8	108.8	-270.0	95	410.0	108.7	-270.0	96	425.4	108.8	-270.0
97	465.0	108.8	-270.0	98	0.0	150.0	-270.0	99	37.9	150.0	-270.0
100	75.8	150.0	-270.0	101	113.8	150.0	-270.0	102	151.7	150.0	-270.0
103	189.6	150.0	-270.0	104	227.5	150.0	-270.0	105	267.1	150.0	-270.0
106	292.5	150.0	-270.0	107	306.7	150.0	-270.0	108	346.3	150.0	-270.0
109	372.5	150.0	-270.0	110	385.8	150.0	-270.0	111	410.0	150.0	-270.0
112	425.4	150.0	-270.0	113	465.0	150.0	-270.0	114	0.0	191.3	-270.0
115	37.9	191.3	-270.0	116	75.8	191.3	-270.0	117	113.8	191.3	-270.0
118	151.7	191.3	-270.0	119	189.6	191.3	-270.0	120	227.5	191.3	-270.0
121	267.1	191.3	-270.0	122	292.5	191.3	-270.0	123	306.7	191.3	-270.0
124	346.3	191.3	-270.0	125	372.5	191.3	-270.0	126	385.8	191.3	-270.0
127	410.0	191.3	-270.0	128	425.4	191.3	-270.0	129	465.0	191.3	-270.0

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

130	0.0	232.5	-270.0	131	37.9	232.5	-270.0	132	75.8	232.5	-270.0
133	113.8	232.5	-270.0	134	151.7	232.5	-270.0	135	189.6	232.5	-270.0
136	227.5	232.5	-270.0	137	267.1	232.5	-270.0	138	292.5	232.5	-270.0
139	306.7	232.5	-270.0	140	346.3	232.5	-270.0	141	372.5	232.5	-270.0
142	385.8	232.5	-270.0	143	410.0	232.5	-270.0	144	425.4	232.5	-270.0
145	465.0	232.5	-270.0	146	0.0	257.5	-270.0	147	37.9	257.5	-270.0
148	75.8	257.5	-270.0	149	113.8	257.5	-270.0	150	151.7	257.5	-270.0
151	189.6	257.5	-270.0	152	227.5	257.5	-270.0	153	267.1	257.5	-270.0
154	292.5	257.5	-270.0	155	306.7	257.5	-270.0	156	346.3	257.5	-270.0
157	372.5	257.5	-270.0	158	385.8	257.5	-270.0	159	410.0	257.5	-270.0
160	425.4	257.5	-270.0	161	465.0	257.5	-270.0	162	0.0	285.0	-270.0
163	37.9	285.0	-270.0	164	75.8	285.0	-270.0	165	113.8	285.0	-270.0
166	151.7	285.0	-270.0	167	189.6	285.0	-270.0	168	227.5	285.0	-270.0
169	267.1	285.0	-270.0	170	292.5	285.0	-270.0	171	306.7	285.0	-270.0
172	346.3	285.0	-270.0	173	372.5	285.0	-270.0	174	385.8	285.0	-270.0
175	410.0	285.0	-270.0	176	425.4	285.0	-270.0	177	465.0	285.0	-270.0
178	0.0	312.5	-270.0	179	37.9	312.5	-270.0	180	75.8	312.5	-270.0
181	113.8	312.5	-270.0	182	151.7	312.5	-270.0	183	189.6	312.5	-270.0
184	227.5	312.5	-270.0	185	267.1	312.5	-270.0	186	292.5	312.5	-270.0
187	306.7	312.5	-270.0	188	346.3	312.5	-270.0	189	372.5	312.5	-270.0
190	385.8	312.5	-270.0	191	410.0	312.5	-270.0	192	425.4	312.5	-270.0
193	465.0	312.5	-270.0	194	0.0	325.0	-270.0	195	37.9	325.0	-270.0
196	75.8	325.0	-270.0	197	113.8	325.0	-270.0	198	151.7	325.0	-270.0
199	189.6	325.0	-270.0	200	227.5	325.0	-270.0	201	280.0	325.0	-270.0
202	292.5	325.0	-270.0	203	306.7	325.0	-270.0	204	346.3	325.0	-270.0
205	372.5	325.0	-270.0	206	385.8	325.0	-270.0	207	410.0	325.0	-270.0
208	425.4	325.0	-270.0	209	465.0	325.0	-270.0	210	280.0	337.5	-270.0
211	410.0	337.5	-270.0	212	280.0	377.5	-270.0	213	410.0	377.5	-270.0
214	280.0	417.5	-270.0	215	410.0	417.5	-270.0	216	280.0	442.5	-270.0
217	292.5	442.5	-270.0	218	320.0	442.5	-270.0	219	372.5	442.5	-270.0
220	385.8	442.5	-270.0	221	410.0	442.5	-270.0	222	0.0	0.0	-231.7
223	37.9	0.0	-231.7	224	75.8	0.0	-231.7	225	113.8	0.0	-231.7
226	151.7	0.0	-231.7	227	189.6	0.0	-231.7	228	227.5	0.0	-231.7
229	267.1	0.0	-231.7	230	292.5	0.0	-231.7	231	306.7	0.0	-231.7
232	346.2	0.0	-231.7	233	372.5	0.0	-231.7	234	385.8	0.0	-231.7
235	410.0	0.0	-231.7	236	425.4	0.0	-231.7	237	465.0	0.0	-231.7
238	0.0	33.8	-231.7	239	465.0	33.8	-231.7	240	0.0	67.5	-231.7
241	465.0	67.5	-231.7	242	465.0	108.8	-231.7	243	465.0	150.0	-231.7
244	465.0	191.3	-231.7	245	465.0	232.5	-231.7	246	0.0	257.5	-231.7
247	465.0	257.5	-231.7	248	0.0	285.0	-231.7	249	465.0	285.0	-231.7
250	0.0	312.5	-231.7	251	465.0	312.5	-231.7	252	0.0	325.0	-231.7
253	37.9	325.0	-231.7	254	75.8	325.0	-231.7	255	113.8	325.0	-231.7
256	151.7	325.0	-231.7	257	189.6	325.0	-231.7	258	227.5	325.0	-231.7
259	267.1	325.0	-231.7	260	280.0	325.0	-231.7	261	292.5	325.0	-231.7
262	306.7	325.0	-231.7	263	346.3	325.0	-231.7	264	372.5	325.0	-231.7
265	385.8	325.0	-231.7	266	410.0	325.0	-231.7	267	425.4	325.0	-231.7
268	465.0	325.0	-231.7	269	280.0	337.5	-231.7	270	410.0	337.5	-231.7
271	280.0	377.5	-231.7	272	410.0	377.5	-231.7	273	280.0	417.5	-231.7
274	410.0	417.5	-231.7	275	280.0	442.5	-231.7	276	292.5	442.5	-231.7
277	320.0	442.5	-231.7	278	372.5	442.5	-231.7	279	385.8	442.5	-231.7
280	410.0	442.5	-231.7	281	0.0	0.0	-193.3	282	37.9	0.0	-193.3
283	75.8	0.0	-193.3	284	113.8	0.0	-193.3	285	151.7	0.0	-193.3
286	189.6	0.0	-193.3	287	227.5	0.0	-193.3	288	267.1	0.0	-193.3
289	292.5	0.0	-193.3	290	306.7	0.0	-193.3	291	346.2	0.0	-193.3
292	372.5	0.0	-193.3	293	385.8	0.0	-193.3	294	410.0	0.0	-193.3
295	425.4	0.0	-193.3	296	465.0	0.0	-193.3	297	0.0	33.8	-193.3
298	465.0	33.8	-193.3	299	0.0	67.5	-193.3	300	465.0	67.5	-193.3
301	465.0	108.8	-193.3	302	465.0	150.0	-193.3	303	465.0	191.3	-193.3
304	465.0	232.5	-193.3	305	0.0	257.5	-193.3	306	465.0	257.5	-193.3
307	0.0	285.0	-193.3	308	465.0	285.0	-193.3	309	0.0	312.5	-193.3
310	465.0	312.5	-193.3	311	0.0	325.0	-193.3	312	37.9	325.0	-193.3
313	75.8	325.0	-193.3	314	113.8	325.0	-193.3	315	151.7	325.0	-193.3
316	189.6	325.0	-193.3	317	227.5	325.0	-193.3	318	267.1	325.0	-193.3
319	280.0	325.0	-193.3	320	292.5	325.0	-193.3	321	306.7	325.0	-193.3
322	346.3	325.0	-193.3	323	372.5	325.0	-193.3	324	385.8	325.0	-193.3
325	410.0	325.0	-193.3	326	425.4	325.0	-193.3	327	465.0	325.0	-193.3
328	280.0	337.5	-193.3	329	410.0	337.5	-193.3	330	280.0	377.5	-193.3
331	410.0	377.5	-193.3	332	280.0	417.5	-193.3	333	410.0	417.5	-193.3
334	280.0	442.5	-193.3	335	292.5	442.5	-193.3	336	320.0	442.5	-193.3
337	372.5	442.5	-193.3	338	385.8	442.5	-193.3	339	410.0	442.5	-193.3
340	0.0	0.0	-155.0	341	37.9	0.0	-155.0	342	75.8	0.0	-155.0
343	113.8	0.0	-155.0	344	151.7	0.0	-155.0	345	189.6	0.0	-155.0
346	227.5	0.0	-155.0	347	267.1	0.0	-155.0	348	292.5	0.0	-155.0
349	306.7	0.0	-155.0	350	346.2	0.0	-155.0	351	372.5	0.0	-155.0
352	385.8	0.0	-155.0	353	410.0	0.0	-155.0	354	425.4	0.0	-155.0
355	465.0	0.0	-155.0	356	0.0	33.8	-155.0	357	465.0	33.8	-155.0
358	0.0	67.5	-155.0	359	465.0	67.5	-155.0	360	465.0	108.8	-155.0
361	465.0	150.0	-155.0	362	465.0	191.3	-155.0	363	465.0	232.5	-155.0
364	0.0	257.5	-155.0	365	465.0	257.5	-155.0	366	0.0	285.0	-155.0

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

367	465.0	285.0	-155.0	368	0.0	312.5	-155.0	369	465.0	312.5	-155.0
370	0.0	325.0	-155.0	371	37.9	325.0	-155.0	372	75.8	325.0	-155.0
373	113.8	325.0	-155.0	374	151.7	325.0	-155.0	375	189.6	325.0	-155.0
376	227.5	325.0	-155.0	377	267.1	325.0	-155.0	378	280.0	325.0	-155.0
379	292.5	325.0	-155.0	380	306.7	325.0	-155.0	381	346.3	325.0	-155.0
382	372.5	325.0	-155.0	383	385.8	325.0	-155.0	384	410.0	325.0	-155.0
385	425.4	325.0	-155.0	386	465.0	325.0	-155.0	387	280.0	337.5	-155.0
388	410.0	337.5	-155.0	389	280.0	377.5	-155.0	390	410.0	377.5	-155.0
391	280.0	417.5	-155.0	392	410.0	417.5	-155.0	393	280.0	442.5	-155.0
394	292.5	442.5	-155.0	395	320.0	442.5	-155.0	396	372.5	442.5	-155.0
397	385.8	442.5	-155.0	398	410.0	442.5	-155.0	399	0.0	0.0	-116.7
400	37.9	0.0	-116.7	401	75.8	0.0	-116.7	402	113.8	0.0	-116.7
403	151.7	0.0	-116.7	404	189.6	0.0	-116.7	405	227.5	0.0	-116.7
406	267.1	0.0	-116.7	407	292.5	0.0	-116.7	408	306.7	0.0	-116.7
409	346.3	0.0	-116.7	410	372.5	0.0	-116.7	411	385.8	0.0	-116.7
412	410.0	0.0	-116.7	413	425.4	0.0	-116.7	414	465.0	0.0	-116.7
415	0.0	33.8	-116.7	416	465.0	33.8	-116.7	417	0.0	67.5	-116.7
418	465.0	67.5	-116.7	419	465.0	108.8	-116.7	420	465.0	150.0	-116.7
421	465.0	191.3	-116.7	422	465.0	232.5	-116.7	423	0.0	257.5	-116.7
424	465.0	257.5	-116.7	425	0.0	285.0	-116.7	426	465.0	285.0	-116.7
427	0.0	312.5	-116.7	428	465.0	312.5	-116.7	429	0.0	325.0	-116.7
430	37.9	325.0	-116.7	431	75.8	325.0	-116.7	432	113.8	325.0	-116.7
433	151.7	325.0	-116.7	434	189.6	325.0	-116.7	435	227.5	325.0	-116.7
436	267.1	325.0	-116.7	437	280.0	325.0	-116.7	438	292.5	325.0	-116.7
439	306.7	325.0	-116.7	440	346.3	325.0	-116.7	441	372.5	325.0	-116.7
442	385.8	325.0	-116.7	443	410.0	325.0	-116.7	444	425.4	325.0	-116.7
445	465.0	325.0	-116.7	446	280.0	337.5	-116.7	447	410.0	337.5	-116.7
448	280.0	377.5	-116.7	449	410.0	377.5	-116.7	450	280.0	417.5	-116.7
451	410.0	417.5	-116.7	452	280.0	442.5	-116.7	453	292.5	442.5	-116.7
454	320.0	442.5	-116.7	455	372.5	442.5	-116.7	456	385.8	442.5	-116.7
457	410.0	442.5	-116.7	458	37.9	325.0	-82.2	459	75.8	325.0	-81.8
460	113.8	325.0	-81.5	461	151.7	325.0	-81.2	462	189.6	325.0	-80.8
463	227.5	325.0	-80.5	464	267.1	325.0	-80.1	465	0.0	0.0	-80.0
466	0.0	33.8	-80.0	467	0.0	67.5	-80.0	468	0.0	108.8	-80.0
469	0.0	150.0	-80.0	470	0.0	191.3	-80.0	471	0.0	232.5	-80.0
472	0.0	257.5	-80.0	473	0.0	285.0	-80.0	474	0.0	312.5	-80.0
475	0.0	325.0	-80.0	476	280.0	325.0	-80.0	477	280.0	337.5	-80.0
478	280.0	377.5	-80.0	479	280.0	417.5	-80.0	480	280.0	442.5	-80.0
481	292.5	442.5	-80.0	482	320.0	442.5	-80.0	483	372.5	442.5	-80.0
484	385.8	442.5	-80.0	485	410.0	442.5	-80.0	486	37.9	0.0	-79.9
487	292.5	325.0	-79.9	488	75.8	0.0	-79.7	489	306.7	325.0	-79.8
490	410.0	417.5	-79.8	491	113.8	0.0	-79.6	492	151.7	0.0	-79.5
493	346.3	325.0	-79.4	494	189.6	0.0	-79.3	495	410.0	377.5	-79.4
496	227.5	0.0	-79.2	497	372.5	325.0	-79.2	498	267.1	0.0	-79.0
499	385.8	325.0	-79.0	500	292.5	0.0	-79.0	501	410.0	337.5	-79.0
502	306.7	0.0	-78.9	503	410.0	325.0	-78.8	504	346.3	0.0	-78.8
505	372.5	0.0	-78.7	506	425.4	325.0	-78.7	507	385.8	0.0	-78.6
508	410.0	0.0	-78.5	509	425.4	0.0	-78.5	510	465.0	0.0	-78.3
511	465.0	33.8	-78.3	512	465.0	67.5	-78.3	513	465.0	108.8	-78.3
514	465.0	150.0	-78.3	515	465.0	191.3	-78.3	516	465.0	232.5	-78.3
517	465.0	257.5	-78.3	518	465.0	285.0	-78.3	519	465.0	312.5	-78.3
520	465.0	325.0	-78.3	521	0.0	0.0	-40.0	522	37.9	0.0	-40.0
523	75.8	0.0	-40.0	524	113.8	0.0	-40.0	525	151.7	0.0	-40.0
526	189.6	0.0	-40.0	527	227.5	0.0	-40.0	528	267.1	0.0	-40.0
529	292.5	0.0	-40.0	530	306.7	0.0	-40.0	531	346.3	0.0	-40.0
532	372.5	0.0	-40.0	533	385.8	0.0	-40.0	534	410.0	0.0	-40.0
535	425.4	0.0	-40.0	536	465.0	0.0	-40.0	537	0.0	33.8	-40.0
538	6.3	33.8	-40.0	539	37.9	33.8	-40.0	540	86.3	33.8	-40.0
541	113.8	33.8	-40.0	542	151.7	33.8	-40.0	543	189.6	33.8	-40.0
544	227.5	33.8	-40.0	545	240.0	33.8	-40.0	546	267.1	33.8	-40.0
547	292.5	33.8	-40.0	548	320.0	33.8	-40.0	549	346.3	33.8	-40.0
550	372.5	33.8	-40.0	551	385.8	33.8	-40.0	552	410.0	33.8	-40.0
553	425.4	33.8	-40.0	554	465.0	33.8	-40.0	555	0.0	67.5	-40.0
556	6.3	67.5	-40.0	557	37.9	67.5	-40.0	558	86.3	67.5	-40.0
559	113.8	67.5	-40.0	560	151.7	67.5	-40.0	561	189.6	67.5	-40.0
562	227.5	67.5	-40.0	563	240.0	67.5	-40.0	564	267.1	67.5	-40.0
565	292.5	67.5	-40.0	566	320.0	67.5	-40.0	567	346.3	67.5	-40.0
568	372.5	67.5	-40.0	569	385.8	67.5	-40.0	570	410.0	67.5	-40.0
571	425.4	67.5	-40.0	572	465.0	67.5	-40.0	573	0.0	108.8	-40.0
574	6.3	108.8	-40.0	575	37.9	108.8	-40.0	576	86.3	108.8	-40.0
577	113.8	108.8	-40.0	578	151.7	108.8	-40.0	579	189.6	108.8	-40.0
580	227.5	108.8	-40.0	581	240.0	108.8	-40.0	582	267.1	108.7	-40.0
583	292.5	108.8	-40.0	584	320.0	108.8	-40.0	585	346.3	108.8	-40.0
586	372.5	108.8	-40.0	587	385.8	108.7	-40.0	588	410.0	108.8	-40.0
589	425.4	108.7	-40.0	590	465.0	108.8	-40.0	591	0.0	150.0	-40.0
592	6.3	150.0	-40.0	593	37.9	150.0	-40.0	594	86.3	150.0	-40.0
595	113.8	150.0	-40.0	596	151.7	150.0	-40.0	597	189.6	150.0	-40.0
598	227.5	150.0	-40.0	599	240.0	150.0	-40.0	600	267.1	150.0	-40.0
601	292.5	150.0	-40.0	602	320.0	150.0	-40.0	603	346.3	150.0	-40.0

SCARICATORE IN VIA PUCCI

604	372.5	150.0	-40.0	605	385.8	150.0	-40.0	606	410.0	150.0	-40.0
607	425.4	150.0	-40.0	608	465.0	150.0	-40.0	609	0.0	191.3	-40.0
610	6.3	191.3	-40.0	611	37.9	191.3	-40.0	612	86.3	191.3	-40.0
613	113.8	191.3	-40.0	614	151.7	191.3	-40.0	615	189.6	191.3	-40.0
616	227.5	191.3	-40.0	617	240.0	191.3	-40.0	618	267.1	191.3	-40.0
619	292.5	191.3	-40.0	620	320.0	191.3	-40.0	621	346.3	191.3	-40.0
622	372.5	191.3	-40.0	623	385.8	191.3	-40.0	624	410.0	191.3	-40.0
625	425.4	191.3	-40.0	626	465.0	191.3	-40.0	627	0.0	232.5	-40.0
628	6.3	232.5	-40.0	629	37.9	232.5	-40.0	630	86.3	232.5	-40.0
631	113.8	232.5	-40.0	632	151.7	232.5	-40.0	633	189.6	232.5	-40.0
634	227.5	232.5	-40.0	635	240.0	232.5	-40.0	636	267.1	232.5	-40.0
637	292.5	232.5	-40.0	638	320.0	232.5	-40.0	639	346.3	232.5	-40.0
640	372.5	232.5	-40.0	641	385.8	232.5	-40.0	642	410.0	232.5	-40.0
643	425.4	232.5	-40.0	644	465.0	232.5	-40.0	645	0.0	257.5	-40.0
646	6.3	257.5	-40.0	647	37.9	257.5	-40.0	648	86.3	257.5	-40.0
649	113.8	257.5	-40.0	650	151.7	257.5	-40.0	651	189.6	257.5	-40.0
652	227.5	257.5	-40.0	653	248.5	257.5	-40.0	654	271.1	257.5	-40.0
655	292.5	257.5	-40.0	656	320.0	257.5	-40.0	657	346.3	257.5	-40.0
658	372.5	257.5	-40.0	659	385.8	257.5	-40.0	660	410.0	257.5	-40.0
661	425.4	257.5	-40.0	662	465.0	257.5	-40.0	663	0.0	285.0	-40.0
664	6.3	285.0	-40.0	665	37.9	285.0	-40.0	666	86.3	285.0	-40.0
667	113.8	285.0	-40.0	668	151.7	285.0	-40.0	669	189.6	285.0	-40.0
670	227.5	285.0	-40.0	671	257.8	285.0	-40.0	672	275.6	285.0	-40.0
673	292.5	285.0	-40.0	674	320.0	285.0	-40.0	675	346.3	285.0	-40.0
676	372.5	285.0	-40.0	677	385.8	285.0	-40.0	678	410.0	285.0	-40.0
679	425.4	285.0	-40.0	680	465.0	285.0	-40.0	681	0.0	312.5	-40.0
682	6.3	312.5	-40.0	683	37.9	312.5	-40.0	684	86.3	312.5	-40.0
685	113.8	312.5	-40.0	686	151.7	312.5	-40.0	687	189.6	312.5	-40.0
688	227.5	312.5	-40.0	689	240.0	312.5	-40.0	690	267.1	312.5	-40.0
691	280.0	312.5	-40.0	692	292.5	312.5	-40.0	693	320.0	312.5	-40.0
694	346.3	312.5	-40.0	695	372.5	312.5	-40.0	696	385.8	312.5	-40.0
697	410.0	312.5	-40.0	698	425.4	312.5	-40.0	699	465.0	312.5	-40.0
700	0.0	325.0	-40.0	701	37.9	325.0	-40.0	702	75.8	325.0	-40.0
703	113.8	325.0	-40.0	704	151.7	325.0	-40.0	705	189.6	325.0	-40.0
706	227.5	325.0	-40.0	707	267.1	325.0	-40.0	708	280.0	325.0	-40.0
709	292.5	325.0	-40.0	710	320.0	325.0	-40.0	711	346.3	325.0	-40.0
712	372.5	325.0	-40.0	713	385.8	325.0	-40.0	714	410.0	325.0	-40.0
715	425.4	325.0	-40.0	716	465.0	325.0	-40.0	717	280.0	337.5	-40.0
718	292.5	337.5	-40.0	719	320.0	337.5	-40.0	720	346.3	337.5	-40.0
721	372.5	337.5	-40.0	722	385.8	337.5	-40.0	723	410.0	337.5	-40.0
724	280.0	377.5	-40.0	725	292.5	377.5	-40.0	726	320.0	377.5	-40.0
727	372.5	377.5	-40.0	728	385.8	377.5	-40.0	729	410.0	377.5	-40.0
730	280.0	417.5	-40.0	731	292.5	417.5	-40.0	732	320.0	417.5	-40.0
733	372.5	417.5	-40.0	734	385.8	417.5	-40.0	735	410.0	417.5	-40.0
736	280.0	442.5	-40.0	737	292.5	442.5	-40.0	738	320.0	442.5	-40.0
739	372.5	442.5	-40.0	740	385.8	442.5	-40.0	741	410.0	442.5	-40.0

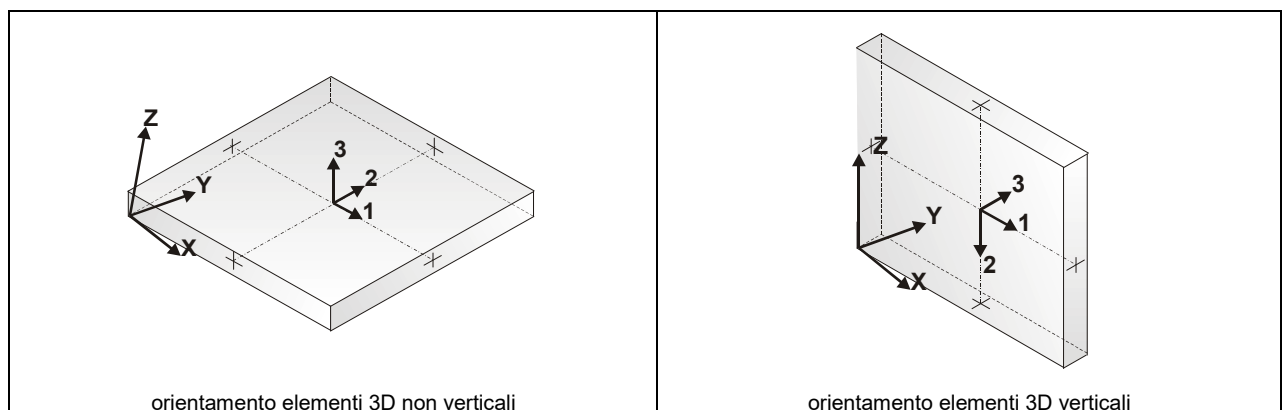
MODELLAZIONE STRUTTURA: ELEMENTI SHELL

LEGENDA TABELLA DATI SHELL

Il programma utilizza per la modellazione elementi a tre o quattro nodi denominati in generale shell.

Ogni elemento shell è individuato dai nodi I, J, K, L (L=I per gli elementi a tre nodi).

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione.



In particolare per ogni elemento viene indicato in tabella:

Elem.	numero dell'elemento
Note	codice di comportamento: Guscio (elemento guscio in elevazione non verticale) Guscio fond. (elemento guscio su suolo elastico) Setto (elemento guscio in elevazione verticale) Membrana (elemento guscio con comportamento membranale)
Nodo I (J, K, L)	numero del nodo I (J, K, L)
Mat.	codice del materiale assegnato all'elemento
Spessore	spessore dell'elemento (costante)
Wink V	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico verticale
Wink O	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico orizzontale

Con riferimento al **Documento di Affidabilità** “Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST” - versione Maggio 2011, disponibile per il download sul sito **www.2si.it**, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
8	MENSOLE CON ELEMENTI PLATE E MATERIALE ORTOTROPO
10	PIASTRA CON ELEMENTI PLATE E MATERIALE ORTOTROPO
21	DRILLING
25	TENSIONI DI ELEMENTI PLATE
31	REALIZZAZIONE DI MESH PIANA SU GEOMETRIA CON PUNTI FISSI IMPORTATA DA FILE .DXF
32	REALIZZAZIONE DI MESH PIANA SU GEOMETRIA CON SEGMENTI E FORI INTERNI IMPORTATA DA FILE .DXF
33	REALIZZAZIONE DI MESH PIANE SU GEOMETRIE COSTRUITE IN PRO_SAP
34	ANALISI DI BUCKLING DI PIASTRA ISOTROPA
35	ANALISI DI BUCKLING DI UN CILINDRO COMPRESSO INCASTRATO ALLA BASE
36	ANALISI DI PARETI FORATE
37	BIMETALLIC STRIP (NAFEMS EXERCISE 6)
38	ANALISI ELASTICA DI PIASTRA CON INTAGLIO CIRCOLARE (FLAT BAR WITH EDGE NOTCHES-NAFEMS EXERCISE 9)
39	PLATEA NERVATA
45	VERIFICA A PUNZONAMENTO ALLO SLU DI PIASTRE IN C.A.
117	PROGETTO E VERIFICA DI GUSCI IN MATERIALE XLAM
118	PROGETTO E VERIFICA DI PARETI IN MATERIALE XLAM E RELATIVI COLLEGAMENTI

Elem.	Note	Nodo I	Nodo J	Nodo K	Nodo L	Mat.	Spessore cm	Svincolo	Wink V daN/cm3	Wink O daN/cm3
1	Guscio fond.	1	2	9	8	3	50.0		0.33	0.19
2	Guscio fond.	2	3	10	9	3	50.0		0.33	0.19
3	Guscio fond.	3	4	11	10	3	50.0		0.33	0.19
4	Guscio fond.	4	5	12	11	3	50.0		0.33	0.19
5	Guscio fond.	5	6	14	13	3	50.0		0.33	0.19
6	Guscio fond.	6	7	15	14	3	50.0		0.33	0.19
7	Guscio fond.	12	5	13		3	50.0		0.33	0.19
8	Guscio fond.	11	12	19		3	50.0		0.33	0.19
9	Guscio fond.	13	14	20		3	50.0		0.33	0.19
10	Guscio fond.	14	15	20		3	50.0		0.33	0.19
11	Guscio fond.	8	9	17	16	3	50.0		0.33	0.19
12	Guscio fond.	9	10	18	17	3	50.0		0.33	0.19
13	Guscio fond.	10	11	19	18	3	50.0		0.33	0.19
14	Guscio fond.	12	13	20	19	3	50.0		0.33	0.19
15	Guscio fond.	20	15	21		3	50.0		0.33	0.19
16	Guscio fond.	16	17	23	22	3	50.0		0.33	0.19
17	Guscio fond.	17	18	24	23	3	50.0		0.33	0.19
18	Guscio fond.	18	19	25	24	3	50.0		0.33	0.19

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

19	Guscio fond.	19	20	26	25	3	50.0	0.33	0.19
20	Guscio fond.	20	21	27	26	3	50.0	0.33	0.19
21	Guscio fond.	22	23	29	28	3	50.0	0.33	0.19
22	Guscio fond.	23	24	30	29	3	50.0	0.33	0.19
23	Guscio fond.	24	25	31	30	3	50.0	0.33	0.19
24	Guscio fond.	25	26	32	31	3	50.0	0.33	0.19
25	Guscio fond.	26	27	33	32	3	50.0	0.33	0.19
26	Setto	201	202	2	1	3	20.0		
27	Setto	202	203	3	2	3	20.0		
28	Setto	203	204	4	3	3	20.0		
29	Setto	204	205	5	4	3	20.0		
30	Setto	205	206	6	5	3	20.0		
31	Setto	206	207	7	6	3	20.0		
32	Setto	1	8	210	201	3	20.0		
33	Setto	7	15	211	207	3	20.0		
34	Setto	8	16	212	210	3	20.0		
35	Setto	15	21	213	211	3	20.0		
36	Setto	16	22	214	212	3	20.0		
37	Setto	21	27	215	213	3	20.0		
38	Setto	22	28	216	214	3	20.0		
39	Setto	27	33	221	215	3	20.0		
40	Setto	216	217	29	28	3	20.0		
41	Setto	217	218	30	29	3	20.0		
42	Setto	218	219	31	30	3	20.0		
43	Setto	219	220	32	31	3	20.0		
44	Setto	220	221	33	32	3	20.0		
45	Guscio fond.	34	35	51	50	3	50.0	0.13	0.07
46	Guscio fond.	35	36	52	51	3	50.0	0.13	0.07
47	Guscio fond.	36	37	53	52	3	50.0	0.13	0.07
48	Guscio fond.	37	38	54	53	3	50.0	0.13	0.07
49	Guscio fond.	38	39	55	54	3	50.0	0.13	0.07
50	Guscio fond.	39	40	56	55	3	50.0	0.13	0.07
51	Guscio fond.	40	41	57	56	3	50.0	0.13	0.07
52	Guscio fond.	41	42	58	57	3	50.0	0.13	0.07
53	Guscio fond.	42	43	59	58	3	50.0	0.13	0.07
54	Guscio fond.	43	44	60	59	3	50.0	0.13	0.07
55	Guscio fond.	44	45	61	60	3	50.0	0.13	0.07
56	Guscio fond.	45	46	62	61	3	50.0	0.13	0.07
57	Guscio fond.	46	47	63	62	3	50.0	0.13	0.07
58	Guscio fond.	47	48	64	63	3	50.0	0.13	0.07
59	Guscio fond.	48	49	65	64	3	50.0	0.13	0.07
60	Guscio fond.	50	51	67	66	3	50.0	0.13	0.07
61	Guscio fond.	51	52	68	67	3	50.0	0.13	0.07
62	Guscio fond.	52	53	69	68	3	50.0	0.13	0.07
63	Guscio fond.	53	54	70	69	3	50.0	0.13	0.07
64	Guscio fond.	54	55	71	70	3	50.0	0.13	0.07
65	Guscio fond.	55	56	72	71	3	50.0	0.13	0.07
66	Guscio fond.	56	57	73	72	3	50.0	0.13	0.07
67	Guscio fond.	57	58	74	73	3	50.0	0.13	0.07
68	Guscio fond.	58	59	75	74	3	50.0	0.13	0.07
69	Guscio fond.	59	60	76	75	3	50.0	0.13	0.07
70	Guscio fond.	60	61	77	76	3	50.0	0.13	0.07
71	Guscio fond.	61	62	78	77	3	50.0	0.13	0.07
72	Guscio fond.	62	63	79	78	3	50.0	0.13	0.07
73	Guscio fond.	63	64	80	79	3	50.0	0.13	0.07
74	Guscio fond.	64	65	81	80	3	50.0	0.13	0.07
75	Guscio fond.	66	67	83	82	3	50.0	0.13	0.07
76	Guscio fond.	67	68	84	83	3	50.0	0.13	0.07
77	Guscio fond.	68	69	85	84	3	50.0	0.13	0.07
78	Guscio fond.	69	70	86	85	3	50.0	0.13	0.07
79	Guscio fond.	70	71	87	86	3	50.0	0.13	0.07
80	Guscio fond.	71	72	88	87	3	50.0	0.13	0.07
81	Guscio fond.	72	73	89	88	3	50.0	0.13	0.07
82	Guscio fond.	73	74	90	89	3	50.0	0.13	0.07
83	Guscio fond.	74	75	91	90	3	50.0	0.13	0.07
84	Guscio fond.	75	76	92	91	3	50.0	0.13	0.07
85	Guscio fond.	76	77	93	92	3	50.0	0.13	0.07
86	Guscio fond.	77	78	94	93	3	50.0	0.13	0.07
87	Guscio fond.	78	79	95	94	3	50.0	0.13	0.07
88	Guscio fond.	79	80	96	95	3	50.0	0.13	0.07
89	Guscio fond.	80	81	97	96	3	50.0	0.13	0.07
90	Guscio fond.	82	83	99	98	3	50.0	0.13	0.07
91	Guscio fond.	83	84	100	99	3	50.0	0.13	0.07
92	Guscio fond.	84	85	101	100	3	50.0	0.13	0.07
93	Guscio fond.	85	86	102	101	3	50.0	0.13	0.07
94	Guscio fond.	86	87	103	102	3	50.0	0.13	0.07
95	Guscio fond.	87	88	104	103	3	50.0	0.13	0.07
96	Guscio fond.	88	89	105	104	3	50.0	0.13	0.07
97	Guscio fond.	89	90	106	105	3	50.0	0.13	0.07

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98	Guscio fond.	90	91	107	106	3	50.0	0.13	0.07
99	Guscio fond.	91	92	108	107	3	50.0	0.13	0.07
100	Guscio fond.	92	93	109	108	3	50.0	0.13	0.07
101	Guscio fond.	93	94	110	109	3	50.0	0.13	0.07
102	Guscio fond.	94	95	111	110	3	50.0	0.13	0.07
103	Guscio fond.	95	96	112	111	3	50.0	0.13	0.07
104	Guscio fond.	96	97	113	112	3	50.0	0.13	0.07
105	Guscio fond.	98	99	115	114	3	50.0	0.13	0.07
106	Guscio fond.	99	100	116	115	3	50.0	0.13	0.07
107	Guscio fond.	100	101	117	116	3	50.0	0.13	0.07
108	Guscio fond.	101	102	118	117	3	50.0	0.13	0.07
109	Guscio fond.	102	103	119	118	3	50.0	0.13	0.07
110	Guscio fond.	103	104	120	119	3	50.0	0.13	0.07
111	Guscio fond.	104	105	121	120	3	50.0	0.13	0.07
112	Guscio fond.	105	106	122	121	3	50.0	0.13	0.07
113	Guscio fond.	106	107	123	122	3	50.0	0.13	0.07
114	Guscio fond.	107	108	124	123	3	50.0	0.13	0.07
115	Guscio fond.	108	109	125	124	3	50.0	0.13	0.07
116	Guscio fond.	109	110	126	125	3	50.0	0.13	0.07
117	Guscio fond.	110	111	127	126	3	50.0	0.13	0.07
118	Guscio fond.	111	112	128	127	3	50.0	0.13	0.07
119	Guscio fond.	112	113	129	128	3	50.0	0.13	0.07
120	Guscio fond.	114	115	131	130	3	50.0	0.13	0.07
121	Guscio fond.	115	116	132	131	3	50.0	0.13	0.07
122	Guscio fond.	116	117	133	132	3	50.0	0.13	0.07
123	Guscio fond.	117	118	134	133	3	50.0	0.13	0.07
124	Guscio fond.	118	119	135	134	3	50.0	0.13	0.07
125	Guscio fond.	119	120	136	135	3	50.0	0.13	0.07
126	Guscio fond.	120	121	137	136	3	50.0	0.13	0.07
127	Guscio fond.	121	122	138	137	3	50.0	0.13	0.07
128	Guscio fond.	122	123	139	138	3	50.0	0.13	0.07
129	Guscio fond.	123	124	140	139	3	50.0	0.13	0.07
130	Guscio fond.	124	125	141	140	3	50.0	0.13	0.07
131	Guscio fond.	125	126	142	141	3	50.0	0.13	0.07
132	Guscio fond.	126	127	143	142	3	50.0	0.13	0.07
133	Guscio fond.	127	128	144	143	3	50.0	0.13	0.07
134	Guscio fond.	128	129	145	144	3	50.0	0.13	0.07
135	Guscio fond.	130	131	147	146	3	50.0	0.13	0.07
136	Guscio fond.	131	132	148	147	3	50.0	0.13	0.07
137	Guscio fond.	132	133	149	148	3	50.0	0.13	0.07
138	Guscio fond.	133	134	150	149	3	50.0	0.13	0.07
139	Guscio fond.	134	135	151	150	3	50.0	0.13	0.07
140	Guscio fond.	135	136	152	151	3	50.0	0.13	0.07
141	Guscio fond.	136	137	153	152	3	50.0	0.13	0.07
142	Guscio fond.	137	138	154	153	3	50.0	0.13	0.07
143	Guscio fond.	138	139	155	154	3	50.0	0.13	0.07
144	Guscio fond.	139	140	156	155	3	50.0	0.13	0.07
145	Guscio fond.	140	141	157	156	3	50.0	0.13	0.07
146	Guscio fond.	141	142	158	157	3	50.0	0.13	0.07
147	Guscio fond.	142	143	159	158	3	50.0	0.13	0.07
148	Guscio fond.	143	144	160	159	3	50.0	0.13	0.07
149	Guscio fond.	144	145	161	160	3	50.0	0.13	0.07
150	Guscio fond.	146	147	163	162	3	50.0	0.13	0.07
151	Guscio fond.	147	148	164	163	3	50.0	0.13	0.07
152	Guscio fond.	148	149	165	164	3	50.0	0.13	0.07
153	Guscio fond.	149	150	166	165	3	50.0	0.13	0.07
154	Guscio fond.	150	151	167	166	3	50.0	0.13	0.07
155	Guscio fond.	151	152	168	167	3	50.0	0.13	0.07
156	Guscio fond.	152	153	169	168	3	50.0	0.13	0.07
157	Guscio fond.	153	154	170	169	3	50.0	0.13	0.07
158	Guscio fond.	154	155	171	170	3	50.0	0.13	0.07
159	Guscio fond.	155	156	172	171	3	50.0	0.13	0.07
160	Guscio fond.	156	157	173	172	3	50.0	0.13	0.07
161	Guscio fond.	157	158	174	173	3	50.0	0.13	0.07
162	Guscio fond.	158	159	175	174	3	50.0	0.13	0.07
163	Guscio fond.	159	160	176	175	3	50.0	0.13	0.07
164	Guscio fond.	160	161	177	176	3	50.0	0.13	0.07
165	Guscio fond.	162	163	179	178	3	50.0	0.13	0.07
166	Guscio fond.	163	164	180	179	3	50.0	0.13	0.07
167	Guscio fond.	164	165	181	180	3	50.0	0.13	0.07
168	Guscio fond.	165	166	182	181	3	50.0	0.13	0.07
169	Guscio fond.	166	167	183	182	3	50.0	0.13	0.07
170	Guscio fond.	167	168	184	183	3	50.0	0.13	0.07
171	Guscio fond.	168	169	185	184	3	50.0	0.13	0.07
172	Guscio fond.	169	170	186	185	3	50.0	0.13	0.07
173	Guscio fond.	170	171	187	186	3	50.0	0.13	0.07
174	Guscio fond.	171	172	188	187	3	50.0	0.13	0.07
175	Guscio fond.	172	173	189	188	3	50.0	0.13	0.07
176	Guscio fond.	173	174	190	189	3	50.0	0.13	0.07

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177	Guscio fond.	174	175	191	190	3	50.0	0.13	0.07
178	Guscio fond.	175	176	192	191	3	50.0	0.13	0.07
179	Guscio fond.	176	177	193	192	3	50.0	0.13	0.07
180	Guscio fond.	178	179	195	194	3	50.0	0.13	0.07
181	Guscio fond.	179	180	196	195	3	50.0	0.13	0.07
182	Guscio fond.	180	181	197	196	3	50.0	0.13	0.07
183	Guscio fond.	181	182	198	197	3	50.0	0.13	0.07
184	Guscio fond.	182	183	199	198	3	50.0	0.13	0.07
185	Guscio fond.	183	184	200	199	3	50.0	0.13	0.07
186	Guscio fond.	184	185	201	200	3	50.0	0.13	0.07
187	Guscio fond.	185	186	202	201	3	50.0	0.13	0.07
188	Guscio fond.	186	187	203	202	3	50.0	0.13	0.07
189	Guscio fond.	187	188	204	203	3	50.0	0.13	0.07
190	Guscio fond.	188	189	205	204	3	50.0	0.13	0.07
191	Guscio fond.	189	190	206	205	3	50.0	0.13	0.07
192	Guscio fond.	190	191	207	206	3	50.0	0.13	0.07
193	Guscio fond.	191	192	208	207	3	50.0	0.13	0.07
194	Guscio fond.	192	193	209	208	3	50.0	0.13	0.07
195	Setto	222	223	35	34	3	20.0		
196	Setto	223	224	36	35	3	20.0		
197	Setto	224	225	37	36	3	20.0		
198	Setto	225	226	38	37	3	20.0		
199	Setto	226	227	39	38	3	20.0		
200	Setto	227	228	40	39	3	20.0		
201	Setto	228	229	41	40	3	20.0		
202	Setto	229	230	42	41	3	20.0		
203	Setto	230	231	43	42	3	20.0		
204	Setto	231	232	44	43	3	20.0		
205	Setto	232	233	45	44	3	20.0		
206	Setto	233	234	46	45	3	20.0		
207	Setto	234	235	47	46	3	20.0		
208	Setto	235	236	48	47	3	20.0		
209	Setto	236	237	49	48	3	20.0		
210	Setto	34	50	238	222	3	20.0		
211	Setto	49	65	239	237	3	20.0		
212	Setto	50	66	240	238	3	20.0		
213	Setto	65	81	241	239	3	20.0		
214	Setto	81	97	242	241	3	20.0		
215	Setto	97	113	243	242	3	20.0		
216	Setto	113	129	244	243	3	20.0		
217	Setto	129	145	245	244	3	20.0		
218	Setto	145	161	247	245	3	20.0		
219	Setto	146	162	248	246	3	20.0		
220	Setto	161	177	249	247	3	20.0		
221	Setto	162	178	250	248	3	20.0		
222	Setto	177	193	251	249	3	20.0		
223	Setto	178	194	252	250	3	20.0		
224	Setto	193	209	268	251	3	20.0		
225	Setto	252	253	195	194	3	20.0		
226	Setto	253	254	196	195	3	20.0		
227	Setto	254	255	197	196	3	20.0		
228	Setto	255	256	198	197	3	20.0		
229	Setto	256	257	199	198	3	20.0		
230	Setto	257	258	200	199	3	20.0		
231	Setto	258	259	201	200	3	20.0		
232	Setto	260	261	202	201	3	20.0		
233	Setto	261	262	203	202	3	20.0		
234	Setto	262	263	204	203	3	20.0		
235	Setto	263	264	205	204	3	20.0		
236	Setto	264	265	206	205	3	20.0		
237	Setto	265	266	207	206	3	20.0		
238	Setto	266	267	208	207	3	20.0		
239	Setto	267	268	209	208	3	20.0		
240	Setto	201	210	269	260	3	20.0		
241	Setto	207	211	270	266	3	20.0		
242	Setto	210	212	271	269	3	20.0		
243	Setto	211	213	272	270	3	20.0		
244	Setto	212	214	273	271	3	20.0		
245	Setto	213	215	274	272	3	20.0		
246	Setto	214	216	275	273	3	20.0		
247	Setto	215	221	280	274	3	20.0		
248	Setto	275	276	217	216	3	20.0		
249	Setto	276	277	218	217	3	20.0		
250	Setto	277	278	219	218	3	20.0		
251	Setto	278	279	220	219	3	20.0		
252	Setto	279	280	221	220	3	20.0		
253	Setto	259	260	201		3	20.0		
254	Setto	281	282	223	222	3	20.0		
255	Setto	282	283	224	223	3	20.0		

SCARICATORE IN VIA PUCCI

256	Setto	283	284	225	224	3	20.0
257	Setto	284	285	226	225	3	20.0
258	Setto	285	286	227	226	3	20.0
259	Setto	286	287	228	227	3	20.0
260	Setto	287	288	229	228	3	20.0
261	Setto	288	289	230	229	3	20.0
262	Setto	289	290	231	230	3	20.0
263	Setto	290	291	232	231	3	20.0
264	Setto	291	292	233	232	3	20.0
265	Setto	292	293	234	233	3	20.0
266	Setto	293	294	235	234	3	20.0
267	Setto	294	295	236	235	3	20.0
268	Setto	295	296	237	236	3	20.0
269	Setto	222	238	297	281	3	20.0
270	Setto	237	239	298	296	3	20.0
271	Setto	238	240	299	297	3	20.0
272	Setto	239	241	300	298	3	20.0
273	Setto	241	242	301	300	3	20.0
274	Setto	242	243	302	301	3	20.0
275	Setto	243	244	303	302	3	20.0
276	Setto	244	245	304	303	3	20.0
277	Setto	245	247	306	304	3	20.0
278	Setto	246	248	307	305	3	20.0
279	Setto	247	249	308	306	3	20.0
280	Setto	248	250	309	307	3	20.0
281	Setto	249	251	310	308	3	20.0
282	Setto	250	252	311	309	3	20.0
283	Setto	251	268	327	310	3	20.0
284	Setto	311	312	253	252	3	20.0
285	Setto	312	313	254	253	3	20.0
286	Setto	313	314	255	254	3	20.0
287	Setto	314	315	256	255	3	20.0
288	Setto	315	316	257	256	3	20.0
289	Setto	316	317	258	257	3	20.0
290	Setto	317	318	259	258	3	20.0
291	Setto	318	319	260	259	3	20.0
292	Setto	319	320	261	260	3	20.0
293	Setto	320	321	262	261	3	20.0
294	Setto	321	322	263	262	3	20.0
295	Setto	322	323	264	263	3	20.0
296	Setto	323	324	265	264	3	20.0
297	Setto	324	325	266	265	3	20.0
298	Setto	325	326	267	266	3	20.0
299	Setto	326	327	268	267	3	20.0
300	Setto	260	269	328	319	3	20.0
301	Setto	266	270	329	325	3	20.0
302	Setto	269	271	330	328	3	20.0
303	Setto	270	272	331	329	3	20.0
304	Setto	271	273	332	330	3	20.0
305	Setto	272	274	333	331	3	20.0
306	Setto	273	275	334	332	3	20.0
307	Setto	274	280	339	333	3	20.0
308	Setto	334	335	276	275	3	20.0
309	Setto	335	336	277	276	3	20.0
310	Setto	336	337	278	277	3	20.0
311	Setto	337	338	279	278	3	20.0
312	Setto	338	339	280	279	3	20.0
313	Setto	340	341	282	281	3	20.0
314	Setto	341	342	283	282	3	20.0
315	Setto	342	343	284	283	3	20.0
316	Setto	343	344	285	284	3	20.0
317	Setto	344	345	286	285	3	20.0
318	Setto	345	346	287	286	3	20.0
319	Setto	346	347	288	287	3	20.0
320	Setto	347	348	289	288	3	20.0
321	Setto	348	349	290	289	3	20.0
322	Setto	349	350	291	290	3	20.0
323	Setto	350	351	292	291	3	20.0
324	Setto	351	352	293	292	3	20.0
325	Setto	352	353	294	293	3	20.0
326	Setto	353	354	295	294	3	20.0
327	Setto	354	355	296	295	3	20.0
328	Setto	281	297	356	340	3	20.0
329	Setto	296	298	357	355	3	20.0
330	Setto	297	299	358	356	3	20.0
331	Setto	298	300	359	357	3	20.0
332	Setto	300	301	360	359	3	20.0
333	Setto	301	302	361	360	3	20.0
334	Setto	302	303	362	361	3	20.0

SCARICATORE IN VIA PUCCI

335	Setto	303	304	363	362	3	20.0
336	Setto	304	306	365	363	3	20.0
337	Setto	305	307	366	364	3	20.0
338	Setto	306	308	367	365	3	20.0
339	Setto	307	309	368	366	3	20.0
340	Setto	308	310	369	367	3	20.0
341	Setto	309	311	370	368	3	20.0
342	Setto	310	327	386	369	3	20.0
343	Setto	370	371	312	311	3	20.0
344	Setto	371	372	313	312	3	20.0
345	Setto	372	373	314	313	3	20.0
346	Setto	373	374	315	314	3	20.0
347	Setto	374	375	316	315	3	20.0
348	Setto	375	376	317	316	3	20.0
349	Setto	376	377	318	317	3	20.0
350	Setto	377	378	319	318	3	20.0
351	Setto	378	379	320	319	3	20.0
352	Setto	379	380	321	320	3	20.0
353	Setto	380	381	322	321	3	20.0
354	Setto	381	382	323	322	3	20.0
355	Setto	382	383	324	323	3	20.0
356	Setto	383	384	325	324	3	20.0
357	Setto	384	385	326	325	3	20.0
358	Setto	385	386	327	326	3	20.0
359	Setto	319	328	387	378	3	20.0
360	Setto	325	329	388	384	3	20.0
361	Setto	328	330	389	387	3	20.0
362	Setto	329	331	390	388	3	20.0
363	Setto	330	332	391	389	3	20.0
364	Setto	331	333	392	390	3	20.0
365	Setto	332	334	393	391	3	20.0
366	Setto	333	339	398	392	3	20.0
367	Setto	393	394	335	334	3	20.0
368	Setto	394	395	336	335	3	20.0
369	Setto	395	396	337	336	3	20.0
370	Setto	396	397	338	337	3	20.0
371	Setto	397	398	339	338	3	20.0
372	Setto	399	400	341	340	3	20.0
373	Setto	400	401	342	341	3	20.0
374	Setto	401	402	343	342	3	20.0
375	Setto	402	403	344	343	3	20.0
376	Setto	403	404	345	344	3	20.0
377	Setto	404	405	346	345	3	20.0
378	Setto	405	406	347	346	3	20.0
379	Setto	406	407	348	347	3	20.0
380	Setto	407	408	349	348	3	20.0
381	Setto	408	409	350	349	3	20.0
382	Setto	409	410	351	350	3	20.0
383	Setto	410	411	352	351	3	20.0
384	Setto	411	412	353	352	3	20.0
385	Setto	412	413	354	353	3	20.0
386	Setto	413	414	355	354	3	20.0
387	Setto	340	356	415	399	3	20.0
388	Setto	355	357	416	414	3	20.0
389	Setto	356	358	417	415	3	20.0
390	Setto	357	359	418	416	3	20.0
391	Setto	359	360	419	418	3	20.0
392	Setto	360	361	420	419	3	20.0
393	Setto	361	362	421	420	3	20.0
394	Setto	362	363	422	421	3	20.0
395	Setto	363	365	424	422	3	20.0
396	Setto	364	366	425	423	3	20.0
397	Setto	365	367	426	424	3	20.0
398	Setto	366	368	427	425	3	20.0
399	Setto	367	369	428	426	3	20.0
400	Setto	368	370	429	427	3	20.0
401	Setto	369	386	445	428	3	20.0
402	Setto	429	430	371	370	3	20.0
403	Setto	430	431	372	371	3	20.0
404	Setto	431	432	373	372	3	20.0
405	Setto	432	433	374	373	3	20.0
406	Setto	433	434	375	374	3	20.0
407	Setto	434	435	376	375	3	20.0
408	Setto	435	436	377	376	3	20.0
409	Setto	436	437	378	377	3	20.0
410	Setto	437	438	379	378	3	20.0
411	Setto	438	439	380	379	3	20.0
412	Setto	439	440	381	380	3	20.0
413	Setto	440	441	382	381	3	20.0

SCARICATORE IN VIA PUCCI

414	Setto	441	442	383	382	3	20.0
415	Setto	442	443	384	383	3	20.0
416	Setto	443	444	385	384	3	20.0
417	Setto	444	445	386	385	3	20.0
418	Setto	378	387	446	437	3	20.0
419	Setto	384	388	447	443	3	20.0
420	Setto	387	389	448	446	3	20.0
421	Setto	388	390	449	447	3	20.0
422	Setto	389	391	450	448	3	20.0
423	Setto	390	392	451	449	3	20.0
424	Setto	391	393	452	450	3	20.0
425	Setto	392	398	457	451	3	20.0
426	Setto	452	453	394	393	3	20.0
427	Setto	453	454	395	394	3	20.0
428	Setto	454	455	396	395	3	20.0
429	Setto	455	456	397	396	3	20.0
430	Setto	456	457	398	397	3	20.0
431	Setto	458	459	431	430	3	20.0
432	Setto	459	460	432	431	3	20.0
433	Setto	460	461	433	432	3	20.0
434	Setto	475	458	430	429	3	20.0
435	Setto	461	462	434	433	3	20.0
436	Setto	462	463	435	434	3	20.0
437	Setto	463	464	436	435	3	20.0
438	Setto	465	486	400	399	3	20.0
439	Setto	399	415	466	465	3	20.0
440	Setto	415	417	467	466	3	20.0
441	Setto	423	425	473	472	3	20.0
442	Setto	425	427	474	473	3	20.0
443	Setto	427	429	475	474	3	20.0
444	Setto	464	476	437	436	3	20.0
445	Setto	476	487	438	437	3	20.0
446	Setto	437	446	477	476	3	20.0
447	Setto	446	448	478	477	3	20.0
448	Setto	448	450	479	478	3	20.0
449	Setto	450	452	480	479	3	20.0
450	Setto	480	481	453	452	3	20.0
451	Setto	481	482	454	453	3	20.0
452	Setto	482	483	455	454	3	20.0
453	Setto	483	484	456	455	3	20.0
454	Setto	484	485	457	456	3	20.0
455	Setto	486	488	401	400	3	20.0
456	Setto	487	489	439	438	3	20.0
457	Setto	451	457	485	490	3	20.0
458	Setto	488	491	402	401	3	20.0
459	Setto	491	492	403	402	3	20.0
460	Setto	489	493	440	439	3	20.0
461	Setto	449	451	490	495	3	20.0
462	Setto	492	494	404	403	3	20.0
463	Setto	494	496	405	404	3	20.0
464	Setto	493	497	441	440	3	20.0
465	Setto	496	498	406	405	3	20.0
466	Setto	497	499	442	441	3	20.0
467	Setto	447	449	495	501	3	20.0
468	Setto	498	500	407	406	3	20.0
469	Setto	500	502	408	407	3	20.0
470	Setto	499	503	443	442	3	20.0
471	Setto	502	504	409	408	3	20.0
472	Setto	443	447	501	503	3	20.0
473	Setto	504	505	410	409	3	20.0
474	Setto	503	506	444	443	3	20.0
475	Setto	505	507	411	410	3	20.0
476	Setto	507	508	412	411	3	20.0
477	Setto	508	509	413	412	3	20.0
478	Setto	506	520	445	444	3	20.0
479	Setto	509	510	414	413	3	20.0
480	Setto	414	416	511	510	3	20.0
481	Setto	416	418	512	511	3	20.0
482	Setto	418	419	513	512	3	20.0
483	Setto	419	420	514	513	3	20.0
484	Setto	420	421	515	514	3	20.0
485	Setto	421	422	516	515	3	20.0
486	Setto	422	424	517	516	3	20.0
487	Setto	424	426	518	517	3	20.0
488	Setto	426	428	519	518	3	20.0
489	Setto	428	445	520	519	3	20.0
490	Setto	701	702	459	458	3	20.0
491	Setto	702	703	460	459	3	20.0
492	Setto	703	704	461	460	3	20.0

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493	Setto	700	701	458	475	3	20.0
494	Setto	704	705	462	461	3	20.0
495	Setto	705	706	463	462	3	20.0
496	Setto	706	707	464	463	3	20.0
497	Setto	521	522	486	465	3	20.0
498	Setto	465	466	537	521	3	20.0
499	Setto	466	467	555	537	3	20.0
500	Setto	467	468	573	555	3	20.0
501	Setto	468	469	591	573	3	20.0
502	Setto	469	470	609	591	3	20.0
503	Setto	470	471	627	609	3	20.0
504	Setto	471	472	645	627	3	20.0
505	Setto	472	473	663	645	3	20.0
506	Setto	473	474	681	663	3	20.0
507	Setto	474	475	700	681	3	20.0
508	Setto	707	708	476	464	3	20.0
509	Setto	708	709	487	476	3	20.0
510	Setto	476	477	717	708	3	20.0
511	Setto	477	478	724	717	3	20.0
512	Setto	478	479	730	724	3	20.0
513	Setto	479	480	736	730	3	20.0
514	Setto	736	737	481	480	3	20.0
515	Setto	737	738	482	481	3	20.0
516	Setto	738	739	483	482	3	20.0
517	Setto	739	740	484	483	3	20.0
518	Setto	740	741	485	484	3	20.0
519	Setto	522	523	488	486	3	20.0
520	Setto	709	710	489	487	3	20.0
521	Setto	490	485	741	735	3	20.0
522	Setto	523	524	491	488	3	20.0
523	Setto	524	525	492	491	3	20.0
524	Setto	710	711	493	489	3	20.0
525	Setto	495	490	735	729	3	20.0
526	Setto	525	526	494	492	3	20.0
527	Setto	526	527	496	494	3	20.0
528	Setto	711	712	497	493	3	20.0
529	Setto	527	528	498	496	3	20.0
530	Setto	712	713	499	497	3	20.0
531	Setto	501	495	729	723	3	20.0
532	Setto	528	529	500	498	3	20.0
533	Setto	529	530	502	500	3	20.0
534	Setto	713	714	503	499	3	20.0
535	Setto	530	531	504	502	3	20.0
536	Setto	503	501	723	714	3	20.0
537	Setto	531	532	505	504	3	20.0
538	Setto	714	715	506	503	3	20.0
539	Setto	532	533	507	505	3	20.0
540	Setto	533	534	508	507	3	20.0
541	Setto	534	535	509	508	3	20.0
542	Setto	715	716	520	506	3	20.0
543	Setto	535	536	510	509	3	20.0
544	Setto	510	511	554	536	3	20.0
545	Setto	511	512	572	554	3	20.0
546	Setto	512	513	590	572	3	20.0
547	Setto	513	514	608	590	3	20.0
548	Setto	514	515	626	608	3	20.0
549	Setto	515	516	644	626	3	20.0
550	Setto	516	517	662	644	3	20.0
551	Setto	517	518	680	662	3	20.0
552	Setto	518	519	699	680	3	20.0
553	Setto	519	520	716	699	3	20.0
554	Guscio	529	530	547		3	30.0
555	Guscio	521	522	538	537	3	30.0
556	Guscio	522	523	540	539	3	30.0
557	Guscio	523	524	541	540	3	30.0
558	Guscio	524	525	542	541	3	30.0
559	Guscio	525	526	543	542	3	30.0
560	Guscio	526	527	544	543	3	30.0
561	Guscio	527	528	546	545	3	30.0
562	Guscio	528	529	547	546	3	30.0
563	Guscio	530	531	548	547	3	30.0
564	Guscio	531	532	550	549	3	30.0
565	Guscio	532	533	551	550	3	30.0
566	Guscio	533	534	552	551	3	30.0
567	Guscio	534	535	553	552	3	30.0
568	Guscio	535	536	554	553	3	30.0
569	Guscio	538	522	539		3	30.0
570	Guscio	544	527	545		3	30.0
571	Guscio	548	531	549		3	30.0

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572	Guscio	537	538	556	555	3	30.0
573	Guscio	538	539	557	556	3	30.0
574	Guscio	539	540	558	557	3	30.0
575	Guscio	540	541	559	558	3	30.0
576	Guscio	541	542	560	559	3	30.0
577	Guscio	542	543	561	560	3	30.0
578	Guscio	543	544	562	561	3	30.0
579	Guscio	544	545	563	562	3	30.0
580	Guscio	545	546	564	563	3	30.0
581	Guscio	546	547	565	564	3	30.0
582	Guscio	547	548	566	565	3	30.0
583	Guscio	548	549	567	566	3	30.0
584	Guscio	549	550	568	567	3	30.0
585	Guscio	550	551	569	568	3	30.0
586	Guscio	551	552	570	569	3	30.0
587	Guscio	552	553	571	570	3	30.0
588	Guscio	553	554	572	571	3	30.0
589	Guscio	555	556	574	573	3	30.0
590	Guscio	556	557	575	574	3	30.0
591	Guscio	557	558	576	575	3	30.0
592	Guscio	558	559	577	576	3	30.0
593	Guscio	559	560	578	577	3	30.0
594	Guscio	560	561	579	578	3	30.0
595	Guscio	561	562	580	579	3	30.0
596	Guscio	562	563	581	580	3	30.0
597	Guscio	563	564	582	581	3	30.0
598	Guscio	564	565	583	582	3	30.0
599	Guscio	565	566	584	583	3	30.0
600	Guscio	566	567	585	584	3	30.0
601	Guscio	567	568	586	585	3	30.0
602	Guscio	568	569	587	586	3	30.0
603	Guscio	569	570	588	587	3	30.0
604	Guscio	570	571	589	588	3	30.0
605	Guscio	571	572	590	589	3	30.0
606	Guscio	573	574	592	591	3	30.0
607	Guscio	574	575	593	592	3	30.0
608	Guscio	575	576	594	593	3	30.0
609	Guscio	576	577	595	594	3	30.0
610	Guscio	577	578	596	595	3	30.0
611	Guscio	578	579	597	596	3	30.0
612	Guscio	579	580	598	597	3	30.0
613	Guscio	580	581	599	598	3	30.0
614	Guscio	581	582	600	599	3	30.0
615	Guscio	582	583	601	600	3	30.0
616	Guscio	583	584	602	601	3	30.0
617	Guscio	584	585	603	602	3	30.0
618	Guscio	585	586	604	603	3	30.0
619	Guscio	586	587	605	604	3	30.0
620	Guscio	587	588	606	605	3	30.0
621	Guscio	588	589	607	606	3	30.0
622	Guscio	589	590	608	607	3	30.0
623	Guscio	591	592	610	609	3	30.0
624	Guscio	592	593	611	610	3	30.0
625	Guscio	593	594	612	611	3	30.0
626	Guscio	594	595	613	612	3	30.0
627	Guscio	595	596	614	613	3	30.0
628	Guscio	596	597	615	614	3	30.0
629	Guscio	597	598	616	615	3	30.0
630	Guscio	598	599	617	616	3	30.0
631	Guscio	599	600	618	617	3	30.0
632	Guscio	600	601	619	618	3	30.0
633	Guscio	601	602	620	619	3	30.0
634	Guscio	602	603	621	620	3	30.0
635	Guscio	603	604	622	621	3	30.0
636	Guscio	604	605	623	622	3	30.0
637	Guscio	605	606	624	623	3	30.0
638	Guscio	606	607	625	624	3	30.0
639	Guscio	607	608	626	625	3	30.0
640	Guscio	609	610	628	627	3	30.0
641	Guscio	610	611	629	628	3	30.0
642	Guscio	611	612	630	629	3	30.0
643	Guscio	612	613	631	630	3	30.0
644	Guscio	613	614	632	631	3	30.0
645	Guscio	614	615	633	632	3	30.0
646	Guscio	615	616	634	633	3	30.0
647	Guscio	616	617	635	634	3	30.0
648	Guscio	617	618	636	635	3	30.0
649	Guscio	618	619	637	636	3	30.0
650	Guscio	619	620	638	637	3	30.0

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651	Guscio	620	621	639	638	3	30.0
652	Guscio	621	622	640	639	3	30.0
653	Guscio	622	623	641	640	3	30.0
654	Guscio	623	624	642	641	3	30.0
655	Guscio	624	625	643	642	3	30.0
656	Guscio	625	626	644	643	3	30.0
657	Guscio	627	628	646	645	3	30.0
658	Guscio	628	629	647	646	11	1.0
659	Guscio	629	630	648	647	11	1.0
660	Guscio	630	631	649	648	3	30.0
661	Guscio	631	632	650	649	3	30.0
662	Guscio	632	633	651	650	3	30.0
663	Guscio	633	634	652	651	3	30.0
664	Guscio	634	635	653	652	11	1.0
665	Guscio	635	636	654	653	11	1.0
666	Guscio	636	637	655	654	11	1.0
667	Guscio	637	638	656	655	11	1.0
668	Guscio	638	639	657	656	3	30.0
669	Guscio	639	640	658	657	3	30.0
670	Guscio	640	641	659	658	3	30.0
671	Guscio	641	642	660	659	3	30.0
672	Guscio	642	643	661	660	3	30.0
673	Guscio	643	644	662	661	3	30.0
674	Guscio	645	646	664	663	3	30.0
675	Guscio	646	647	665	664	11	1.0
676	Guscio	647	648	666	665	11	1.0
677	Guscio	648	649	667	666	3	30.0
678	Guscio	649	650	668	667	3	30.0
679	Guscio	650	651	669	668	3	30.0
680	Guscio	651	652	670	669	3	30.0
681	Guscio	652	653	671	670	11	1.0
682	Guscio	653	654	672	671	11	1.0
683	Guscio	654	655	673	672	11	1.0
684	Guscio	655	656	674	673	11	1.0
685	Guscio	656	657	675	674	3	30.0
686	Guscio	657	658	676	675	3	30.0
687	Guscio	658	659	677	676	3	30.0
688	Guscio	659	660	678	677	3	30.0
689	Guscio	660	661	679	678	3	30.0
690	Guscio	661	662	680	679	3	30.0
691	Guscio	670	671	689		11	1.0
692	Guscio	663	664	682	681	3	30.0
693	Guscio	664	665	683	682	11	1.0
694	Guscio	665	666	684	683	11	1.0
695	Guscio	666	667	685	684	3	30.0
696	Guscio	667	668	686	685	3	30.0
697	Guscio	668	669	687	686	3	30.0
698	Guscio	669	670	688	687	3	30.0
699	Guscio	671	672	691	690	11	1.0
700	Guscio	672	673	692	691	11	1.0
701	Guscio	673	674	693	692	11	1.0
702	Guscio	674	675	694	693	3	30.0
703	Guscio	675	676	695	694	3	30.0
704	Guscio	676	677	696	695	3	30.0
705	Guscio	677	678	697	696	3	30.0
706	Guscio	678	679	698	697	3	30.0
707	Guscio	679	680	699	698	3	30.0
708	Guscio	688	670	689		11	1.0
709	Guscio	689	671	690		11	1.0
710	Guscio	681	682	700		3	30.0
711	Guscio	688	689	706		3	30.0
712	Guscio	682	683	701	700	3	30.0
713	Guscio	683	684	702	701	3	30.0
714	Guscio	684	685	703	702	3	30.0
715	Guscio	685	686	704	703	3	30.0
716	Guscio	686	687	705	704	3	30.0
717	Guscio	687	688	706	705	3	30.0
718	Guscio	689	690	707	706	3	30.0
719	Guscio	690	691	708	707	3	30.0
720	Guscio	691	692	709	708	3	30.0
721	Guscio	692	693	710	709	3	30.0
722	Guscio	693	694	711	710	3	30.0
723	Guscio	694	695	712	711	3	30.0
724	Guscio	695	696	713	712	3	30.0
725	Guscio	696	697	714	713	3	30.0
726	Guscio	697	698	715	714	3	30.0
727	Guscio	698	699	716	715	3	30.0
728	Guscio	708	709	718	717	3	30.0
729	Guscio	709	710	719	718	3	30.0

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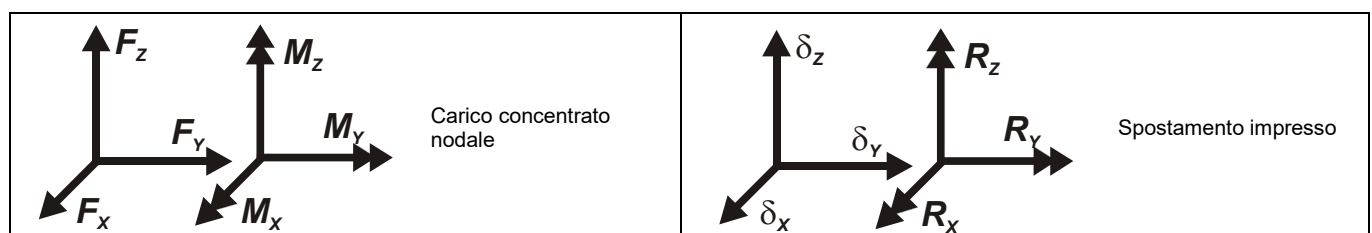
730	Guscio	710	711	720	719	3	30.0
731	Guscio	711	712	721	720	3	30.0
732	Guscio	712	713	722	721	3	30.0
733	Guscio	713	714	723	722	3	30.0
734	Guscio	720	721	727		11	1.0
735	Guscio	717	718	725	724	3	30.0
736	Guscio	718	719	726	725	11	1.0
737	Guscio	719	720	727	726	11	1.0
738	Guscio	721	722	728	727	3	30.0
739	Guscio	722	723	729	728	3	30.0
740	Guscio	724	725	731	730	3	30.0
741	Guscio	725	726	732	731	11	1.0
742	Guscio	726	727	733	732	11	1.0
743	Guscio	727	728	734	733	3	30.0
744	Guscio	728	729	735	734	3	30.0
745	Guscio	730	731	737	736	3	30.0
746	Guscio	731	732	738	737	3	30.0
747	Guscio	732	733	739	738	3	30.0
748	Guscio	733	734	740	739	3	30.0
749	Guscio	734	735	741	740	3	30.0

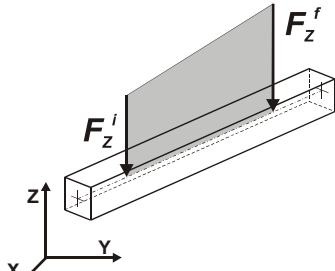
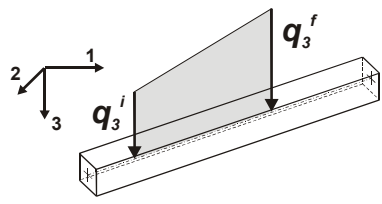
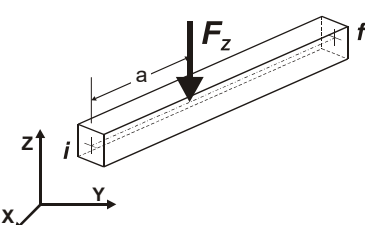
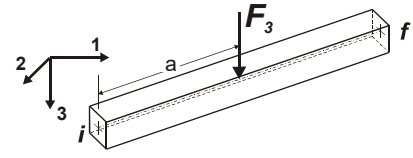
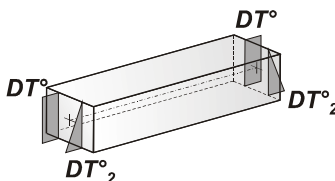
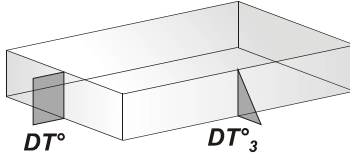
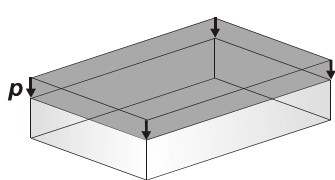
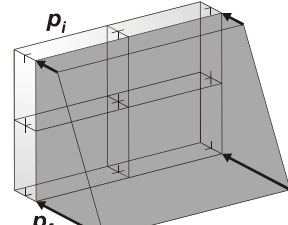
MODELLAZIONE DELLE AZIONI

LEGENDA TABELLA DATI AZIONI

Il programma consente l'uso di diverse tipologie di carico (azioni). Le azioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni azione applicata alla struttura viene di riportato il codice, il tipo e la sigla identificativa. Le tabelle successive dettagliano i valori caratteristici di ogni azione in relazione al tipo. Le tabelle riportano infatti i seguenti dati in relazione al tipo:

1	carico concentrato nodale 6 dati (forza F_x , F_y , F_z , momento M_x , M_y , M_z)
2	spostamento nodale impresso 6 dati (spostamento T_x , T_y , T_z , rotazione R_x , R_y , R_z)
3	carico distribuito globale su elemento tipo trave 7 dati (f_x , f_y , f_z , m_x , m_y , m_z , ascissa di inizio carico) 7 dati (f_x , f_y , f_z , m_x , m_y , m_z , ascissa di fine carico)
4	carico distribuito locale su elemento tipo trave 7 dati (f_1 , f_2 , f_3 , m_1 , m_2 , m_3 , ascissa di inizio carico) 7 dati (f_1 , f_2 , f_3 , m_1 , m_2 , m_3 , ascissa di fine carico)
5	carico concentrato globale su elemento tipo trave 7 dati (F_x , F_y , F_z , M_x , M_y , M_z , ascissa di carico)
6	carico concentrato locale su elemento tipo trave 7 dati (F_1 , F_2 , F_3 , M_1 , M_2 , M_3 , ascissa di carico)
7	variazione termica applicata ad elemento tipo trave 7 dati (variazioni termiche: uniforme, media e differenza in altezza e larghezza al nodo iniziale e finale)
8	carico di pressione uniforme su elemento tipo piastra 1 dato (pressione)
9	carico di pressione variabile su elemento tipo piastra 4 dati (pressione, quota, pressione, quota)
10	variazione termica applicata ad elemento tipo piastra 2 dati (variazioni termiche: media e differenza nello spessore)
11	carico variabile generale su elementi tipo trave e piastra 1 dato descrizione della tipologia 4 dati per segmento (posizione, valore, posizione, valore) la tipologia precisa l'ascissa di definizione, la direzione del carico, la modalità di carico e la larghezza d'influenza per gli elementi tipo trave
12	gruppo di carichi con impronta su piastra 9 dati (numero di ripetizioni in direzione X e Y, valore di ciascun carico, posizione centrale del primo, dimensioni dell'impronta, interasse tra i carichi)



 Carico distribuito globale	 Carico distribuito locale
 Carico concentrato globale	 Carico concentrato locale
 Carico termico 2D	 Carico termico 3D
 Carico pressione uniforme	 Carico pressione variabile

Tipo	carico di pressione uniforme su piastra	
Id	Tipo	pressione
		daN/ m2
5	Platea Gk2-Acqua-P3:p=0.25	2500.00
6	Platea Qk - Manutenzione-P3:p= 2.000e-02	200.00
10	Sagomatura in cls-P3:p= 3.750e-02	375.00

Tipo	carico di pressione variabile su piastra				
Id	Tipo	pressione	quota	pressione	quota
		daN/ m2	m	daN/ m2	m
1	Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00	0.0	0.0	4597.00	-3.10
2	Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00	0.0	0.0	-4597.00	-3.10

Tipo	carico variabile generale				
Id	Tipo	ascissa	valore	ascissa	valore
		m	daN/ m2	m	daN/ m2
8	Sovraccarico-QV:var x - Qz - Area				
	X - X Qz Area L2=0.0	-100.00	-2500.00	100.00	-2500.00
9	Strada-QV:var x - Qz - Area				
	X - X Qz Area L2=0.0	-100.00	-500.00	100.00	-500.00

SCHEMATIZZAZIONE DEI CASI DI CARICO

LEGENDA TABELLA CASI DI CARICO

Il programma consente l'applicazione di diverse tipologie di casi di carico.

Sono previsti i seguenti 11 tipi di casi di carico:

	Sigla	Tipo	Descrizione
1	Ggk	A	caso di carico comprensivo del peso proprio struttura
2	Gk	NA	caso di carico con azioni permanenti
3	Qk	NA	caso di carico con azioni variabili
4	Gsk	A	caso di carico comprensivo dei carichi permanenti sui solai e sulle coperture
5	Qsk	A	caso di carico comprensivo dei carichi variabili sui solai
6	Qnk	A	caso di carico comprensivo dei carichi di neve sulle coperture
7	Qtk	SA	caso di carico comprensivo di una variazione termica agente sulla struttura
8	Qvk	NA	caso di carico comprensivo di azioni da vento sulla struttura
9	Esk	SA	caso di carico sismico con analisi statica equivalente
10	Edk	SA	caso di carico sismico con analisi dinamica
11	Etk	NA	caso di carico comprensivo di azioni derivanti dall' incremento di spinta delle terre in condizione sismica
12	Pk	NA	caso di carico comprensivo di azioni derivanti da coazioni, cedimenti e precompressioni

Sono di tipo automatico A (ossia non prevedono introduzione dati da parte dell'utente) i seguenti casi di carico: 1-Ggk; 4-Gsk; 5-Qsk; 6-Qnk.

Sono di tipo semi-automatico SA (ossia prevedono una minima introduzione dati da parte dell'utente) i seguenti casi di carico:

7-Qtk, in quanto richiede solo il valore della variazione termica;

9-Esk e 10-Edk, in quanto richiedono il valore dell'angolo di ingresso del sisma e l'individuazione dei casi di carico partecipanti alla definizione delle masse.

Sono di tipo non automatico NA ossia prevedono la diretta applicazione di carichi generici agli elementi strutturali (si veda il precedente punto Modellazione delle Azioni) i restanti casi di carico.

Nella tabella successiva vengono riportati i casi di carico agenti sulla struttura, con l'indicazione dei dati relativi al caso di carico stesso:

Numero Tipo e Sigla identificativa, Valore di riferimento del caso di carico (se previsto).

In successione, per i casi di carico non automatici, viene riportato l'elenco di nodi ed elementi direttamente caricati con la sigla identificativa del carico.

Per i casi di carico di tipo sismico (9-Esk e 10-Edk), viene riportata la tabella di definizione delle masse: per ogni caso di carico partecipante alla definizione delle masse viene indicata la relativa aliquota (partecipazione) considerata. Si precisa che per i caso di carico 5-Qsk e 6-Qnk la partecipazione è prevista localmente per ogni elemento solaio o copertura presente nel modello (si confronti il valore Sksol nel capitolo relativo agli elementi solaio) e pertanto la loro partecipazione è di norma pari a uno.

CDC	Tipo	Sigla Id	Note
1	Ggk	CDC=Ggk (peso proprio della struttura)	
2	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)	partecipazione:1.00 per 1 CDC=Ggk (peso proprio della struttura)
3	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)	come precedente CDC sismico
4	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)	come precedente CDC sismico
5	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)	come precedente CDC sismico
6	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. +)	come precedente CDC sismico
7	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -)	come precedente CDC sismico
8	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +)	come precedente CDC sismico
9	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -)	come precedente CDC sismico
10	Gk	Spinta terreno	D3 :da 4 a 5 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
			D3 :da 6 a 7 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 : 9 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
			D3 :da 10 a 11 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 16 a 17 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 : 19 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
			D3 :da 20 a 21 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00

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CDC	Tipo	Sigla Id	Note
			D3 :da 22 a 26 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
			D3 : 31 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
			D3 : 54 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
			D3 :da 57 a 58 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 59 a 60 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
			D3 : 67 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 110 a 114 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 : 120 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 121 a 128 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
			D3 :da 129 a 131 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 133 a 138 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 141 a 144 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 146 a 151 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 154 a 157 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 159 a 164 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 167 a 170 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 172 a 177 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 180 a 183 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 185 a 190 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 : 193 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 194 a 205 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
			D3 :da 206 a 225 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 229 a 294 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
			D3 :da 295 a 299 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 308 a 362 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 363 a 377 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
			D3 : 411 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
			D3 :da 561 a 574 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 577 a 590 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
			D3 :da 598 a 604 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 613 a 619 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 636 a 642 Azione : Spinta terreno - (Strato 1)-PL3:pi=0.0 qi=0.0 pf=-0.46 qf=-310.00
			D3 :da 723 a 728 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
			D3 :da 738 a 744 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
			D3 :da 773 a 783 Azione : Spinta terreno + (Strato 1)-PL3:pi=0.0 qi=0.0 pf=0.46 qf=-310.00
11	Gk	Platea Gk - Acqua+Pompe	D3 : 8 Azione : Platea Gk2-Acqua-P3:p=0.25
			D3 : 12 Azione : Platea Gk2-Acqua-P3:p=0.25
			D3 : 15 Azione : Platea Gk2-Acqua-P3:p=0.25
			D3 :da 55 a 56 Azione : Platea Gk2-Acqua-P3:p=0.25
			D3 :da 61 a 62 Azione : Platea Gk2-Acqua-P3:p=0.25
			D3 :da 68 a 109 Azione : Platea Gk2-Acqua-P3:p=0.25
			D3 :da 414 a 485 Azione : Platea Gk2-Acqua-P3:p=0.25
			D3 :da 575 a 576 Azione : Platea Gk2-Acqua-P3:p=0.25
			D3 :da 594 a 597 Azione : Platea Gk2-Acqua-P3:p=0.25
			D3 :da 620 a 622 Azione : Platea Gk2-Acqua-P3:p=0.25
			D3 :da 630 a 635 Azione : Platea Gk2-Acqua-P3:p=0.25
			D3 :da 650 a 652 Azione : Platea Gk2-Acqua-P3:p=0.25
			D3 :da 729 a 737 Azione : Platea Gk2-Acqua-P3:p=0.25

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CDC	Tipo	Sigla Id	Note
			D3 :da 745 a 751 Azione : Platea Gk2-Acqua-P3:p=0.25
			D3 :da 753 a 772 Azione : Platea Gk2-Acqua-P3:p=0.25
12	Qk	Platea Qk-Manutenzione	D3 : 8 Azione : Platea Qk - Manutenzione-P3:p= 2.000e-02
			D3 : 12 Azione : Platea Qk - Manutenzione-P3:p= 2.000e-02
			D3 : 15 Azione : Platea Qk - Manutenzione-P3:p= 2.000e-02
			D3 :da 55 a 56 Azione : Platea Qk - Manutenzione-P3:p= 2.000e-02
			D3 :da 61 a 62 Azione : Platea Qk - Manutenzione-P3:p= 2.000e-02
			D3 :da 68 a 109 Azione : Platea Qk - Manutenzione-P3:p= 2.000e-02
			D3 :da 414 a 485 Azione : Platea Qk - Manutenzione-P3:p= 2.000e-02
			D3 :da 575 a 576 Azione : Platea Qk - Manutenzione-P3:p= 2.000e-02
			D3 :da 594 a 597 Azione : Platea Qk - Manutenzione-P3:p= 2.000e-02
			D3 :da 620 a 622 Azione : Platea Qk - Manutenzione-P3:p= 2.000e-02
			D3 :da 630 a 635 Azione : Platea Qk - Manutenzione-P3:p= 2.000e-02
			D3 :da 650 a 652 Azione : Platea Qk - Manutenzione-P3:p= 2.000e-02
			D3 :da 729 a 737 Azione : Platea Qk - Manutenzione-P3:p= 2.000e-02
			D3 :da 745 a 751 Azione : Platea Qk - Manutenzione-P3:p= 2.000e-02
			D3 :da 753 a 772 Azione : Platea Qk - Manutenzione-P3:p= 2.000e-02
13	Gk	Strada Gk	D3 :da 1 a 3 Azione : Strada-QV:var x - Qz - Area
			D3 :da 27 a 30 Azione : Strada-QV:var x - Qz - Area
			D3 :da 32 a 53 Azione : Strada-QV:var x - Qz - Area
			D3 :da 63 a 66 Azione : Strada-QV:var x - Qz - Area
			D3 :da 226 a 228 Azione : Strada-QV:var x - Qz - Area
			D3 :da 300 a 307 Azione : Strada-QV:var x - Qz - Area
			D3 :da 378 a 410 Azione : Strada-QV:var x - Qz - Area
			D3 : 412 Azione : Strada-QV:var x - Qz - Area
			D3 :da 486 a 560 Azione : Strada-QV:var x - Qz - Area
			D3 :da 591 a 593 Azione : Strada-QV:var x - Qz - Area
			D3 : 612 Azione : Strada-QV:var x - Qz - Area
			D3 :da 653 a 654 Azione : Strada-QV:var x - Qz - Area
			D3 :da 714 a 722 Azione : Strada-QV:var x - Qz - Area
			D3 : 752 Azione : Strada-QV:var x - Qz - Area
			D3 : 784 Azione : Strada-QV:var x - Qz - Area
14	Qk	Sovraccarico Qk	D3 :da 1 a 3 Azione : Sovraccarico-QV:var x - Qz - Area
			D3 :da 27 a 30 Azione : Sovraccarico-QV:var x - Qz - Area
			D3 :da 32 a 53 Azione : Sovraccarico-QV:var x - Qz - Area
			D3 :da 63 a 66 Azione : Sovraccarico-QV:var x - Qz - Area
			D3 :da 226 a 228 Azione : Sovraccarico-QV:var x - Qz - Area
			D3 :da 300 a 307 Azione : Sovraccarico-QV:var x - Qz - Area
			D3 :da 378 a 410 Azione : Sovraccarico-QV:var x - Qz - Area
			D3 : 412 Azione : Sovraccarico-QV:var x - Qz - Area
			D3 :da 486 a 560 Azione : Sovraccarico-QV:var x - Qz - Area
			D3 :da 591 a 593 Azione : Sovraccarico-QV:var x - Qz - Area
			D3 : 612 Azione : Sovraccarico-QV:var x - Qz - Area
			D3 :da 653 a 654 Azione : Sovraccarico-QV:var x - Qz - Area
			D3 :da 714 a 722 Azione : Sovraccarico-QV:var x - Qz - Area
			D3 : 752 Azione : Sovraccarico-QV:var x - Qz - Area
			D3 : 784 Azione : Sovraccarico-QV:var x - Qz - Area
15	Gk	Gk1-Sagomatura cls	D3 : 8 Azione : Sagomatura in cls-P3:p= 3.750e-02
			D3 : 12 Azione : Sagomatura in cls-P3:p= 3.750e-02
			D3 : 15 Azione : Sagomatura in cls-P3:p= 3.750e-02
			D3 :da 55 a 56 Azione : Sagomatura in cls-P3:p= 3.750e-02
			D3 :da 61 a 62 Azione : Sagomatura in cls-P3:p= 3.750e-02
			D3 :da 68 a 109 Azione : Sagomatura in cls-P3:p= 3.750e-02
			D3 :da 414 a 485 Azione : Sagomatura in cls-P3:p= 3.750e-02
			D3 :da 575 a 576 Azione : Sagomatura in cls-P3:p= 3.750e-02
			D3 :da 594 a 597 Azione : Sagomatura in cls-P3:p= 3.750e-02
			D3 :da 620 a 622 Azione : Sagomatura in cls-P3:p= 3.750e-02
			D3 :da 630 a 635 Azione : Sagomatura in cls-P3:p= 3.750e-02
			D3 :da 650 a 652 Azione : Sagomatura in cls-P3:p= 3.750e-02
			D3 :da 729 a 737 Azione : Sagomatura in cls-P3:p= 3.750e-02
			D3 :da 745 a 751 Azione : Sagomatura in cls-P3:p= 3.750e-02
			D3 :da 753 a 772 Azione : Sagomatura in cls-P3:p= 3.750e-02

DEFINIZIONE DELLE COMBINAZIONI

LEGENDA TABELLA COMBINAZIONI DI CARICO

Il programma combina i diversi tipi di casi di carico (CDC) secondo le regole previste dalla normativa vigente. Le combinazioni previste sono destinate al controllo di sicurezza della struttura ed alla verifica

degli spostamenti e delle sollecitazioni. La prima tabella delle combinazioni riportata di seguito comprende le seguenti informazioni: Numero, Tipo, Sigla identificativa. Una seconda tabella riporta il peso nella combinazione assunto per ogni caso di carico.

Ai fini delle verifiche degli stati limite si definiscono le seguenti combinazioni delle azioni:

Combinazione fondamentale SLU

$$\gamma_{G1} \cdot G_1 + \gamma_{G2} \cdot G_2 + \gamma_P \cdot P + \gamma_{Q1} \cdot Q_{k1} + \gamma_{Q2} \cdot \psi_{02} \cdot Q_{k2} + \gamma_{Q3} \cdot \psi_{03} \cdot Q_{k3} + \dots$$

Combinazione caratteristica (rara) SLE

$$G_1 + G_2 + P + Q_{k1} + \psi_{02} \cdot Q_{k2} + \psi_{03} \cdot Q_{k3} + \dots$$

Combinazione frequente SLE

$$G_1 + G_2 + P + \psi_{11} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$$

Combinazione quasi permanente SLE

$$G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$$

Combinazione sismica, impiegata per gli stati limite ultimi e di esercizio connessi all'azione sismica E
 $E + G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$

Combinazione eccezionale, impiegata per gli stati limite connessi alle azioni eccezionali

$$G_1 + G_2 + A_d + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$$

Dove:

NTC 2018 Tabella 2.5.I

Destinazione d'uso/azione	ψ_0	ψ_1	ψ_2
Categoria A residenziali	0,70	0,50	0,30
Categoria B uffici	0,70	0,50	0,30
Categoria C ambienti suscettibili di affollamento	0,70	0,70	0,60
Categoria D ambienti ad uso commerciale	0,70	0,70	0,60
Categoria E biblioteche, archivi, magazzini,...	1,00	0,90	0,80
Categoria F Rimesse e parcheggi (autoveicoli ≤ 30 kN)	0,70	0,70	0,60
Categoria G Rimesse e parcheggi (autoveicoli > 30 kN)	0,70	0,50	0,30
Categoria H Coperture	0,00	0,00	0,00
Vento	0,60	0,20	0,00
Neve a quota ≤ 1000 m	0,50	0,20	0,00
Neve a quota > 1000 m	0,70	0,50	0,20
Variazioni Termiche	0,60	0,50	0,00

Nelle verifiche possono essere adottati in alternativa due diversi approcci progettuali:

- per l'approccio 1 si considerano due diverse combinazioni di gruppi di coefficienti di sicurezza parziali per le azioni, per i materiali e per la resistenza globale (combinazione 1 con coefficienti A1 e combinazione 2 con coefficienti A2),
- per l'approccio 2 si definisce un'unica combinazione per le azioni, per la resistenza dei materiali e per la resistenza globale (con coefficienti A1).

NTC 2018 Tabella 2.6.I

		Coefficiente γ_f	EQU	A1	A2
Carichi permanenti	Favorevoli	γ_{G1}	0,9	1,0	1,0
	Sfavorevoli		1,1	1,3	1,0
Carichi permanenti non strutturali (Non compiutamente definiti)	Favorevoli	γ_{G2}	0,8	0,8	0,8
	Sfavorevoli		1,5	1,5	1,3
Carichi variabili	Favorevoli	γ_{Qi}	0,0	0,0	0,0
	Sfavorevoli		1,5	1,5	1,3

Cmb	Tipo	Sigla Id	effetto P-delta
1	SLU	Comb. SLU A1 1	
2	SLU	Comb. SLU A1 2	
3	SLU	Comb. SLU A1 3	
4	SLU	Comb. SLU A1 4	
5	SLU	Comb. SLU A1 5	
6	SLU	Comb. SLU A1 6	
7	SLU	Comb. SLU A1 7	
8	SLU	Comb. SLU A1 8	
9	SLU	Comb. SLU A1 (SLV sism.) 9	
10	SLU	Comb. SLU A1 (SLV sism.) 10	
11	SLU	Comb. SLU A1 (SLV sism.) 11	
12	SLU	Comb. SLU A1 (SLV sism.) 12	
13	SLU	Comb. SLU A1 (SLV sism.) 13	
14	SLU	Comb. SLU A1 (SLV sism.) 14	
15	SLU	Comb. SLU A1 (SLV sism.) 15	
16	SLU	Comb. SLU A1 (SLV sism.) 16	
17	SLU	Comb. SLU A1 (SLV sism.) 17	
18	SLU	Comb. SLU A1 (SLV sism.) 18	
19	SLU	Comb. SLU A1 (SLV sism.) 19	
20	SLU	Comb. SLU A1 (SLV sism.) 20	
21	SLU	Comb. SLU A1 (SLV sism.) 21	
22	SLU	Comb. SLU A1 (SLV sism.) 22	
23	SLU	Comb. SLU A1 (SLV sism.) 23	
24	SLU	Comb. SLU A1 (SLV sism.) 24	
25	SLU	Comb. SLU A1 (SLV sism.) 25	
26	SLU	Comb. SLU A1 (SLV sism.) 26	
27	SLU	Comb. SLU A1 (SLV sism.) 27	
28	SLU	Comb. SLU A1 (SLV sism.) 28	
29	SLU	Comb. SLU A1 (SLV sism.) 29	
30	SLU	Comb. SLU A1 (SLV sism.) 30	
31	SLU	Comb. SLU A1 (SLV sism.) 31	
32	SLU	Comb. SLU A1 (SLV sism.) 32	
33	SLU	Comb. SLU A1 (SLV sism.) 33	
34	SLU	Comb. SLU A1 (SLV sism.) 34	
35	SLU	Comb. SLU A1 (SLV sism.) 35	
36	SLU	Comb. SLU A1 (SLV sism.) 36	
37	SLU	Comb. SLU A1 (SLV sism.) 37	
38	SLU	Comb. SLU A1 (SLV sism.) 38	
39	SLU	Comb. SLU A1 (SLV sism.) 39	
40	SLU	Comb. SLU A1 (SLV sism.) 40	
41	SLD(sis)	Comb. SLE (SLD Danno sism.) 41	
42	SLD(sis)	Comb. SLE (SLD Danno sism.) 42	
43	SLD(sis)	Comb. SLE (SLD Danno sism.) 43	
44	SLD(sis)	Comb. SLE (SLD Danno sism.) 44	
45	SLD(sis)	Comb. SLE (SLD Danno sism.) 45	
46	SLD(sis)	Comb. SLE (SLD Danno sism.) 46	
47	SLD(sis)	Comb. SLE (SLD Danno sism.) 47	
48	SLD(sis)	Comb. SLE (SLD Danno sism.) 48	
49	SLD(sis)	Comb. SLE (SLD Danno sism.) 49	
50	SLD(sis)	Comb. SLE (SLD Danno sism.) 50	
51	SLD(sis)	Comb. SLE (SLD Danno sism.) 51	
52	SLD(sis)	Comb. SLE (SLD Danno sism.) 52	
53	SLD(sis)	Comb. SLE (SLD Danno sism.) 53	
54	SLD(sis)	Comb. SLE (SLD Danno sism.) 54	
55	SLD(sis)	Comb. SLE (SLD Danno sism.) 55	
56	SLD(sis)	Comb. SLE (SLD Danno sism.) 56	
57	SLD(sis)	Comb. SLE (SLD Danno sism.) 57	
58	SLD(sis)	Comb. SLE (SLD Danno sism.) 58	
59	SLD(sis)	Comb. SLE (SLD Danno sism.) 59	
60	SLD(sis)	Comb. SLE (SLD Danno sism.) 60	
61	SLD(sis)	Comb. SLE (SLD Danno sism.) 61	
62	SLD(sis)	Comb. SLE (SLD Danno sism.) 62	
63	SLD(sis)	Comb. SLE (SLD Danno sism.) 63	
64	SLD(sis)	Comb. SLE (SLD Danno sism.) 64	
65	SLD(sis)	Comb. SLE (SLD Danno sism.) 65	
66	SLD(sis)	Comb. SLE (SLD Danno sism.) 66	
67	SLD(sis)	Comb. SLE (SLD Danno sism.) 67	
68	SLD(sis)	Comb. SLE (SLD Danno sism.) 68	
69	SLD(sis)	Comb. SLE (SLD Danno sism.) 69	
70	SLD(sis)	Comb. SLE (SLD Danno sism.) 70	
71	SLD(sis)	Comb. SLE (SLD Danno sism.) 71	
72	SLD(sis)	Comb. SLE (SLD Danno sism.) 72	
73	SLE(r)	Comb. SLE(rara) 73	
74	SLE(r)	Comb. SLE(rara) 74	

SCARICATORE IN VIA PUCCI

Cmb	Tipo	Sigla Id	effetto P-delta
75	SLE(r)	Comb. SLE(rara) 75	
76	SLE(r)	Comb. SLE(rara) 76	

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
1	1.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.30	0.0
	1.30													
2	1.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.30	1.50	0.0	1.30	1.50
	1.30													
3	1.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.30	0.0
	1.30													
4	1.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.30	1.50	1.50	1.30	1.50
	1.30													
5	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.80	0.0	1.00	0.0
	1.00													
6	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.80	0.0	1.00	1.50
	1.00													
7	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.80	1.50	1.00	0.0
	1.00													
8	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.80	1.50	1.00	1.50
	1.00													
9	1.00	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
10	1.00	-1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
11	1.00	1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
12	1.00	1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
13	1.00	-1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
14	1.00	-1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
15	1.00	1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
16	1.00	1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
17	1.00	0.0	-1.00	-0.30	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
18	1.00	0.0	-1.00	0.30	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
19	1.00	0.0	1.00	-0.30	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
20	1.00	0.0	1.00	0.30	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
21	1.00	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
22	1.00	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
23	1.00	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
24	1.00	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
25	1.00	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
26	1.00	-0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
27	1.00	0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
28	1.00	0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
29	1.00	0.0	-0.30	-1.00	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
30	1.00	0.0	-0.30	1.00	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
31	1.00	0.0	0.30	-1.00	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
32	1.00	0.0	0.30	1.00	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
33	1.00	-0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
34	1.00	-0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
35	1.00	0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
36	1.00	0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
37	1.00	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
38	1.00	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
39	1.00	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
40	1.00	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
41	1.00	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
42	1.00	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
43	1.00	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
44	1.00	0.0	0.0	0.0	0.0	1.00	0.0	0.30	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
45	1.00	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	-0.30	1.00	1.00	0.80	1.00	0.80
	1.00													
46	1.00	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	0.30	1.00	1.00	0.80	1.00	0.80
	1.00													
47	1.00	0.0	0.0	0.0	0.0	1.00	0.0	0.0	-0.30	1.00	1.00	0.80	1.00	0.80
	1.00													
48	1.00	0.0	0.0	0.0	0.0	1.00	0.0	0.0	0.30	1.00	1.00	0.80	1.00	0.80
	1.00													
49	1.00	0.0	0.0	0.0	0.0	0.0	-1.00	-0.30	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
50	1.00	0.0	0.0	0.0	0.0	0.0	-1.00	0.30	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
51	1.00	0.0	0.0	0.0	0.0	0.0	1.00	-0.30	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
52	1.00	0.0	0.0	0.0	0.0	0.0	1.00	0.30	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
53	1.00	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	1.00	1.00	0.80	1.00	0.80
	1.00													
54	1.00	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	1.00	1.00	0.80	1.00	0.80
	1.00													
55	1.00	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	1.00	1.00	0.80	1.00	0.80
	1.00													
56	1.00	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30	1.00	1.00	0.80	1.00	0.80
	1.00													
57	1.00	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
58	1.00	0.0	0.0	0.0	0.0	-0.30	0.0	1.00	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
59	1.00	0.0	0.0	0.0	0.0	0.30	0.0	-1.00	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
60	1.00	0.0	0.0	0.0	0.0	0.30	0.0	1.00	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
61	1.00	0.0	0.0	0.0	0.0	0.0	-0.30	-1.00	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
62	1.00	0.0	0.0	0.0	0.0	0.0	-0.30	1.00	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
63	1.00	0.0	0.0	0.0	0.0	0.0	0.30	-1.00	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
64	1.00	0.0	0.0	0.0	0.0	0.0	0.30	1.00	0.0	1.00	1.00	0.80	1.00	0.80
	1.00													
65	1.00	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	-1.00	1.00	1.00	0.80	1.00	0.80
	1.00													
66	1.00	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	1.00	1.00	1.00	0.80	1.00	0.80
	1.00													
67	1.00	0.0	0.0	0.0	0.0	0.30	0.0	0.0	-1.00	1.00	1.00	0.80	1.00	0.80
	1.00													
68	1.00	0.0	0.0	0.0	0.0	0.30	0.0	0.0	1.00	1.00	1.00	0.80	1.00	0.80
	1.00													
69	1.00	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00	1.00	1.00	0.80	1.00	0.80
	1.00													
70	1.00	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00	1.00	1.00	0.80	1.00	0.80
	1.00													
71	1.00	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00	1.00	1.00	0.80	1.00	0.80
	1.00													
72	1.00	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00	1.00	1.00	0.80	1.00	0.80
	1.00													
73	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	0.0

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	1.00													
74	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	1.00	0.0	1.00	1.00
	1.00													
75	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	0.0
	1.00													
76	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	1.00	1.00	1.00	1.00
	1.00													

AZIONE SISMICA

VALUTAZIONE DELL' AZIONE SISMICA

L'azione sismica sulle costruzioni è valutata a partire dalla "pericolosità sismica di base", in condizioni ideali di sito di riferimento rigido con superficie topografica orizzontale. Allo stato attuale, la pericolosità sismica su reticolo di riferimento nell'intervallo di riferimento è fornita dai dati pubblicati sul sito <http://esse1.mi.ingv.it/>. Per punti non coincidenti con il reticolo di riferimento e periodi di ritorno non contemplati direttamente si opera come indicato nell' allegato alle NTC (rispettivamente media pesata e interpolazione). L' azione sismica viene definita in relazione ad un periodo di riferimento V_r che si ricava, per ciascun tipo di costruzione, moltiplicandone la vita nominale per il coefficiente d'uso (vedi tabella Parametri della struttura). Fissato il periodo di riferimento V_r e la probabilità di superamento P_{ver} associata a ciascuno degli stati limite considerati, si ottiene il periodo di ritorno T_r e i relativi parametri di pericolosità sismica (vedi tabella successiva):

a_g : accelerazione orizzontale massima del terreno;

F_o : valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale;

T^*c : periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale;

Parametri della struttura					
Classe d'uso	Vita V_n [anni]	Coeff. Uso	Periodo V_r [anni]	Tipo di suolo	Categoria topografica
III	50.0	1.5	75.0	B	T1

Individuati su reticolo di riferimento i parametri di pericolosità sismica si valutano i parametri spettrali riportati in tabella:

S è il coefficiente che tiene conto della categoria di sottosuolo e delle condizioni topografiche mediante la relazione seguente $S = S_s \cdot S_t$ (3.2.3)

F_o è il fattore che quantifica l'amplificazione spettrale massima, su sito di riferimento rigido orizzontale

F_v è il fattore che quantifica l'amplificazione spettrale massima verticale, in termini di accelerazione orizzontale massima del terreno a_g su sito di riferimento rigido orizzontale

T_b è il periodo corrispondente all'inizio del tratto dello spettro ad accelerazione costante.

T_c è il periodo corrispondente all'inizio del tratto dello spettro a velocità costante.

T_d è il periodo corrispondente all'inizio del tratto dello spettro a spostamento costante.

Id nodo	Longitudine	Latitudine	Distanza
			Km
Loc.	14.642	40.743	
33650	14.612	40.729	2.959
33651	14.678	40.729	3.398
33429	14.679	40.779	5.056
33428	14.613	40.779	4.674

SL	P_{ver}	T_r	a_g	F_o	T^*c
		Anni	g		sec
SLO	81.0	45.0	0.050	2.360	0.310
SLD	63.0	75.0	0.062	2.420	0.340
SLV	10.0	712.0	0.141	2.520	0.410
SLC	5.0	1462.0	0.174	2.560	0.430

SCARICATORE IN VIA PUCCI

SL	ag	S	Fo	Fv	Tb	Tc	Td
	g				sec	sec	sec
SLO	0.050	1.200	2.360	0.712	0.144	0.431	1.800
SLD	0.062	1.200	2.420	0.816	0.155	0.464	1.850
SLV	0.141	1.200	2.520	1.277	0.180	0.539	2.163
SLC	0.174	1.200	2.560	1.440	0.187	0.560	2.295

RISULTATI ANALISI SISMICHE

LEGENDA TABELLA ANALISI SISMICHE

Il programma consente l'analisi di diverse configurazioni sismiche.

Sono previsti, infatti, i seguenti casi di carico:

9. Esk caso di carico sismico con analisi statica equivalente

10. Edk caso di carico sismico con analisi dinamica

Ciascun caso di carico è caratterizzato da un angolo di ingresso e da una configurazione di masse determinante la forza sismica complessiva (si rimanda al capitolo relativo ai casi di carico per chiarimenti inerenti questo aspetto).

Nella colonna Note, in funzione della norma in uso sono riportati i parametri fondamentali che caratterizzano l'azione sismica: in particolare possono essere presenti i seguenti valori:

Angolo di ingresso	Angolo di ingresso dell'azione sismica orizzontale
Fattore di importanza	Fattore di importanza dell'edificio, in base alla categoria di appartenenza
Zona sismica	Zona sismica
Accelerazione ag	Accelerazione orizzontale massima sul suolo
Categoria suolo	Categoria di profilo stratigrafico del suolo di fondazione
Fattore q	Fattore di struttura/di comportamento. Dipendente dalla tipologia strutturale
Fattore di sito S	Fattore dipendente dalla stratigrafia e dal profilo topografico
Classe di duttilità CD	Classe di duttilità della struttura – "A" duttilità alta, "B" duttilità bassa
Fattore riduz. SLD	Fattore di riduzione dello spettro elastico per lo stato limite di danno
Periodo proprio T1	Periodo proprio di vibrazione della struttura
Coefficiente Lambda	Coefficiente dipendente dal periodo proprio T1 e dal numero di piani della struttura
Ordinata spettro Sd(T1)	Valore delle ordinate dello spettro di progetto per lo stato limite ultimo, componente orizzontale (verticale Svd)
Ordinata spettro Se(T1)	Valore delle ordinate dello spettro elastico ridotta del fattore SLD per lo stato limite di danno, componente orizzontale (verticale Sve)
Ordinata spettro S (Tb-Tc)	Valore dell' ordinata dello spettro in uso nel tratto costante
numero di modi considerati	Numero di modi di vibrare della struttura considerati nell'analisi dinamica

Per ciascun caso di carico sismico viene riportato l'insieme di dati sotto riportati (le masse sono espresse in unità di forza):

a) analisi sismica statica equivalente:

- quota, posizione del centro di applicazione e azione orizzontale risultante, posizione del baricentro delle rigidezze, rapporto r/L_s (per strutture a nucleo), indici di regolarità e/r secondo EC8 4.2.3.2
- azione sismica complessiva

b) analisi sismica dinamica con spettro di risposta:

- quota, posizione del centro di massa e massa risultante, posizione del baricentro delle rigidezze, rapporto r/L_s (per strutture a nucleo) , indici di regolarità e/r secondo EC8 4.2.3.2
- frequenza, periodo, accelerazione spettrale, massa eccitata nelle tre direzioni globali per tutti i modi

- massa complessiva ed aliquota di massa complessiva eccitata.

Per ciascuna combinazione sismica definita SLD o SLO viene riportato il livello di deformazione ϵ_T (dr) degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso anche in unità $1000 \cdot \epsilon_T/h$ da confrontare direttamente con i valori forniti nella norma (es. 5 per edifici con tamponamenti collegati rigidamente alla struttura, 10.0 per edifici con tamponamenti collegati elasticamente, 3 per edifici in muratura ordinaria, 4 per edifici in muratura armata). Qualora si applichi il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") l'analisi sismica dinamica può essere comprensiva di sollecitazione verticale contemporanea a quella orizzontale, nel qual caso è effettuata una sovrapposizione degli effetti in ragione della radice dei quadrati degli effetti stessi. Per ciascuna combinazione sismica - analisi effettuate con il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") - viene riportato il livello di deformazione ϵ_T , ϵ_P e ϵ_D degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso in unità $1000 \cdot \epsilon_T/h$ da confrontare direttamente con il valore 2 o 4 per la verifica. Per gli edifici sismicamente isolati si riportano di seguito le verifiche condotte sui dispositivi di isolamento. Le verifiche sono effettuate secondo la circolare 619/2009 del C.S.LL.PP nelle combinazioni in SLC come previsto dal DM 17-01-2018. Per ogni combinazione è riportato il codice di verifica ed i valori utilizzati per la verifica: spostamento dE , area ridotta e dimensione A_2 , azione verticale, deformazioni di taglio dell'elastomero e tensioni nell'acciaio. Qualora si applichi l'Ordinanza 3274 e s.m.i. le verifiche sono eseguite in accordo con l'allegato 10.A. In particolare la tabella, per ogni combinazione di calcolo, riporta:

Nodo	Nodo di appoggio dell' isolatore
Cmb	Combinazione oggetto della verifica
Verif.	Codice di verifica ok – verifica positiva , NV – verifica negativa, ND – verifica non completata
dE	Spostamento relativo tra le due facce (amplificato del 20% per Ordinanza 3274 e smi) combinato con la regola del 30%
Ang fi	Angolo utilizzato per il calcolo dell' area ridotta A_r (per dispositivi circolari)
V	Azione verticale agente
Ar	Area ridotta efficace
Dim A2	Dimensione utile per il calcolo della deformazione per rotazione
Sig s	Tensione nell' inserto in acciaio
Gam c(a,s,t)	Deformazioni di taglio dell' elastomero
Vcr	Carico critico per instabilità

Affinché la verifica sia positiva deve essere:

- 1) $V > 0$
- 2) $\text{Sig s} < f_{yk}$
- 3) $\text{Gam t} < 5$
- 4) $\text{Gam s} < \text{Gam} \cdot (\text{caratteristica dell' elastomero})$
- 5) $\text{Gam s} < 2$
- 6) $V < 0.5 V_{cr}$

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Maggio 2011, disponibile per il download sul sito **www.2si.it**, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
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23	DM 2008: SPETTRO
29	SISMICA 1000/H, SOMMA V, EFFETTO P-δ
30	ANALISI DI UN EDIFICIO CON ISOLATORI SISMICI
70	MASSE SISMICHE
75	PROGETTO DI ISOLATORI ELASTOMERICI
76	VERIFICA DI ISOLATORI ELASTOMERICI
77	VERIFICA DI ISOLATORI FRICTION PENDULUM

Calcolo del fattore di comportamento secondo il D.M. 17/01/2018

Classe di duttilità media (CD"B").

Parametri fattore in direzione x e y

Sistema costruttivo: calcestruzzo

Tipologia strutturale: altre tipologie

Valore base fattore $q_0 = 1.500$

Fattore di regolarità $K_R = 1.0$

Fattore dissipativo $q_D = q_0 \cdot K_R = 1.500$

Fattori di comportamento utilizzati Dissipativi

q SLU x: 1.500

q SLU y: 1.500

q SLU z: 1.500

CDC	Tipo	Sigla Id	Note
2	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)	
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.284 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.462 sec.
			fattore q: 1.500
			fattore per spost. μ_d : 1.584
			classe di duttilità CD: B
			numero di modi considerati: 9
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
-0.40	1.305e+04	2.46	1.74	0.0	-0.22	2.38	1.66	1.365	0.024	0.039
-0.78	698.79	4.65	1.63	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
-0.78	52.71	4.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	37.93	4.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	126.58	3.98	1.35	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
-0.79	63.09	3.46	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	49.91	4.10	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	51.51	3.07	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	88.25	3.59	1.92	0.0	-0.17	0.0	0.0	0.0	0.0	0.0
-0.79	98.23	3.11	1.19	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
-0.79	112.21	2.77	1.10	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
-0.79	149.34	3.03	1.94	0.0	-0.19	0.0	0.0	0.0	0.0	0.0
-0.79	61.43	3.46	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	72.67	1.52	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	72.67	1.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	186.44	2.51	2.29	0.0	-0.21	0.0	0.0	0.0	0.0	0.0
-0.80	99.89	1.07	0.89	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
-0.80	1044.12	1.59	2.87	0.0	-0.22	0.16	4.35	0.147	2.133	0.620
-0.80	50.31	2.67	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	74.27	2.27	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.90	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.52	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.14	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.82	72.67	0.76	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0

SCARICATORE IN VIA PUCCI

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
-0.82	72.67	0.38	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-1.17	3311.80	2.83	2.12	0.0	-0.22	0.0	0.0	0.0	0.0	0.0
-1.55	3363.72	2.81	2.13	0.0	-0.22	2.63	1.66	1.262	0.051	0.227
-1.93	3363.76	2.81	2.13	0.0	-0.22	0.0	0.0	0.0	0.0	0.0
-2.32	3362.73	2.81	2.13	0.0	-0.22	0.0	0.0	0.0	0.0	0.0
-2.70	2116.02	2.94	2.48	0.0	-0.22	3.45	3.84	0.187	0.547	1.694
-3.05	433.13	3.45	3.84	0.0	-0.06	0.0	0.0	0.0	0.0	0.0
Risulta	3.255e+04									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.872	0.534	0.284	9469.52	29.1	1.289e+04	39.6	103.24	0.3	0.0	0.0
2	2.166	0.462	0.284	1.329e+04	40.8	9858.30	30.3	4.62	1.42e-02	0.0	0.0
3	2.795	0.358	0.284	239.81	0.7	58.42	0.2	6.11	1.88e-02	0.0	0.0
4	4.268	0.234	0.284	371.32	1.1	205.03	0.6	3.167e+04	97.3	0.0	0.0
5	5.070	0.197	0.284	3791.71	11.6	5360.30	16.5	4.48	1.38e-02	0.0	0.0
6	5.169	0.193	0.284	5392.62	16.6	4179.04	12.8	759.84	2.3	0.0	0.0
7	83.667	0.012	0.177	4.51e-04	1.38e-06	0.02	5.12e-05	0.05	1.55e-04	0.0	0.0
8	84.355	0.012	0.177	2.12e-03	6.52e-06	0.07	2.23e-04	0.02	7.42e-05	0.0	0.0
9	140.676	0.007	0.173	3.35e-03	1.03e-05	2.15e-06	0.0	2.79e-04	0.0	0.0	0.0
Risulta				3.255e+04		3.255e+04		3.255e+04			
In percentuale				100.00		100.00		100.00			

CDC	Tipo	Sigla Id	Note
3	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)	
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.284 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.458 sec.
			fattore q: 1.500
			fattore per spost. mu d: 1.589
			classe di duttilità CD: B
			numero di modi considerati: 9
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
-0.40	1.305e+04	2.46	1.74	0.0	0.22	2.38	1.66	1.365	0.024	0.039
-0.78	698.79	4.65	1.63	0.0	0.16	0.0	0.0	0.0	0.0	0.0
-0.78	52.71	4.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	37.93	4.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	126.58	3.98	1.35	0.0	0.16	0.0	0.0	0.0	0.0	0.0
-0.79	63.09	3.46	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	49.91	4.10	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	51.51	3.07	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	88.25	3.59	1.92	0.0	0.17	0.0	0.0	0.0	0.0	0.0
-0.79	98.23	3.11	1.19	0.0	0.16	0.0	0.0	0.0	0.0	0.0
-0.79	112.21	2.77	1.10	0.0	0.16	0.0	0.0	0.0	0.0	0.0
-0.79	149.34	3.03	1.94	0.0	0.19	0.0	0.0	0.0	0.0	0.0
-0.79	61.43	3.46	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	72.67	1.52	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	72.67	1.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	186.44	2.51	2.29	0.0	0.21	0.0	0.0	0.0	0.0	0.0
-0.80	99.89	1.07	0.89	0.0	0.16	0.0	0.0	0.0	0.0	0.0
-0.80	1044.12	1.59	2.87	0.0	0.22	0.16	4.35	0.147	2.133	0.620
-0.80	50.31	2.67	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	74.27	2.27	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.90	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.52	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.14	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.82	72.67	0.76	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.82	72.67	0.38	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0

SCARICATORE IN VIA PUCCI

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
-1.17	3311.80	2.83	2.12	0.0	0.22	0.0	0.0	0.0	0.0	0.0
-1.55	3363.72	2.81	2.13	0.0	0.22	2.63	1.66	1.262	0.051	0.227
-1.93	3363.76	2.81	2.13	0.0	0.22	0.0	0.0	0.0	0.0	0.0
-2.32	3362.73	2.81	2.13	0.0	0.22	0.0	0.0	0.0	0.0	0.0
-2.70	2116.02	2.94	2.48	0.0	0.22	3.45	3.84	0.187	0.547	1.694
-3.05	433.13	3.45	3.84	0.0	0.06	0.0	0.0	0.0	0.0	0.0
Risulta	3.255e+04									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.865	0.536	0.284	9563.70	29.4	1.292e+04	39.7	102.23	0.3	0.0	0.0
2	2.185	0.458	0.284	1.350e+04	41.5	9907.18	30.4	5.72	1.76e-02	0.0	0.0
3	2.788	0.359	0.284	1.92	5.90e-03	9.28	2.85e-02	4.54	1.40e-02	0.0	0.0
4	4.268	0.234	0.284	355.64	1.1	188.58	0.6	3.173e+04	97.5	0.0	0.0
5	5.054	0.198	0.284	3598.28	11.1	5579.29	17.1	3.19	9.80e-03	0.0	0.0
6	5.199	0.192	0.284	5533.72	17.0	3950.62	12.1	710.05	2.2	0.0	0.0
7	83.779	0.012	0.177	3.09e-04	0.0	0.03	8.88e-05	0.04	1.20e-04	0.0	0.0
8	84.013	0.012	0.177	2.04e-03	6.27e-06	0.06	1.89e-04	0.04	1.09e-04	0.0	0.0
9	139.451	0.007	0.174	3.46e-03	1.06e-05	2.13e-05	0.0	2.93e-04	0.0	0.0	0.0
Risulta				3.255e+04		3.255e+04		3.255e+04			
In percentuale				100.00		100.00		100.00			

CDC	Tipo	Sigla Id	Note
4	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)	
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.284 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.537 sec.
			fattore q: 1.500
			fattore per spost. mu d: 1.502
			classe di duttilità CD: B
			numero di modi considerati: 9
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
-0.40	1.305e+04	2.46	1.74	0.23	0.0	2.38	1.66	1.365	0.024	0.039
-0.78	698.79	4.65	1.63	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.78	52.71	4.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	37.93	4.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	126.58	3.98	1.35	0.03	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	63.09	3.46	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	49.91	4.10	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	51.51	3.07	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	88.25	3.59	1.92	0.06	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	98.23	3.11	1.19	0.06	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	112.21	2.77	1.10	0.07	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	149.34	3.03	1.94	0.11	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	61.43	3.46	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	72.67	1.52	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	72.67	1.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	186.44	2.51	2.29	0.17	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	99.89	1.07	0.89	0.13	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	1044.12	1.59	2.87	0.21	0.0	0.16	4.35	0.147	2.133	0.620
-0.80	50.31	2.67	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	74.27	2.27	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.90	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.52	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.14	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.82	72.67	0.76	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.82	72.67	0.38	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-1.17	3311.80	2.83	2.12	0.23	0.0	0.0	0.0	0.0	0.0	0.0

SCARICATORE IN VIA PUCCI

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
-1.55	3363.72	2.81	2.13	0.23	0.0	2.63	1.66	1.262	0.051	0.227
-1.93	3363.76	2.81	2.13	0.23	0.0	0.0	0.0	0.0	0.0	0.0
-2.32	3362.73	2.81	2.13	0.23	0.0	0.0	0.0	0.0	0.0	0.0
-2.70	2116.02	2.94	2.48	0.23	0.0	3.45	3.84	0.187	0.547	1.694
-3.05	433.13	3.45	3.84	0.07	0.0	0.0	0.0	0.0	0.0	0.0
Risulta	3.255e+04									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.864	0.537	0.284	8633.84	26.5	1.387e+04	42.6	100.47	0.3	0.0	0.0
2	2.170	0.461	0.284	1.424e+04	43.7	8990.63	27.6	8.80	2.70e-02	0.0	0.0
3	2.832	0.353	0.284	142.52	0.4	52.35	0.2	1.81	5.56e-03	0.0	0.0
4	4.268	0.234	0.284	368.85	1.1	182.03	0.6	3.171e+04	97.4	0.0	0.0
5	5.071	0.197	0.284	5372.91	16.5	3714.74	11.4	58.10	0.2	0.0	0.0
6	5.201	0.192	0.284	3793.07	11.7	5739.21	17.6	668.20	2.1	0.0	0.0
7	84.054	0.012	0.177	1.28e-03	3.95e-06	8.77e-04	2.70e-06	0.07	2.10e-04	0.0	0.0
8	85.921	0.012	0.176	1.07e-03	3.30e-06	0.09	2.69e-04	4.85e-03	1.49e-05	0.0	0.0
9	141.230	0.007	0.173	3.37e-03	1.03e-05	1.30e-05	0.0	2.96e-04	0.0	0.0	0.0
Risulta				3.255e+04		3.255e+04		3.255e+04			
In percentuale				100.00		100.00		100.00			

CDC	Tipo	Sigla Id	Note
5	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)	
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.284 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.534 sec.
			fattore q: 1.500
			fattore per spost. mu d: 1.504
			classe di duttilità CD: B
			numero di modi considerati: 9
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
-0.40	1.305e+04	2.46	1.74	-0.23	0.0	2.38	1.66	1.365	0.024	0.039
-0.78	698.79	4.65	1.63	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.78	52.71	4.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	37.93	4.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	126.58	3.98	1.35	-0.03	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	63.09	3.46	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	49.91	4.10	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	51.51	3.07	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	88.25	3.59	1.92	-0.06	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	98.23	3.11	1.19	-0.06	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	112.21	2.77	1.10	-0.07	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	149.34	3.03	1.94	-0.11	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	61.43	3.46	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	72.67	1.52	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	72.67	1.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	186.44	2.51	2.29	-0.17	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	99.89	1.07	0.89	-0.13	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	1044.12	1.59	2.87	-0.21	0.0	0.16	4.35	0.147	2.133	0.620
-0.80	50.31	2.67	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	74.27	2.27	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.90	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.52	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.14	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.82	72.67	0.76	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.82	72.67	0.38	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-1.17	3311.80	2.83	2.12	-0.23	0.0	0.0	0.0	0.0	0.0	0.0
-1.55	3363.72	2.81	2.13	-0.23	0.0	2.63	1.66	1.262	0.051	0.227

SCARICATORE IN VIA PUCCI

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
-1.93	3363.76	2.81	2.13	-0.23	0.0	0.0	0.0	0.0	0.0	0.0
-2.32	3362.73	2.81	2.13	-0.23	0.0	0.0	0.0	0.0	0.0	0.0
-2.70	2116.02	2.94	2.48	-0.23	0.0	3.45	3.84	0.187	0.547	1.694
-3.05	433.13	3.45	3.84	-0.07	0.0	0.0	0.0	0.0	0.0	0.0
Risulta	3.255e+04									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.872	0.534	0.284	9328.42	28.7	1.302e+04	40.0	102.80	0.3	0.0	0.0
2	2.185	0.458	0.284	1.368e+04	42.0	9735.81	29.9	6.47	1.99e-02	0.0	0.0
3	2.749	0.364	0.284	2.51	7.73e-03	20.27	6.23e-02	2.75	8.44e-03	0.0	0.0
4	4.268	0.234	0.284	375.19	1.2	200.82	0.6	3.167e+04	97.3	0.0	0.0
5	5.055	0.198	0.284	3559.74	10.9	5619.67	17.3	2.84	8.73e-03	0.0	0.0
6	5.169	0.193	0.284	5609.62	17.2	3949.96	12.1	761.92	2.3	0.0	0.0
7	82.277	0.012	0.177	6.20e-04	1.91e-06	0.09	2.75e-04	2.44e-05	0.0	0.0	0.0
8	83.565	0.012	0.177	1.95e-03	5.98e-06	1.83e-03	5.64e-06	0.08	2.32e-04	0.0	0.0
9	140.125	0.007	0.174	3.33e-03	1.02e-05	1.20e-05	0.0	2.75e-04	0.0	0.0	0.0
Risulta				3.255e+04		3.255e+04		3.255e+04			
In percentuale				100.00		100.00		100.00			

CDC	Tipo	Sigla Id	Note
6	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. +)	
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.181 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.462 sec.
			numero di modi considerati: 9
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
-0.40	1.305e+04	2.46	1.74	0.0	-0.22	2.38	1.66	1.365	0.024	0.039
-0.78	698.79	4.65	1.63	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
-0.78	52.71	4.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	37.93	4.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	126.58	3.98	1.35	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
-0.79	63.09	3.46	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	49.91	4.10	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	51.51	3.07	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	88.25	3.59	1.92	0.0	-0.17	0.0	0.0	0.0	0.0	0.0
-0.79	98.23	3.11	1.19	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
-0.79	112.21	2.77	1.10	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
-0.79	149.34	3.03	1.94	0.0	-0.19	0.0	0.0	0.0	0.0	0.0
-0.79	61.43	3.46	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	72.67	1.52	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	72.67	1.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	186.44	2.51	2.29	0.0	-0.21	0.0	0.0	0.0	0.0	0.0
-0.80	99.89	1.07	0.89	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
-0.80	1044.12	1.59	2.87	0.0	-0.22	0.16	4.35	0.147	2.133	0.620
-0.80	50.31	2.67	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	74.27	2.27	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.90	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.52	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.14	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.82	72.67	0.76	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.82	72.67	0.38	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-1.17	3311.80	2.83	2.12	0.0	-0.22	0.0	0.0	0.0	0.0	0.0
-1.55	3363.72	2.81	2.13	0.0	-0.22	2.63	1.66	1.262	0.051	0.227
-1.93	3363.76	2.81	2.13	0.0	-0.22	0.0	0.0	0.0	0.0	0.0
-2.32	3362.73	2.81	2.13	0.0	-0.22	0.0	0.0	0.0	0.0	0.0
-2.70	2116.02	2.94	2.48	0.0	-0.22	3.45	3.84	0.187	0.547	1.694
-3.05	433.13	3.45	3.84	0.0	-0.06	0.0	0.0	0.0	0.0	0.0

SCARICATORE IN VIA PUCCI

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
Risulta	3.255e+04									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.872	0.534	0.157	9469.52	29.1	1.289e+04	39.6	103.24	0.3	0.0	0.0
2	2.166	0.462	0.181	1.329e+04	40.8	9858.30	30.3	4.62	1.42e-02	0.0	0.0
3	2.795	0.358	0.181	239.81	0.7	58.42	0.2	6.11	1.88e-02	0.0	0.0
4	4.268	0.234	0.181	371.32	1.1	205.03	0.6	3.167e+04	97.3	0.0	0.0
5	5.070	0.197	0.181	3791.71	11.6	5360.30	16.5	4.48	1.38e-02	0.0	0.0
6	5.169	0.193	0.181	5392.62	16.6	4179.04	12.8	759.84	2.3	0.0	0.0
7	83.667	0.012	0.083	4.51e-04	1.38e-06	0.02	5.12e-05	0.05	1.55e-04	0.0	0.0
8	84.355	0.012	0.083	2.12e-03	6.52e-06	0.07	2.23e-04	0.02	7.42e-05	0.0	0.0
9	140.676	0.007	0.080	3.35e-03	1.03e-05	2.15e-06	0.0	2.79e-04	0.0	0.0	0.0
Risulta				3.255e+04		3.255e+04		3.255e+04			
In percentuale				100.00		100.00		100.00			

CDC	Tipo	Sigla Id	Note
7	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -)	
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.181 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.458 sec.
			numero di modi considerati: 9
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
-0.40	1.305e+04	2.46	1.74	0.0	0.22	2.38	1.66	1.365	0.024	0.039
-0.78	698.79	4.65	1.63	0.0	0.16	0.0	0.0	0.0	0.0	0.0
-0.78	52.71	4.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	37.93	4.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	126.58	3.98	1.35	0.0	0.16	0.0	0.0	0.0	0.0	0.0
-0.79	63.09	3.46	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	49.91	4.10	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	51.51	3.07	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	88.25	3.59	1.92	0.0	0.17	0.0	0.0	0.0	0.0	0.0
-0.79	98.23	3.11	1.19	0.0	0.16	0.0	0.0	0.0	0.0	0.0
-0.79	112.21	2.77	1.10	0.0	0.16	0.0	0.0	0.0	0.0	0.0
-0.79	149.34	3.03	1.94	0.0	0.19	0.0	0.0	0.0	0.0	0.0
-0.79	61.43	3.46	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	72.67	1.52	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	72.67	1.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	186.44	2.51	2.29	0.0	0.21	0.0	0.0	0.0	0.0	0.0
-0.80	99.89	1.07	0.89	0.0	0.16	0.0	0.0	0.0	0.0	0.0
-0.80	1044.12	1.59	2.87	0.0	0.22	0.16	4.35	0.147	2.133	0.620
-0.80	50.31	2.67	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	74.27	2.27	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.90	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.52	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.14	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.82	72.67	0.76	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.82	72.67	0.38	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-1.17	3311.80	2.83	2.12	0.0	0.22	0.0	0.0	0.0	0.0	0.0
-1.55	3363.72	2.81	2.13	0.0	0.22	2.63	1.66	1.262	0.051	0.227
-1.93	3363.76	2.81	2.13	0.0	0.22	0.0	0.0	0.0	0.0	0.0
-2.32	3362.73	2.81	2.13	0.0	0.22	0.0	0.0	0.0	0.0	0.0
-2.70	2116.02	2.94	2.48	0.0	0.22	3.45	3.84	0.187	0.547	1.694
-3.05	433.13	3.45	3.84	0.0	0.06	0.0	0.0	0.0	0.0	0.0
Risulta	3.255e+04									

SCARICATORE IN VIA PUCCI

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.865	0.536	0.157	9563.70	29.4	1.292e+04	39.7	102.23	0.3	0.0	0.0
2	2.185	0.458	0.181	1.350e+04	41.5	9907.18	30.4	5.72	1.76e-02	0.0	0.0
3	2.788	0.359	0.181	1.92	5.90e-03	9.28	2.85e-02	4.54	1.40e-02	0.0	0.0
4	4.268	0.234	0.181	355.64	1.1	188.58	0.6	3.173e+04	97.5	0.0	0.0
5	5.054	0.198	0.181	3598.28	11.1	5579.29	17.1	3.19	9.80e-03	0.0	0.0
6	5.199	0.192	0.181	5533.72	17.0	3950.62	12.1	710.05	2.2	0.0	0.0
7	83.779	0.012	0.083	3.09e-04	0.0	0.03	8.88e-05	0.04	1.20e-04	0.0	0.0
8	84.013	0.012	0.083	2.04e-03	6.27e-06	0.06	1.89e-04	0.04	1.09e-04	0.0	0.0
9	139.451	0.007	0.080	3.46e-03	1.06e-05	2.13e-05	0.0	2.93e-04	0.0	0.0	0.0
Risulta				3.255e+04		3.255e+04		3.255e+04			
In percentuale				100.00		100.00		100.00			

CDC	Tipo	Sigla Id	Note
8	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +)	
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.181 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.537 sec.
			numero di modi considerati: 9
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
-0.40	1.305e+04	2.46	1.74	0.23	0.0	2.38	1.66	1.365	0.024	0.039
-0.78	698.79	4.65	1.63	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.78	52.71	4.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	37.93	4.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	126.58	3.98	1.35	0.03	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	63.09	3.46	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	49.91	4.10	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	51.51	3.07	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	88.25	3.59	1.92	0.06	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	98.23	3.11	1.19	0.06	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	112.21	2.77	1.10	0.07	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	149.34	3.03	1.94	0.11	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	61.43	3.46	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	72.67	1.52	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	72.67	1.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	186.44	2.51	2.29	0.17	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	99.89	1.07	0.89	0.13	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	1044.12	1.59	2.87	0.21	0.0	0.16	4.35	0.147	2.133	0.620
-0.80	50.31	2.67	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	74.27	2.27	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.90	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.52	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.14	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.82	72.67	0.76	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.82	72.67	0.38	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-1.17	3311.80	2.83	2.12	0.23	0.0	0.0	0.0	0.0	0.0	0.0
-1.55	3363.72	2.81	2.13	0.23	0.0	2.63	1.66	1.262	0.051	0.227
-1.93	3363.76	2.81	2.13	0.23	0.0	0.0	0.0	0.0	0.0	0.0
-2.32	3362.73	2.81	2.13	0.23	0.0	0.0	0.0	0.0	0.0	0.0
-2.70	2116.02	2.94	2.48	0.23	0.0	3.45	3.84	0.187	0.547	1.694
-3.05	433.13	3.45	3.84	0.07	0.0	0.0	0.0	0.0	0.0	0.0
Risulta	3.255e+04									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.864	0.537	0.157	8633.84	26.5	1.387e+04	42.6	100.47	0.3	0.0	0.0
2	2.170	0.461	0.181	1.424e+04	43.7	8990.63	27.6	8.80	2.70e-02	0.0	0.0

SCARICATORE IN VIA PUCCI

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
3	2.832	0.353	0.181	142.52	0.4	52.35	0.2	1.81	5.56e-03	0.0	0.0
4	4.268	0.234	0.181	368.85	1.1	182.03	0.6	3.171e+04	97.4	0.0	0.0
5	5.071	0.197	0.181	5372.91	16.5	3714.74	11.4	58.10	0.2	0.0	0.0
6	5.201	0.192	0.181	3793.07	11.7	5739.21	17.6	668.20	2.1	0.0	0.0
7	84.054	0.012	0.083	1.28e-03	3.95e-06	8.77e-04	2.70e-06	0.07	2.10e-04	0.0	0.0
8	85.921	0.012	0.083	1.07e-03	3.30e-06	0.09	2.69e-04	4.85e-03	1.49e-05	0.0	0.0
9	141.230	0.007	0.080	3.37e-03	1.03e-05	1.30e-05	0.0	2.96e-04	0.0	0.0	0.0
Risulta In percentuale				3.255e+04 100.00		3.255e+04 100.00		3.255e+04 100.00			

CDC	Tipo	Sigla Id	Note
9	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -)	
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.181 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.534 sec.
			numero di modi considerati: 9
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	m	m	m	m	m	m			
-0.40	1.305e+04	2.46	1.74	-0.23	0.0	2.38	1.66	1.365	0.024	0.039
-0.78	698.79	4.65	1.63	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.78	52.71	4.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	37.93	4.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	126.58	3.98	1.35	-0.03	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	63.09	3.46	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	49.91	4.10	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	51.51	3.07	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	88.25	3.59	1.92	-0.06	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	98.23	3.11	1.19	-0.06	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	112.21	2.77	1.10	-0.07	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	149.34	3.03	1.94	-0.11	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	61.43	3.46	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.79	72.67	1.52	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	72.67	1.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	186.44	2.51	2.29	-0.17	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	99.89	1.07	0.89	-0.13	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	1044.12	1.59	2.87	-0.21	0.0	0.16	4.35	0.147	2.133	0.620
-0.80	50.31	2.67	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.80	74.27	2.27	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.90	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.52	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.81	72.67	1.14	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.82	72.67	0.76	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-0.82	72.67	0.38	3.25	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-1.17	3311.80	2.83	2.12	-0.23	0.0	0.0	0.0	0.0	0.0	0.0
-1.55	3363.72	2.81	2.13	-0.23	0.0	2.63	1.66	1.262	0.051	0.227
-1.93	3363.76	2.81	2.13	-0.23	0.0	0.0	0.0	0.0	0.0	0.0
-2.32	3362.73	2.81	2.13	-0.23	0.0	0.0	0.0	0.0	0.0	0.0
-2.70	2116.02	2.94	2.48	-0.23	0.0	3.45	3.84	0.187	0.547	1.694
-3.05	433.13	3.45	3.84	-0.07	0.0	0.0	0.0	0.0	0.0	0.0
Risulta	3.255e+04									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.872	0.534	0.157	9328.42	28.7	1.302e+04	40.0	102.80	0.3	0.0	0.0
2	2.185	0.458	0.181	1.368e+04	42.0	9735.81	29.9	6.47	1.99e-02	0.0	0.0
3	2.749	0.364	0.181	2.51	7.73e-03	20.27	6.23e-02	2.75	8.44e-03	0.0	0.0
4	4.268	0.234	0.181	375.19	1.2	200.82	0.6	3.167e+04	97.3	0.0	0.0
5	5.055	0.198	0.181	3559.74	10.9	5619.67	17.3	2.84	8.73e-03	0.0	0.0

SCARICATORE IN VIA PUCCI

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
6	5.169	0.193	0.181	5609.62	17.2	3949.96	12.1	761.92	2.3	0.0	0.0
7	82.277	0.012	0.083	6.20e-04	1.91e-06	0.09	2.75e-04	2.44e-05	0.0	0.0	0.0
8	83.565	0.012	0.083	1.95e-03	5.98e-06	1.83e-03	5.64e-06	0.08	2.32e-04	0.0	0.0
9	140.125	0.007	0.080	3.33e-03	1.02e-05	1.20e-05	0.0	2.75e-04	0.0	0.0	0.0
Risulta				3.255e+04		3.255e+04		3.255e+04			
In percentuale				100.00		100.00		100.00			

RISULTATI OPERE DI FONDAZIONE

LEGENDA RISULTATI OPERE DI FONDAZIONE

Il controllo dei risultati delle analisi condotte, per quanto concerne le opere di fondazione, è possibile in relazione alle tabelle sotto riportate.

La prima tabella è riferita alle fondazioni tipo palo e plinto su pali.

Per questo tipo di fondazione vengono riportate le sei componenti di sollecitazione (esprese nel riferimento globale della struttura) per ogni palo componente l'opera.

In particolare viene riportato:

Nodo	numero del nodo a cui è applicato il plinto
Tipo	codice corrispondente al nome assegnato al tipo di plinto di fondazione: 3) palo singolo (<i>PALO</i>) 4) plinto su palo 5) plinto su due pali (<i>PL.2P</i>) 6) plinto su tre pali (<i>PL.3P</i>) 7) plinto su quattro pali (<i>PL.4P</i>) 8) plinto rettangolare su cinque pali (<i>PL.5P.R</i>) 9) plinto pentagonale su cinque pali (<i>PL.5P</i>) 10) plinto su sei pali (<i>PL.6P</i>)
Palo	numero del palo
Comb.	combinazione di carico in cui si verificano le sei componenti di sollecitazione.
Quota	quota assoluta della sezione del palo per cui si riportano le sei componenti di sollecitazione.

L'azione F_z (corrispondente allo sforzo normale nel palo) è costante poiché il peso del palo stesso non è considerato nella modellazione.

La seconda tabella è riferita alle fondazioni tipo plinto su suolo elastico.

Per questo tipo di fondazione vengono riportate le pressioni nei quattro vertici dell'impronta sul terreno.

In particolare viene riportato:

Nodo	numero del nodo a cui è applicato il plinto
Tipo	Codice identificativo del nome assegnato al plinto
area	area dell'impronta del plinto
Wink O Wink V	coefficienti di Winkler (orizzontale e verticale) adottati
Comb	Combinazione di carico in cui si verificano i valori riportati
Pt (P1 P2 P3 P4)	valori di pressione nei vertici

La terza tabella è riferita alle fondazioni tipo platea su suolo elastico.

Per questo tipo di fondazione vengono riportate le pressioni in ogni vertice (nodo) degli elementi costituenti la platea.

La quarta tabella è riferita alle fondazioni tipo trave su suolo elastico.

Per questo tipo di fondazione vengono riportate le pressioni alle estremità dell'elemento e la massima (in valore assoluto) pressione lungo lo sviluppo dell'elemento.

Vengono inoltre riportati, con funzione statistica, i valori massimo e minimo delle pressioni che compaiono nella tabella.

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Settembre 2014, disponibile per il download sul sito **www.2si.it**, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
105	PLINTO SUPERFICIALE
106	PLINTO SUPERFICIALE
107	PLINTO SUPERFICIALE
108	PLINTO SUPERFICIALE
109	PLINTO SUPERFICIALE
110	PLINTO SUPERFICIALE
111	PLINTO SUPERFICIALE
112	PLINTO SUPERFICIALE
113	PLINTO SUPERFICIALE
114	PLINTO SUPERFICIALE
115	PLINTO SUPERFICIALE
116	PLINTO SUPERFICIALE
117	PLINTO SUPERFICIALE
118	PLINTO SUPERFICIALE
119	PLINTO SUPERFICIALE
120	PLINTO SUPERFICIALE
121	PLINTO SUPERFICIALE
122	PLINTO SUPERFICIALE
123	PLINTO SUPERFICIALE
124	FONDAZIONE NASTRIFORME
125	CALCOLO DEI K DI WINKLER

Nodo (G)	Pt 1/12	Pt 2/13	Pt 3...	Pt 4...							
	daN/cm2	daN/cm2	daN/cm2	daN/cm2	daN/cm2	daN/cm2	daN/cm2	daN/cm2	daN/cm2	daN/cm2	daN/cm2
1	-2.51	-1.86	-1.79	-1.79							
2	-2.50	-1.85	-1.78	-1.77							
3	-2.48	-1.83	-1.76	-1.76							
4	-2.42	-1.80	-1.73	-1.72							
5	-2.39	-1.79	-1.72	-1.70							
6	-2.37	-1.79	-1.72	-1.68							
7	-2.34	-1.80	-1.71	-1.66							
8	-2.47	-1.85	-1.77	-1.75							
9	-2.45	-1.84	-1.76	-1.74							
10	-2.43	-1.82	-1.74	-1.72							
11	-2.37	-1.78	-1.71	-1.68							
12	-2.34	-1.77	-1.70	-1.66							
13	-2.33	-1.77	-1.70	-1.66							
14	-2.32	-1.77	-1.69	-1.65							
15	-2.29	-1.77	-1.69	-1.62							
16	-2.31	-1.82	-1.71	-1.64							
17	-2.29	-1.80	-1.69	-1.63							
18	-2.26	-1.77	-1.67	-1.61							
19	-2.20	-1.73	-1.63	-1.56							
20	-2.16	-1.71	-1.61	-1.54							
21	-2.13	-1.70	-1.60	-1.51							
22	-2.15	-1.78	-1.64	-1.53							
23	-2.13	-1.76	-1.63	-1.52							
24	-2.10	-1.73	-1.60	-1.49							
25	-2.03	-1.67	-1.56	-1.45							
26	-2.00	-1.66	-1.54	-1.43							
27	-1.97	-1.64	-1.52	-1.40							
28	-2.05	-1.76	-1.60	-1.46							
29	-2.03	-1.74	-1.59	-1.45							
30	-1.99	-1.70	-1.56	-1.42							
31	-1.92	-1.64	-1.51	-1.37							
32	-1.90	-1.63	-1.50	-1.36							
33	-1.87	-1.61	-1.48	-1.34							
34	-1.59	-1.20	-1.15	-1.12							
35	-1.57	-1.17	-1.13	-1.11							
36	-1.55	-1.15	-1.10	-1.09							
37	-1.53	-1.13	-1.09	-1.08							
38	-1.51	-1.12	-1.07	-1.06							
39	-1.49	-1.11	-1.06	-1.05							
40	-1.47	-1.10	-1.05	-1.04							
41	-1.45	-1.10	-1.04	-1.02							
42	-1.44	-1.10	-1.03	-1.01							
43	-1.43	-1.10	-1.03	-1.01							

SCARICATORE IN VIA PUCCI

44	-1.41	-1.10	-1.02	-0.99
45	-1.39	-1.10	-1.02	-0.98
46	-1.39	-1.10	-1.02	-0.98
47	-1.37	-1.10	-1.01	-0.97
48	-1.37	-1.10	-1.01	-0.96
49	-1.35	-1.10	-1.01	-0.95
50	-1.54	-1.16	-1.11	-1.09
51	-1.52	-1.13	-1.09	-1.07
52	-1.50	-1.10	-1.06	-1.06
53	-1.48	-1.08	-1.04	-1.04
54	-1.46	-1.07	-1.03	-1.03
55	-1.44	-1.05	-1.01	-1.01
56	-1.42	-1.05	-1.00	-1.00
57	-1.40	-1.04	-0.99	-0.99
58	-1.38	-1.04	-0.99	-0.98
59	-1.38	-1.04	-0.99	-0.97
60	-1.36	-1.04	-0.98	-0.96
61	-1.34	-1.04	-0.98	-0.95
62	-1.34	-1.04	-0.97	-0.94
63	-1.32	-1.05	-0.97	-0.93
64	-1.32	-1.05	-0.97	-0.93
65	-1.30	-1.05	-0.96	-0.91
66	-1.48	-1.13	-1.07	-1.05
67	-1.46	-1.09	-1.05	-1.04
68	-1.44	-1.06	-1.03	-1.02
69	-1.43	-1.04	-1.00	-1.01
70	-1.41	-1.01	-0.98	-0.99
71	-1.39	-1.00	-0.97	-0.98
72	-1.37	-0.99	-0.96	-0.97
73	-1.35	-0.99	-0.95	-0.95
74	-1.33	-0.99	-0.94	-0.94
75	-1.33	-0.99	-0.94	-0.94
76	-1.31	-0.99	-0.93	-0.92
77	-1.29	-0.99	-0.93	-0.91
78	-1.29	-0.99	-0.93	-0.91
79	-1.27	-0.99	-0.93	-0.90
80	-1.27	-1.00	-0.93	-0.89
81	-1.25	-1.00	-0.92	-0.88
82	-1.42	-1.08	-1.03	-1.01
83	-1.40	-1.05	-1.01	-0.99
84	-1.38	-1.02	-0.98	-0.98
85	-1.36	-0.99	-0.96	-0.96
86	-1.34	-0.96	-0.93	-0.95
87	-1.32	-0.94	-0.92	-0.94
88	-1.30	-0.93	-0.90	-0.92
89	-1.28	-0.92	-0.89	-0.91
90	-1.27	-0.92	-0.89	-0.90
91	-1.26	-0.92	-0.89	-0.89
92	-1.24	-0.92	-0.88	-0.88
93	-1.23	-0.93	-0.88	-0.87
94	-1.22	-0.93	-0.88	-0.86
95	-1.21	-0.93	-0.87	-0.86
96	-1.20	-0.93	-0.87	-0.85
97	-1.18	-0.94	-0.87	-0.84
98	-1.36	-1.04	-0.99	-0.96
99	-1.34	-1.01	-0.96	-0.95
100	-1.32	-0.98	-0.94	-0.93
101	-1.30	-0.94	-0.91	-0.92
102	-1.28	-0.91	-0.89	-0.91
103	-1.26	-0.88	-0.87	-0.89
104	-1.24	-0.86	-0.85	-0.88
105	-1.22	-0.86	-0.84	-0.86
106	-1.21	-0.86	-0.83	-0.85
107	-1.20	-0.86	-0.83	-0.85
108	-1.18	-0.86	-0.83	-0.84
109	-1.17	-0.86	-0.83	-0.83
110	-1.16	-0.87	-0.83	-0.82
111	-1.15	-0.87	-0.82	-0.81
112	-1.14	-0.88	-0.82	-0.81
113	-1.12	-0.88	-0.82	-0.79
114	-1.30	-1.01	-0.95	-0.92
115	-1.28	-0.98	-0.93	-0.91
116	-1.26	-0.94	-0.90	-0.89
117	-1.24	-0.90	-0.87	-0.88
118	-1.22	-0.87	-0.85	-0.86
119	-1.20	-0.84	-0.82	-0.85
120	-1.18	-0.80	-0.80	-0.84
121	-1.16	-0.79	-0.78	-0.82
122	-1.15	-0.79	-0.78	-0.81

SCARICATORE IN VIA PUCCI

123	-1.14	-0.80	-0.78	-0.81
124	-1.12	-0.80	-0.78	-0.79
125	-1.11	-0.81	-0.78	-0.78
126	-1.10	-0.81	-0.78	-0.78
127	-1.09	-0.82	-0.78	-0.77
128	-1.08	-0.82	-0.78	-0.76
129	-1.06	-0.83	-0.78	-0.75
130	-1.24	-0.98	-0.92	-0.88
131	-1.22	-0.94	-0.89	-0.86
132	-1.20	-0.91	-0.86	-0.85
133	-1.18	-0.87	-0.84	-0.83
134	-1.16	-0.84	-0.81	-0.82
135	-1.14	-0.80	-0.79	-0.81
136	-1.12	-0.77	-0.76	-0.79
137	-1.10	-0.75	-0.74	-0.78
138	-1.08	-0.75	-0.74	-0.77
139	-1.08	-0.75	-0.74	-0.76
140	-1.06	-0.76	-0.74	-0.75
141	-1.04	-0.76	-0.74	-0.74
142	-1.04	-0.76	-0.74	-0.73
143	-1.02	-0.77	-0.74	-0.73
144	-1.02	-0.77	-0.74	-0.72
145	-1.00	-0.78	-0.74	-0.71
146	-1.20	-0.96	-0.90	-0.85
147	-1.18	-0.93	-0.87	-0.84
148	-1.16	-0.89	-0.84	-0.82
149	-1.14	-0.86	-0.82	-0.81
150	-1.12	-0.82	-0.79	-0.79
151	-1.10	-0.79	-0.77	-0.78
152	-1.08	-0.76	-0.74	-0.77
153	-1.06	-0.74	-0.73	-0.75
154	-1.05	-0.73	-0.72	-0.74
155	-1.04	-0.73	-0.72	-0.74
156	-1.02	-0.73	-0.71	-0.72
157	-1.01	-0.74	-0.71	-0.71
158	-1.00	-0.74	-0.71	-0.71
159	-0.99	-0.74	-0.71	-0.70
160	-0.98	-0.75	-0.71	-0.69
161	-0.96	-0.76	-0.71	-0.68
162	-1.16	-0.94	-0.87	-0.82
163	-1.14	-0.91	-0.85	-0.81
164	-1.12	-0.87	-0.82	-0.79
165	-1.10	-0.84	-0.79	-0.78
166	-1.08	-0.81	-0.77	-0.77
167	-1.06	-0.78	-0.75	-0.75
168	-1.04	-0.75	-0.73	-0.74
169	-1.02	-0.73	-0.71	-0.72
170	-1.01	-0.72	-0.70	-0.71
171	-1.00	-0.71	-0.70	-0.71
172	-0.98	-0.71	-0.69	-0.69
173	-0.97	-0.71	-0.69	-0.68
174	-0.96	-0.71	-0.69	-0.68
175	-0.95	-0.72	-0.68	-0.67
176	-0.94	-0.72	-0.68	-0.67
177	-0.92	-0.73	-0.68	-0.65
178	-1.12	-0.93	-0.85	-0.79
179	-1.10	-0.89	-0.82	-0.78
180	-1.08	-0.86	-0.80	-0.77
181	-1.06	-0.83	-0.78	-0.75
182	-1.04	-0.80	-0.75	-0.74
183	-1.02	-0.77	-0.73	-0.72
184	-1.00	-0.74	-0.71	-0.71
185	-0.98	-0.72	-0.69	-0.69
186	-0.97	-0.71	-0.68	-0.69
187	-0.96	-0.70	-0.68	-0.68
188	-0.94	-0.69	-0.67	-0.67
189	-0.92	-0.69	-0.66	-0.66
190	-0.92	-0.69	-0.66	-0.65
191	-0.91	-0.69	-0.66	-0.64
192	-0.90	-0.69	-0.66	-0.64
193	-0.88	-0.70	-0.66	-0.62
194	-1.10	-0.92	-0.84	-0.78
195	-1.08	-0.89	-0.81	-0.77
196	-1.06	-0.86	-0.79	-0.75
197	-1.04	-0.82	-0.77	-0.74
198	-1.02	-0.79	-0.75	-0.72
199	-1.00	-0.77	-0.72	-0.71
200	-0.98	-0.74	-0.70	-0.70
201	-0.95	-0.71	-0.68	-0.68

202	-0.95	-0.70	-0.67	-0.67
203	-0.94	-0.69	-0.67	-0.67
204	-0.92	-0.68	-0.66	-0.65
205	-0.91	-0.68	-0.65	-0.64
206	-0.90	-0.68	-0.65	-0.64
207	-0.89	-0.68	-0.65	-0.63
208	-0.88	-0.68	-0.65	-0.62
209	-0.86	-0.69	-0.65	-0.61

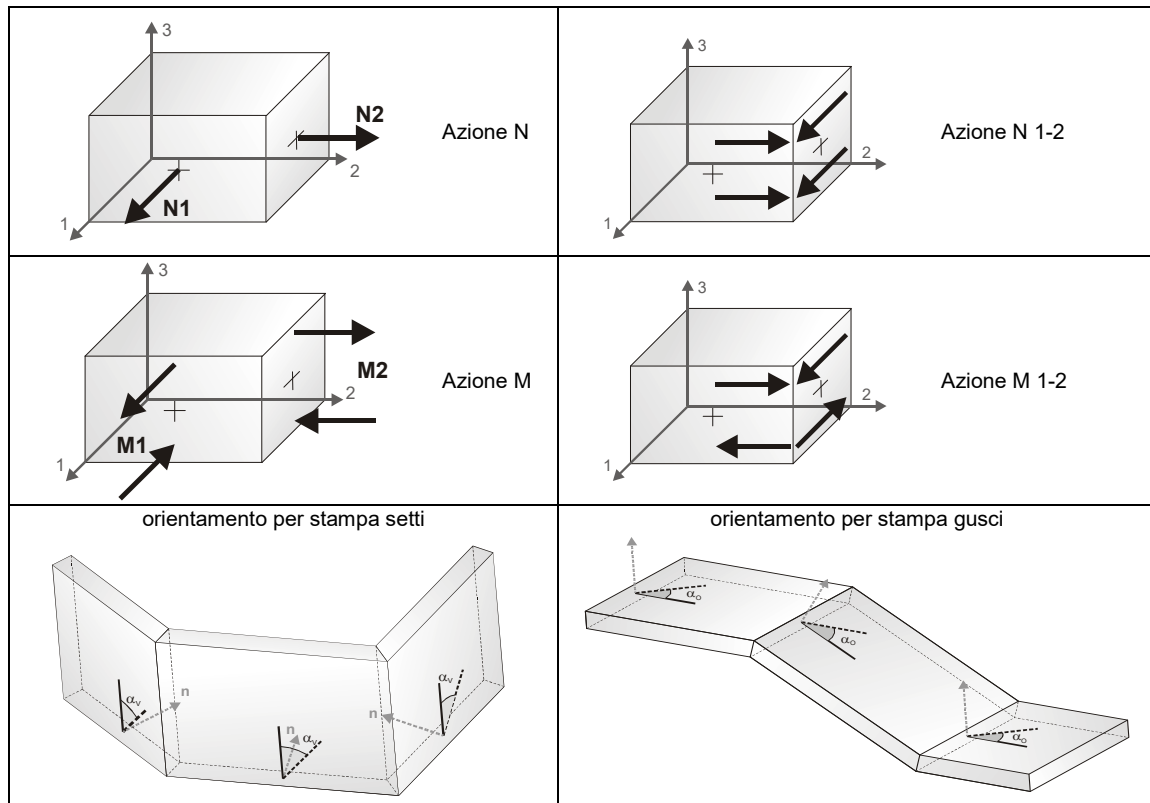
Nodo (G)	Pt 1/12	Pt 2/13	Pt 3...	Pt 4...
	-2.51			
	-0.61			

RISULTATI ELEMENTI TIPO SHELL

LEGENDA RISULTATI ELEMENTI TIPO SHELL

Il controllo dei risultati delle analisi condotte, per quanto concerne gli elementi tipo shell, è possibile in relazione alle tabelle sottoriportate.

Per ogni elemento, e per ogni combinazione(o caso di carico) vengono riportati i risultati più significativi.



In particolare vengono riportati in ogni nodo di un elemento per ogni combinazione:

tensione di Von Mises		(valore riassuntivo del complessivo stato di sollecitazione)
N max		sforzo membranale principale massimo
N min		sforzo membranale principale minimo
M max		sforzo flessionale principale massimo
M min		sforzo flessionale principale minimo
N1	N2	sforzi membranali e flessionali in direzione locale 1 e 2 dell'elemento (lo sforzo 2-1 è uguale allo sforzo 1-2 per la reciprocità delle tensioni tangenziali)
N1-2	M1	
M2	M1-2	

I suddetti risultati possono a scelta del progettista essere preceduti o sostituiti da valori di sollecitazione non più riferiti al sistema locale dell'elemento ma al sistema globale.

In questo caso gli elementi vengono raggruppati in gruppi (M_S: macro gusci o macro setti, raggruppati per materiale, spessore, e posizione fisica) per la valutazione dei valori mediati ai nodi appartenenti agli elementi dei gruppi stessi.

I valori di sollecitazione sono, in questo caso, riferiti ad una terna specifica del gruppo ruotata di α_0 attorno all'asse Z per i gusci e ruotata di α_v attorno alla normale (che per definizione è orizzontale) al piano del setto. Per i setti, in particolare, se α_v è zero, l'asse '1-1 rappresenta la verticale e l'asse '2-2 l'orizzontale contenuta nel setto. Le azioni sui setti possono essere espresse anche con formato macro, cioè riferite all'intero macroelemento. In particolare vengono riportati per ogni quota Z dei nodi e per ogni combinazione i seguenti valori:

N memb.	Azione membranale complessiva agente sulla parete in direzione Z
V memb.	Azione complessiva di taglio agente nel piano del macroelemento
V orto	Azione complessiva di taglio agente in direzione perpendicolare al macroelemento
M memb.	Azione flessionale complessiva agente nel piano del macroelemento
M orto	Azione flessionale complessiva agente in direzione perpendicolare al macroelemento
T	Azione torsionale complessiva agente nel piano orizzontale

Macro	Tipo	Angolo 1-Z (gradi)
2	Setto	0.0

M_S	Cmb	Z cm	N memb. daN	V memb. daN	V orto daN	M memb. daN cm	M orto daN cm	T daN cm
2	2	-305.00	-6271.42	-1069.81	-707.82	-8986.00	-3.784e+04	336.02
2	2	-270.00	-6472.57	-964.99	-1312.55	-5.503e+04	-7.316e+04	-8751.18
2	2	-231.67	-3.034e+04	-816.09	-7684.28	-5.066e+05	4.926e+04	-1.345e+04
2	2	-231.67	-3.034e+04	-816.09	-7684.28	-5.066e+05	4.926e+04	-1.345e+04
2	2	-193.33	-2.884e+04	-663.89	-3326.78	-4.023e+05	-6.257e+04	-3698.47
2	2	-193.33	-2.884e+04	-663.89	-3326.78	-4.023e+05	-6.257e+04	-3698.47
2	2	-155.00	-2.833e+04	-584.21	-772.63	-4.041e+05	-5.797e+04	1944.16
2	2	-116.67	-2.873e+04	-393.18	1911.39	-5.221e+05	2.432e+04	9057.16
2	2	-116.67	-2.873e+04	-393.18	1911.39	-5.221e+05	2.432e+04	9057.16
2	2	-82.18	-3.008e+04	-136.50	6267.38	-6.371e+05	2.009e+05	1.831e+04
2	2	-81.84	-3.001e+04	-87.04	6580.71	-6.564e+05	2.045e+05	1.402e+04
2	2	-81.50	-2.991e+04	-71.74	6825.99	-6.745e+05	2.035e+05	9317.56
2	2	-81.16	-2.984e+04	-60.76	7153.67	-6.872e+05	2.059e+05	6175.25
2	2	-80.81	-2.977e+04	-79.48	7488.07	-6.944e+05	2.089e+05	6357.38
2	2	-80.47	-2.972e+04	-80.64	7754.62	-6.961e+05	2.079e+05	1.163e+04
2	2	-80.12	-2.968e+04	-17.98	8086.68	-6.937e+05	2.117e+05	1.836e+04
2	2	-80.00	-2.967e+04	-22.22	8195.73	-6.914e+05	2.123e+05	1.909e+04
2	2	-79.89	-2.962e+04	-87.66	8265.05	-6.882e+05	2.137e+05	1.885e+04
2	2	-79.76	-2.961e+04	-122.39	8296.40	-6.872e+05	2.142e+05	1.858e+04
2	2	-79.40	-2.951e+04	-193.92	8276.73	-6.763e+05	2.144e+05	1.565e+04
2	2	-79.17	-2.951e+04	-190.00	8354.61	-6.745e+05	2.166e+05	1.662e+04
2	2	-79.05	-2.950e+04	-190.43	8399.69	-6.713e+05	2.181e+05	1.805e+04
2	2	-78.83	-2.947e+04	-111.80	8412.89	-6.637e+05	2.188e+05	2.044e+04
2	2	-78.69	-2.948e+04	-67.40	8420.61	-6.648e+05	2.176e+05	2.087e+04
2	2	-78.33	-2.936e+04	-27.08	8624.48	-6.312e+05	2.201e+05	2.021e+04
2	2	-40.00	-3.237e+04	-251.93	1.351e+04	-7.052e+05	6.449e+05	9231.51
2	5	-305.00	-2767.46	-649.18	770.98	-1622.36	-3.224e+04	-1002.25
2	5	-270.00	-3084.98	-684.30	1406.18	-1.728e+04	5872.19	-2768.12
2	5	-231.67	-9104.13	-675.49	-5072.40	2.391e+04	3511.48	2558.58

SCARICATORE IN VIA PUCCI

2	5	-231.67	-9104.13	-675.49	-5072.40	2.391e+04	3511.48	2558.58
2	5	-193.33	-7962.38	-652.98	-2494.09	1.912e+05	-6.739e+04	2865.76
2	5	-193.33	-7962.38	-652.98	-2494.09	1.912e+05	-6.739e+04	2865.76
2	5	-155.00	-7199.96	-607.24	-993.28	2.473e+05	-7.022e+04	433.47
2	5	-116.67	-6687.32	-535.53	200.83	1.886e+05	-3.676e+04	-1568.52
2	5	-116.67	-6687.32	-535.53	200.83	1.886e+05	-3.676e+04	-1568.52
2	5	-82.18	-6420.58	-536.01	1738.07	8.141e+04	2.585e+04	-1223.25
2	5	-81.84	-6331.60	-538.33	1951.88	6.329e+04	2.712e+04	-894.82
2	5	-81.50	-6250.00	-539.52	2134.92	4.914e+04	2.670e+04	-1233.88
2	5	-81.16	-6172.13	-540.14	2338.20	3.812e+04	2.708e+04	-1883.48
2	5	-80.81	-6097.81	-540.44	2535.78	3.025e+04	2.769e+04	-2165.77
2	5	-80.47	-6023.87	-534.83	2710.28	2.543e+04	2.752e+04	-1733.99
2	5	-80.12	-5946.19	-541.75	2870.47	2.353e+04	2.843e+04	-1473.10
2	5	-80.00	-5921.25	-565.95	2894.99	2.378e+04	2.834e+04	-1515.84
2	5	-79.89	-5901.77	-590.63	2897.48	2.471e+04	2.846e+04	-1726.24
2	5	-79.76	-5876.03	-597.59	2907.31	2.643e+04	2.863e+04	-1866.19
2	5	-79.40	-5814.48	-613.15	2906.70	3.197e+04	2.912e+04	-2610.23
2	5	-79.17	-5783.53	-608.02	2924.02	3.597e+04	2.988e+04	-2532.25
2	5	-79.05	-5759.35	-605.19	2934.46	3.964e+04	3.031e+04	-2314.02
2	5	-78.83	-5723.35	-571.80	2935.37	4.601e+04	3.055e+04	-1957.17
2	5	-78.69	-5697.18	-549.95	2968.21	5.113e+04	3.030e+04	-1898.91
2	5	-78.33	-5623.22	-534.63	3086.91	6.792e+04	3.118e+04	-2261.30
2	5	-40.00	-6554.82	-635.37	4418.47	-3.902e+04	1.747e+05	-614.24
2	8	-305.00	-5170.03	-902.31	-970.76	-8920.39	-2.782e+04	685.09
2	8	-270.00	-5258.97	-786.85	-1753.88	-5.137e+04	-7.547e+04	-7894.27
2	8	-231.67	-2.792e+04	-721.24	-6166.69	-4.914e+05	4.806e+04	-1.445e+04
2	8	-231.67	-2.792e+04	-721.24	-6166.69	-4.914e+05	4.806e+04	-1.445e+04
2	8	-193.33	-2.668e+04	-579.39	-2573.13	-4.441e+05	-4.243e+04	-4884.29
2	8	-193.33	-2.668e+04	-579.39	-2573.13	-4.441e+05	-4.243e+04	-4884.29
2	8	-155.00	-2.633e+04	-514.49	-467.31	-4.708e+05	-3.672e+04	1487.82
2	8	-116.67	-2.682e+04	-344.95	1860.01	-5.788e+05	3.582e+04	9284.86
2	8	-116.67	-2.682e+04	-344.95	1860.01	-5.788e+05	3.582e+04	9284.86
2	8	-82.18	-2.821e+04	-88.00	5752.00	-6.654e+05	1.939e+05	1.859e+04
2	8	-81.84	-2.816e+04	-36.76	6001.19	-6.792e+05	1.971e+05	1.420e+04
2	8	-81.50	-2.809e+04	-20.76	6191.24	-6.931e+05	1.963e+05	9595.21
2	8	-81.16	-2.803e+04	-9.67	6458.06	-7.025e+05	1.985e+05	6642.87
2	8	-80.81	-2.799e+04	-28.46	6733.13	-7.074e+05	2.013e+05	6911.16
2	8	-80.47	-2.796e+04	-32.42	6947.18	-7.076e+05	2.004e+05	1.206e+04
2	8	-80.12	-2.795e+04	31.98	7231.76	-7.045e+05	2.040e+05	1.873e+04
2	8	-80.00	-2.794e+04	34.91	7334.84	-7.024e+05	2.046e+05	1.948e+04
2	8	-79.89	-2.790e+04	-22.98	7404.17	-6.994e+05	2.060e+05	1.931e+04
2	8	-79.76	-2.790e+04	-55.58	7432.42	-6.990e+05	2.064e+05	1.908e+04
2	8	-79.40	-2.781e+04	-122.31	7412.53	-6.897e+05	2.064e+05	1.637e+04
2	8	-79.17	-2.782e+04	-119.95	7485.04	-6.891e+05	2.084e+05	1.732e+04
2	8	-79.05	-2.782e+04	-121.29	7526.83	-6.870e+05	2.098e+05	1.868e+04
2	8	-78.83	-2.780e+04	-53.16	7540.81	-6.812e+05	2.105e+05	2.096e+04
2	8	-78.69	-2.782e+04	-15.45	7540.63	-6.840e+05	2.094e+05	2.137e+04
2	8	-78.33	-2.772e+04	21.02	7708.74	-6.556e+05	2.116e+05	2.083e+04
2	8	-40.00	-3.042e+04	-174.20	1.215e+04	-6.955e+05	5.929e+05	9429.12
2	24	-305.00	-3530.56	-1330.09	109.90	-1.258e+04	-2.916e+04	-735.92
2	24	-270.00	-3657.45	-1284.96	-18.50	-4.344e+04	-3.631e+04	-6985.85
2	24	-231.67	-1.846e+04	-3853.09	-6424.63	-9.607e+04	5.446e+04	-8311.95
2	24	-231.67	-1.846e+04	-3853.09	-6424.63	-9.607e+04	5.446e+04	-8311.95
2	24	-193.33	-1.749e+04	-3725.92	-2766.48	-3.726e+04	-4.562e+04	-333.44
2	24	-193.33	-1.749e+04	-3725.92	-2766.48	-3.726e+04	-4.562e+04	-333.44
2	24	-155.00	-1.713e+04	-3476.26	-851.29	-2.810e+04	-5.161e+04	3208.42
2	24	-116.67	-1.728e+04	-3074.74	990.46	-1.286e+05	1649.95	6616.16
2	24	-116.67	-1.728e+04	-3074.74	990.46	-1.286e+05	1649.95	6616.16
2	24	-82.18	-1.825e+04	-2594.45	3836.14	-1.918e+05	1.078e+05	1.164e+04
2	24	-81.84	-1.816e+04	-2516.68	4099.11	-2.124e+05	1.106e+05	9560.24
2	24	-81.50	-1.805e+04	-2457.42	4300.71	-2.320e+05	1.099e+05	7031.71
2	24	-81.16	-1.795e+04	-2390.78	4548.67	-2.476e+05	1.111e+05	5177.91
2	24	-80.81	-1.785e+04	-2328.81	4798.15	-2.592e+05	1.125e+05	5180.01
2	24	-80.47	-1.774e+04	-2248.45	4984.69	-2.674e+05	1.113e+05	8092.96
2	24	-80.12	-1.765e+04	-2153.14	5198.57	-2.726e+05	1.133e+05	1.155e+04
2	24	-80.00	-1.762e+04	-2149.91	5255.40	-2.731e+05	1.135e+05	1.190e+04
2	24	-79.89	-1.758e+04	-2188.50	5278.63	-2.707e+05	1.141e+05	1.171e+04
2	24	-79.76	-1.757e+04	-2205.11	5289.44	-2.696e+05	1.141e+05	1.157e+04
2	24	-79.40	-1.750e+04	-2243.66	5260.51	-2.629e+05	1.135e+05	9565.20
2	24	-79.17	-1.750e+04	-2239.15	5300.13	-2.617e+05	1.143e+05	1.010e+04
2	24	-79.05	-1.749e+04	-2237.72	5326.78	-2.593e+05	1.152e+05	1.090e+04
2	24	-78.83	-1.751e+04	-2181.06	5337.16	-2.606e+05	1.158e+05	1.230e+04
2	24	-78.69	-1.756e+04	-2138.08	5346.93	-2.691e+05	1.151e+05	1.256e+04
2	24	-78.33	-1.752e+04	-2067.60	5470.91	-2.561e+05	1.169e+05	1.203e+04
2	24	-40.00	-1.948e+04	-2219.14	8475.51	-3.072e+05	3.878e+05	6910.40
2	28	-305.00	-3330.29	-598.69	-875.71	-1950.47	-3.481e+04	-862.44
2	28	-270.00	-3415.14	-553.56	-1004.11	-3.112e+04	-4.189e+04	-6932.32
2	28	-231.67	-1.713e+04	-1802.32	-6822.86	-3.006e+05	6.280e+04	-5248.50
2	28	-231.67	-1.713e+04	-1802.32	-6822.86	-3.006e+05	6.280e+04	-5248.50

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

2	28	-193.33	-1.623e+04	-1665.22	-2868.53	-1.697e+05	-4.612e+04	1551.92
2	28	-193.33	-1.623e+04	-1665.22	-2868.53	-1.697e+05	-4.612e+04	1551.92
2	28	-155.00	-1.618e+04	-1519.91	-849.52	-1.159e+05	-5.508e+04	5016.24
2	28	-116.67	-1.677e+04	-1287.74	995.44	-1.446e+05	-2838.50	7484.36
2	28	-116.67	-1.677e+04	-1287.74	995.44	-1.446e+05	-2838.50	7484.36
2	28	-82.18	-1.772e+04	-1051.34	3805.47	-2.381e+05	1.078e+05	1.137e+04
2	28	-81.84	-1.765e+04	-977.79	4058.85	-2.542e+05	1.106e+05	9326.59
2	28	-81.50	-1.760e+04	-922.24	4257.49	-2.663e+05	1.103e+05	6945.84
2	28	-81.16	-1.754e+04	-863.56	4513.91	-2.768e+05	1.116e+05	5117.16
2	28	-80.81	-1.748e+04	-814.06	4777.00	-2.852e+05	1.129e+05	5084.09
2	28	-80.47	-1.738e+04	-748.40	4974.24	-2.913e+05	1.115e+05	7734.73
2	28	-80.12	-1.729e+04	-664.86	5193.02	-2.942e+05	1.133e+05	1.081e+04
2	28	-80.00	-1.727e+04	-661.38	5252.72	-2.943e+05	1.135e+05	1.109e+04
2	28	-79.89	-1.724e+04	-715.48	5278.71	-2.924e+05	1.142e+05	1.090e+04
2	28	-79.76	-1.722e+04	-747.18	5292.81	-2.913e+05	1.144e+05	1.077e+04
2	28	-79.40	-1.716e+04	-815.70	5269.57	-2.847e+05	1.143e+05	8999.45
2	28	-79.17	-1.716e+04	-824.58	5316.45	-2.831e+05	1.155e+05	9539.36
2	28	-79.05	-1.714e+04	-830.11	5348.57	-2.804e+05	1.163e+05	1.035e+04
2	28	-78.83	-1.713e+04	-795.34	5357.92	-2.761e+05	1.166e+05	1.170e+04
2	28	-78.69	-1.713e+04	-793.80	5370.51	-2.754e+05	1.158e+05	1.192e+04
2	28	-78.33	-1.706e+04	-856.21	5497.46	-2.555e+05	1.171e+05	1.131e+04
2	28	-40.00	-1.917e+04	-1014.70	8504.63	-3.444e+05	3.880e+05	5924.47
2	39	-305.00	-4748.23	-1037.88	700.46	-7261.78	-2.349e+04	151.23
2	39	-270.00	-5029.06	-992.75	572.07	-3.661e+04	-3.064e+04	-4721.10
2	39	-231.67	-2.091e+04	-909.96	-4574.81	-9.221e+04	-3533.58	-1.035e+04
2	39	-231.67	-2.091e+04	-909.96	-4574.81	-9.221e+04	-3533.58	-1.035e+04
2	39	-193.33	-1.949e+04	-854.47	-2235.71	-4.565e+04	-5.940e+04	-5616.82
2	39	-193.33	-1.949e+04	-854.47	-2235.71	-4.565e+04	-5.940e+04	-5616.82
2	39	-155.00	-1.849e+04	-800.34	-612.45	-9.054e+04	-4.836e+04	-3463.09
2	39	-116.67	-1.795e+04	-652.25	1138.89	-2.559e+05	8556.38	690.94
2	39	-116.67	-1.795e+04	-652.25	1138.89	-2.559e+05	8556.38	690.94
2	39	-82.18	-1.832e+04	-450.69	3935.58	-3.595e+05	1.224e+05	7873.70
2	39	-81.84	-1.823e+04	-457.08	4150.63	-3.794e+05	1.242e+05	5574.13
2	39	-81.50	-1.812e+04	-480.35	4321.83	-3.984e+05	1.234e+05	2768.72
2	39	-81.16	-1.803e+04	-510.37	4532.03	-4.099e+05	1.248e+05	866.82
2	39	-80.81	-1.797e+04	-558.45	4749.50	-4.143e+05	1.267e+05	980.05
2	39	-80.47	-1.795e+04	-593.13	4943.33	-4.127e+05	1.265e+05	4069.49
2	39	-80.12	-1.795e+04	-585.77	5185.02	-4.070e+05	1.291e+05	8172.71
2	39	-80.00	-1.795e+04	-600.15	5257.94	-4.037e+05	1.294e+05	8589.26
2	39	-79.89	-1.791e+04	-624.88	5306.17	-4.014e+05	1.303e+05	8405.46
2	39	-79.76	-1.790e+04	-629.60	5333.04	-4.004e+05	1.308e+05	8177.06
2	39	-79.40	-1.782e+04	-638.26	5337.23	-3.925e+05	1.314e+05	6286.08
2	39	-79.17	-1.781e+04	-618.24	5380.51	-3.905e+05	1.329e+05	6837.03
2	39	-79.05	-1.780e+04	-609.55	5402.13	-3.880e+05	1.339e+05	7695.63
2	39	-78.83	-1.779e+04	-533.77	5408.57	-3.852e+05	1.345e+05	9143.57
2	39	-78.69	-1.781e+04	-463.98	5420.93	-3.873e+05	1.339e+05	9428.63
2	39	-78.33	-1.772e+04	-315.62	5571.92	-3.630e+05	1.360e+05	9101.07
2	39	-40.00	-1.944e+04	-459.23	8594.39	-4.060e+05	4.065e+05	3774.95
2	40	-305.00	-3384.51	-852.29	-703.26	-7627.30	-3.508e+04	-699.36
2	40	-270.00	-3483.95	-807.16	-831.65	-3.775e+04	-4.217e+04	-6990.83
2	40	-231.67	-1.705e+04	-2178.77	-6978.65	-3.151e+05	6.806e+04	-4127.56
2	40	-231.67	-1.705e+04	-2178.77	-6978.65	-3.151e+05	6.806e+04	-4127.56
2	40	-193.33	-1.624e+04	-2041.72	-2917.98	-1.838e+05	-4.492e+04	3123.99
2	40	-193.33	-1.624e+04	-2041.72	-2917.98	-1.838e+05	-4.492e+04	3123.99
2	40	-155.00	-1.623e+04	-1876.81	-878.31	-1.198e+05	-5.541e+04	6182.84
2	40	-116.67	-1.684e+04	-1620.32	982.20	-1.405e+05	-4090.37	8668.69
2	40	-116.67	-1.684e+04	-1620.32	982.20	-1.405e+05	-4090.37	8668.69
2	40	-82.18	-1.788e+04	-1348.59	3803.39	-2.096e+05	1.049e+05	1.190e+04
2	40	-81.84	-1.782e+04	-1267.55	4067.46	-2.245e+05	1.079e+05	9864.27
2	40	-81.50	-1.776e+04	-1205.51	4275.65	-2.376e+05	1.073e+05	7462.36
2	40	-81.16	-1.769e+04	-1136.49	4541.17	-2.495e+05	1.086e+05	5621.68
2	40	-80.81	-1.762e+04	-1075.17	4803.84	-2.602e+05	1.101e+05	5541.78
2	40	-80.47	-1.751e+04	-1000.48	4996.03	-2.692e+05	1.089e+05	8345.84
2	40	-80.12	-1.740e+04	-913.94	5202.51	-2.759e+05	1.108e+05	1.154e+04
2	40	-80.00	-1.737e+04	-912.59	5257.18	-2.773e+05	1.110e+05	1.186e+04
2	40	-79.89	-1.734e+04	-967.75	5278.11	-2.753e+05	1.116e+05	1.167e+04
2	40	-79.76	-1.733e+04	-999.48	5286.99	-2.742e+05	1.116e+05	1.154e+04
2	40	-79.40	-1.726e+04	-1068.61	5253.88	-2.675e+05	1.110e+05	9712.56
2	40	-79.17	-1.725e+04	-1078.14	5299.73	-2.657e+05	1.121e+05	1.025e+04
2	40	-79.05	-1.724e+04	-1083.78	5331.36	-2.628e+05	1.129e+05	1.103e+04
2	40	-78.83	-1.722e+04	-1048.81	5341.03	-2.581e+05	1.133e+05	1.237e+04
2	40	-78.69	-1.724e+04	-1044.38	5354.17	-2.597e+05	1.125e+05	1.259e+04
2	40	-78.33	-1.718e+04	-1095.84	5482.78	-2.432e+05	1.138e+05	1.198e+04
2	40	-40.00	-1.925e+04	-1253.02	8484.85	-3.285e+05	3.846e+05	6733.17
2	56	-305.00	-3784.16	-1108.38	3.19	-9898.07	-2.960e+04	-503.44
2	56	-270.00	-3943.08	-1063.25	-125.21	-4.021e+04	-3.672e+04	-6433.02
2	56	-231.67	-1.862e+04	-2626.25	-6132.93	-1.616e+05	4.429e+04	-7556.77
2	56	-231.67	-1.862e+04	-2626.25	-6132.93	-1.616e+05	4.429e+04	-7556.77
2	56	-193.33	-1.758e+04	-2509.17	-2681.45	-8.367e+04	-4.873e+04	-635.85

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

2	56	-193.33	-1.758e+04	-2509.17	-2681.45	-8.367e+04	-4.873e+04	-635.85
2	56	-155.00	-1.717e+04	-2332.08	-800.44	-7.143e+04	-5.195e+04	2429.24
2	56	-116.67	-1.730e+04	-2038.40	1025.24	-1.633e+05	1632.93	5769.51
2	56	-116.67	-1.730e+04	-2038.40	1025.24	-1.633e+05	1632.93	5769.51
2	56	-82.18	-1.815e+04	-1691.28	3851.49	-2.390e+05	1.107e+05	1.080e+04
2	56	-81.84	-1.806e+04	-1632.16	4102.62	-2.578e+05	1.133e+05	8678.51
2	56	-81.50	-1.797e+04	-1591.39	4298.59	-2.751e+05	1.126e+05	6117.84
2	56	-81.16	-1.788e+04	-1546.50	4542.13	-2.884e+05	1.139e+05	4256.16
2	56	-80.81	-1.780e+04	-1510.27	4787.55	-2.979e+05	1.155e+05	4258.30
2	56	-80.47	-1.771e+04	-1458.61	4977.70	-3.039e+05	1.145e+05	7175.95
2	56	-80.12	-1.764e+04	-1387.11	5196.30	-3.067e+05	1.166e+05	1.071e+04
2	56	-80.00	-1.762e+04	-1389.16	5256.47	-3.064e+05	1.169e+05	1.106e+04
2	56	-79.89	-1.758e+04	-1429.92	5285.13	-3.042e+05	1.176e+05	1.087e+04
2	56	-79.76	-1.757e+04	-1448.68	5299.32	-3.031e+05	1.177e+05	1.072e+04
2	56	-79.40	-1.750e+04	-1490.20	5277.34	-2.962e+05	1.174e+05	8794.42
2	56	-79.17	-1.750e+04	-1486.58	5319.75	-2.946e+05	1.184e+05	9334.68
2	56	-79.05	-1.748e+04	-1485.71	5346.68	-2.921e+05	1.194e+05	1.014e+04
2	56	-78.83	-1.749e+04	-1431.47	5355.95	-2.908e+05	1.199e+05	1.154e+04
2	56	-78.69	-1.752e+04	-1394.32	5367.41	-2.958e+05	1.192e+05	1.179e+04
2	56	-78.33	-1.746e+04	-1343.89	5499.48	-2.791e+05	1.209e+05	1.129e+04
2	56	-40.00	-1.940e+04	-1495.43	8507.90	-3.379e+05	3.916e+05	6058.54
2	60	-305.00	-3672.95	-684.29	-568.17	-3426.76	-3.281e+04	-569.67
2	60	-270.00	-3808.60	-639.16	-696.57	-3.272e+04	-3.989e+04	-6386.16
2	60	-231.67	-1.787e+04	-1415.25	-6347.86	-2.775e+05	4.857e+04	-5790.12
2	60	-231.67	-1.787e+04	-1415.25	-6347.86	-2.775e+05	4.857e+04	-5790.12
2	60	-193.33	-1.686e+04	-1303.64	-2737.06	-1.580e+05	-4.917e+04	443.73
2	60	-193.33	-1.686e+04	-1303.64	-2737.06	-1.580e+05	-4.917e+04	443.73
2	60	-155.00	-1.663e+04	-1195.26	-796.94	-1.211e+05	-5.407e+04	3436.37
2	60	-116.67	-1.700e+04	-1003.63	1030.04	-1.719e+05	-1008.85	6229.67
2	60	-116.67	-1.700e+04	-1003.63	1030.04	-1.719e+05	-1008.85	6229.67
2	60	-82.18	-1.784e+04	-798.48	3834.98	-2.663e+05	1.108e+05	1.060e+04
2	60	-81.84	-1.777e+04	-742.33	4079.89	-2.826e+05	1.134e+05	8495.79
2	60	-81.50	-1.770e+04	-704.21	4273.69	-2.957e+05	1.130e+05	6027.95
2	60	-81.16	-1.764e+04	-664.39	4522.04	-3.061e+05	1.143e+05	4180.95
2	60	-80.81	-1.758e+04	-635.84	4775.39	-3.137e+05	1.158e+05	4168.86
2	60	-80.47	-1.750e+04	-593.13	4971.89	-3.183e+05	1.148e+05	6935.26
2	60	-80.12	-1.743e+04	-528.60	5193.60	-3.197e+05	1.168e+05	1.023e+04
2	60	-80.00	-1.741e+04	-530.61	5255.65	-3.193e+05	1.170e+05	1.055e+04
2	60	-79.89	-1.738e+04	-579.40	5286.24	-3.173e+05	1.178e+05	1.036e+04
2	60	-79.76	-1.737e+04	-606.12	5302.56	-3.163e+05	1.180e+05	1.020e+04
2	60	-79.40	-1.730e+04	-663.40	5284.29	-3.094e+05	1.180e+05	8423.00
2	60	-79.17	-1.730e+04	-666.91	5330.95	-3.076e+05	1.193e+05	8963.86
2	60	-79.05	-1.728e+04	-669.80	5361.06	-3.049e+05	1.202e+05	9780.53
2	60	-78.83	-1.726e+04	-627.58	5369.60	-3.002e+05	1.205e+05	1.115e+04
2	60	-78.69	-1.727e+04	-613.63	5382.66	-2.996e+05	1.197e+05	1.138e+04
2	60	-78.33	-1.719e+04	-637.73	5516.77	-2.786e+05	1.212e+05	1.083e+04
2	60	-40.00	-1.921e+04	-792.96	8526.85	-3.604e+05	3.920e+05	5460.38
2	65	-305.00	-4734.67	-726.02	243.04	-5224.12	-2.733e+04	179.43
2	65	-270.00	-5005.06	-680.89	114.64	-3.415e+04	-3.444e+04	-4647.13
2	65	-231.67	-2.011e+04	306.18	-4901.03	-2.434e+05	3997.38	-7469.27
2	65	-231.67	-2.011e+04	306.18	-4901.03	-2.434e+05	3997.38	-7469.27
2	65	-193.33	-1.877e+04	379.53	-2315.25	-1.491e+05	-5.951e+04	-3159.65
2	65	-193.33	-1.877e+04	379.53	-2315.25	-1.491e+05	-5.951e+04	-3159.65
2	65	-155.00	-1.797e+04	379.70	-622.06	-1.577e+05	-5.075e+04	-1672.66
2	65	-116.67	-1.770e+04	428.70	1135.40	-2.724e+05	4855.84	1943.88
2	65	-116.67	-1.770e+04	428.70	1135.40	-2.724e+05	4855.84	1943.88
2	65	-82.18	-1.814e+04	485.33	3911.96	-3.693e+05	1.197e+05	8097.60
2	65	-81.84	-1.808e+04	477.07	4130.56	-3.845e+05	1.216e+05	5831.26
2	65	-81.50	-1.799e+04	451.79	4304.88	-3.992e+05	1.207e+05	3095.46
2	65	-81.16	-1.793e+04	419.02	4524.90	-4.087e+05	1.220e+05	1186.38
2	65	-80.81	-1.787e+04	365.55	4747.82	-4.131e+05	1.241e+05	1245.57
2	65	-80.47	-1.786e+04	322.08	4945.38	-4.126e+05	1.240e+05	4255.45
2	65	-80.12	-1.785e+04	320.17	5185.18	-4.089e+05	1.267e+05	8213.43
2	65	-80.00	-1.784e+04	304.12	5257.27	-4.065e+05	1.271e+05	8615.61
2	65	-79.89	-1.780e+04	268.25	5304.75	-4.044e+05	1.279e+05	8428.15
2	65	-79.76	-1.779e+04	253.44	5330.16	-4.034e+05	1.284e+05	8205.08
2	65	-79.40	-1.771e+04	224.59	5330.80	-3.953e+05	1.289e+05	6398.25
2	65	-79.17	-1.770e+04	235.50	5378.88	-3.928e+05	1.305e+05	6945.35
2	65	-79.05	-1.768e+04	239.66	5403.52	-3.899e+05	1.315e+05	7792.70
2	65	-78.83	-1.765e+04	301.76	5409.26	-3.827e+05	1.321e+05	9206.87
2	65	-78.69	-1.765e+04	347.21	5423.96	-3.816e+05	1.314e+05	9473.06
2	65	-78.33	-1.755e+04	418.65	5578.93	-3.564e+05	1.332e+05	9097.53
2	65	-40.00	-1.932e+04	271.77	8598.35	-4.193e+05	4.035e+05	3812.53
2	72	-305.00	-3702.30	-831.30	-471.94	-6864.16	-3.299e+04	-477.19
2	72	-270.00	-3846.17	-786.17	-600.34	-3.673e+04	-4.008e+04	-6424.95
2	72	-231.67	-1.781e+04	-1650.85	-6448.08	-2.870e+05	5.192e+04	-5128.84
2	72	-231.67	-1.781e+04	-1650.85	-6448.08	-2.870e+05	5.192e+04	-5128.84
2	72	-193.33	-1.686e+04	-1538.72	-2768.41	-1.671e+05	-4.842e+04	1363.03
2	72	-193.33	-1.686e+04	-1538.72	-2768.41	-1.671e+05	-4.842e+04	1363.03

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

2	72	-155.00	-1.665e+04	-1417.42	-814.86	-1.238e+05	-5.427e+04	4146.23
2	72	-116.67	-1.705e+04	-1210.23	1021.60	-1.694e+05	-1751.19	6951.99
2	72	-116.67	-1.705e+04	-1210.23	1021.60	-1.694e+05	-1751.19	6951.99
2	72	-82.18	-1.793e+04	-983.61	3833.32	-2.493e+05	1.091e+05	1.091e+04
2	72	-81.84	-1.786e+04	-922.85	4084.72	-2.649e+05	1.118e+05	8817.55
2	72	-81.50	-1.780e+04	-880.76	4284.58	-2.786e+05	1.112e+05	6335.71
2	72	-81.16	-1.773e+04	-834.86	4538.72	-2.899e+05	1.125e+05	4481.29
2	72	-80.81	-1.766e+04	-799.38	4791.95	-2.988e+05	1.142e+05	4440.65
2	72	-80.47	-1.758e+04	-751.34	4985.45	-3.051e+05	1.132e+05	7308.88
2	72	-80.12	-1.749e+04	-685.18	5199.68	-3.088e+05	1.153e+05	1.068e+04
2	72	-80.00	-1.747e+04	-688.40	5258.64	-3.091e+05	1.155e+05	1.103e+04
2	72	-79.89	-1.744e+04	-737.84	5286.12	-3.071e+05	1.162e+05	1.083e+04
2	72	-79.76	-1.743e+04	-764.66	5299.30	-3.061e+05	1.163e+05	1.068e+04
2	72	-79.40	-1.736e+04	-822.50	5275.07	-2.991e+05	1.160e+05	8867.85
2	72	-79.17	-1.735e+04	-826.45	5321.16	-2.972e+05	1.172e+05	9405.24
2	72	-79.05	-1.734e+04	-829.45	5351.01	-2.944e+05	1.181e+05	1.021e+04
2	72	-78.83	-1.732e+04	-787.18	5359.71	-2.894e+05	1.185e+05	1.157e+04
2	72	-78.69	-1.733e+04	-771.80	5373.09	-2.902e+05	1.177e+05	1.180e+04
2	72	-78.33	-1.726e+04	-790.38	5508.10	-2.714e+05	1.192e+05	1.125e+04
2	72	-40.00	-1.926e+04	-944.90	8515.10	-3.508e+05	3.899e+05	5948.13
2	73	-305.00	-2926.97	-633.15	789.59	-1374.66	-3.245e+04	-1030.72
2	73	-270.00	-3254.45	-668.33	1417.63	-1.639e+04	6198.17	-2783.69
2	73	-231.67	-8925.65	-612.08	-5069.97	1.076e+04	3596.19	2693.43
2	73	-231.67	-8925.65	-612.08	-5069.97	1.076e+04	3596.19	2693.43
2	73	-193.33	-7828.98	-587.45	-2497.28	1.820e+05	-6.735e+04	3057.57
2	73	-193.33	-7828.98	-587.45	-2497.28	1.820e+05	-6.735e+04	3057.57
2	73	-155.00	-7107.28	-541.09	-997.60	2.428e+05	-7.032e+04	625.42
2	73	-116.67	-6631.59	-469.39	195.61	1.886e+05	-3.704e+04	-1425.66
2	73	-116.67	-6631.59	-469.39	195.61	1.886e+05	-3.704e+04	-1425.66
2	73	-82.18	-6390.65	-469.95	1734.52	8.369e+04	2.541e+04	-1172.93
2	73	-81.84	-6301.66	-472.91	1948.32	6.554e+04	2.668e+04	-844.25
2	73	-81.50	-6220.38	-474.29	2131.56	5.142e+04	2.626e+04	-1179.46
2	73	-81.16	-6142.73	-474.87	2334.75	4.040e+04	2.663e+04	-1826.18
2	73	-80.81	-6068.70	-475.08	2532.37	3.253e+04	2.725e+04	-2109.33
2	73	-80.47	-5994.85	-468.81	2706.96	2.770e+04	2.708e+04	-1679.67
2	73	-80.12	-5917.01	-475.53	2866.81	2.577e+04	2.797e+04	-1431.56
2	73	-80.00	-5891.98	-499.69	2890.52	2.602e+04	2.787e+04	-1478.08
2	73	-79.89	-5872.72	-524.45	2892.56	2.694e+04	2.798e+04	-1689.76
2	73	-79.76	-5846.99	-531.43	2902.48	2.866e+04	2.815e+04	-1830.71
2	73	-79.40	-5785.56	-547.07	2902.10	3.420e+04	2.865e+04	-2572.82
2	73	-79.17	-5754.76	-541.93	2919.52	3.819e+04	2.940e+04	-2494.10
2	73	-79.05	-5730.67	-539.07	2930.06	4.185e+04	2.983e+04	-2275.31
2	73	-78.83	-5694.82	-505.39	2930.35	4.821e+04	3.005e+04	-1917.18
2	73	-78.69	-5668.26	-483.46	2962.04	5.341e+04	2.979e+04	-1857.52
2	73	-78.33	-5594.15	-468.58	3080.83	7.026e+04	3.067e+04	-2227.50
2	73	-40.00	-6545.37	-568.97	4437.40	-3.785e+04	1.745e+05	-622.09
2	74	-305.00	-4464.87	-808.31	-379.01	-6339.09	-2.942e+04	105.56
2	74	-270.00	-4635.99	-743.08	-693.65	-3.947e+04	-4.816e+04	-6194.90
2	74	-231.67	-2.154e+04	-667.95	-5800.47	-3.275e+05	3.326e+04	-8700.37
2	74	-231.67	-2.154e+04	-667.95	-5800.47	-3.275e+05	3.326e+04	-8700.37
2	74	-193.33	-2.036e+04	-564.61	-2548.70	-2.378e+05	-5.072e+04	-2185.85
2	74	-193.33	-2.036e+04	-564.61	-2548.70	-2.378e+05	-5.072e+04	-2185.85
2	74	-155.00	-1.990e+04	-505.72	-645.22	-2.341e+05	-4.795e+04	1251.54
2	74	-116.67	-2.008e+04	-368.80	1303.82	-3.230e+05	1.146e+04	5752.78
2	74	-116.67	-2.008e+04	-368.80	1303.82	-3.230e+05	1.146e+04	5752.78
2	74	-82.18	-2.093e+04	-197.70	4411.89	-4.151e+05	1.376e+05	1.202e+04
2	74	-81.84	-2.086e+04	-164.70	4649.29	-4.303e+05	1.402e+05	9198.30
2	74	-81.50	-2.079e+04	-154.55	4837.11	-4.443e+05	1.395e+05	6018.17
2	74	-81.16	-2.073e+04	-147.33	5082.71	-4.542e+05	1.411e+05	3835.14
2	74	-80.81	-2.067e+04	-159.91	5331.97	-4.601e+05	1.432e+05	3919.38
2	74	-80.47	-2.063e+04	-160.28	5532.89	-4.619e+05	1.425e+05	7491.42
2	74	-80.12	-2.060e+04	-119.53	5775.80	-4.605e+05	1.452e+05	1.202e+04
2	74	-80.00	-2.059e+04	-125.62	5852.21	-4.590e+05	1.456e+05	1.250e+04
2	74	-79.89	-2.055e+04	-172.49	5898.99	-4.567e+05	1.465e+05	1.232e+04
2	74	-79.76	-2.054e+04	-196.56	5921.15	-4.558e+05	1.469e+05	1.212e+04
2	74	-79.40	-2.046e+04	-246.28	5907.83	-4.478e+05	1.470e+05	1.006e+04
2	74	-79.17	-2.046e+04	-242.99	5962.00	-4.461e+05	1.486e+05	1.072e+04
2	74	-79.05	-2.045e+04	-242.91	5993.40	-4.434e+05	1.497e+05	1.170e+04
2	74	-78.83	-2.042e+04	-186.19	6002.65	-4.375e+05	1.502e+05	1.334e+04
2	74	-78.69	-2.043e+04	-153.72	6012.79	-4.376e+05	1.494e+05	1.364e+04
2	74	-78.33	-2.034e+04	-124.56	6164.48	-4.130e+05	1.512e+05	1.315e+04
2	74	-40.00	-2.246e+04	-288.08	9583.14	-4.760e+05	4.534e+05	6076.62
2	76	-305.00	-4528.68	-801.90	-371.57	-6240.01	-2.950e+04	94.17
2	76	-270.00	-4703.78	-736.69	-689.07	-3.911e+04	-4.803e+04	-6201.13
2	76	-231.67	-2.147e+04	-642.58	-5799.50	-3.328e+05	3.330e+04	-8646.43
2	76	-231.67	-2.147e+04	-642.58	-5799.50	-3.328e+05	3.330e+04	-8646.43
2	76	-193.33	-2.031e+04	-538.39	-2549.97	-2.415e+05	-5.071e+04	-2109.12
2	76	-193.33	-2.031e+04	-538.39	-2549.97	-2.415e+05	-5.071e+04	-2109.12
2	76	-155.00	-1.986e+04	-479.26	-646.95	-2.359e+05	-4.799e+04	1328.31

SCARICATORE IN VIA PUCCI

2	76	-116.67	-2.006e+04	-342.34	1301.73	-3.229e+05	1.135e+04	5809.92
2	76	-116.67	-2.006e+04	-342.34	1301.73	-3.229e+05	1.135e+04	5809.92
2	76	-82.18	-2.092e+04	-171.28	4410.47	-4.142e+05	1.374e+05	1.204e+04
2	76	-81.84	-2.085e+04	-138.53	4647.86	-4.294e+05	1.400e+05	9218.53
2	76	-81.50	-2.078e+04	-128.46	4835.77	-4.434e+05	1.393e+05	6039.94
2	76	-81.16	-2.072e+04	-121.23	5081.33	-4.533e+05	1.409e+05	3858.06
2	76	-80.81	-2.066e+04	-133.76	5330.61	-4.592e+05	1.430e+05	3941.96
2	76	-80.47	-2.062e+04	-133.87	5531.56	-4.610e+05	1.423e+05	7513.15
2	76	-80.12	-2.059e+04	-93.05	5774.34	-4.596e+05	1.450e+05	1.204e+04
2	76	-80.00	-2.057e+04	-99.11	5850.42	-4.581e+05	1.454e+05	1.252e+04
2	76	-79.89	-2.054e+04	-146.01	5897.02	-4.558e+05	1.463e+05	1.233e+04
2	76	-79.76	-2.053e+04	-170.09	5919.22	-4.549e+05	1.467e+05	1.213e+04
2	76	-79.40	-2.045e+04	-219.85	5905.99	-4.469e+05	1.469e+05	1.008e+04
2	76	-79.17	-2.045e+04	-216.55	5960.21	-4.452e+05	1.484e+05	1.074e+04
2	76	-79.05	-2.044e+04	-216.46	5991.64	-4.426e+05	1.495e+05	1.172e+04
2	76	-78.83	-2.041e+04	-159.63	6000.64	-4.366e+05	1.500e+05	1.336e+04
2	76	-78.69	-2.042e+04	-127.13	6010.32	-4.367e+05	1.492e+05	1.366e+04
2	76	-78.33	-2.033e+04	-98.14	6162.05	-4.121e+05	1.510e+05	1.317e+04
2	76	-40.00	-2.246e+04	-261.52	9590.72	-4.755e+05	4.532e+05	6073.48
M_S			N memb.	V memb.	V orto	M memb.	M orto	T
			-3.237e+04	-3853.09	-7684.28	-7.076e+05	-7.547e+04	-1.445e+04
			-2767.46	485.33	1.351e+04	2.473e+05	6.449e+05	2.137e+04

Macro	Tipo	Angolo 1-Z (gradi)
3	Setto	0.0

M_S	Cmb	Z	N memb.	V memb.	V orto	M memb.	M orto	T
		cm	daN	daN	daN	daN cm	daN cm	daN cm
3	1	-305.00	-3473.48	-553.03	770.67	1.519e+04	-2.745e+04	-175.58
3	1	-270.00	-3072.58	-348.65	1270.37	1.959e+04	8277.77	-6.74
3	1	-231.67	-3188.84	2896.27	744.23	8513.99	6829.68	197.83
3	1	-231.67	-3188.84	2896.27	744.23	8513.99	6829.68	197.83
3	1	-193.33	-3155.19	1577.44	667.29	-2.451e+04	767.51	188.87
3	1	-193.33	-3155.19	1577.44	667.29	-2.451e+04	767.51	188.87
3	1	-155.00	-2757.99	-302.38	621.55	-3.517e+04	-1509.32	196.01
3	1	-116.67	-2135.33	-1776.37	524.24	-2.511e+04	-823.21	259.03
3	1	-116.67	-2135.33	-1776.37	524.24	-2.511e+04	-823.21	259.03
3	1	-80.00	-1368.16	-2272.50	330.59	-6949.91	500.80	346.82
3	1	-40.00	-416.16	-1355.33	-171.81	4603.61	-5787.34	671.20
3	4	-305.00	-6051.36	-1331.99	937.42	8855.98	-3.300e+04	62.01
3	4	-270.00	-6282.90	-2285.44	1291.76	5.575e+04	6021.37	2110.81
3	4	-231.67	-6266.54	781.17	798.00	7.664e+04	6858.04	-313.62
3	4	-231.67	-6266.54	781.17	798.00	7.664e+04	6858.04	-313.62
3	4	-193.33	-6372.13	184.58	697.78	6.508e+04	2372.16	-143.88
3	4	-193.33	-6372.13	184.58	697.78	6.508e+04	2372.16	-143.88
3	4	-155.00	-5748.30	-1318.50	635.39	6.179e+04	994.00	-348.35
3	4	-116.67	-4476.44	-2096.68	477.73	6.878e+04	1295.68	-560.12
3	4	-116.67	-4476.44	-2096.68	477.73	6.878e+04	1295.68	-560.12
3	4	-80.00	-2743.36	-1111.15	515.48	5.691e+04	-1780.62	-725.79
3	4	-40.00	-1068.04	1285.05	-488.73	-1.028e+04	-2.059e+04	-924.87
3	5	-305.00	-2496.53	-387.23	582.02	1.130e+04	-2.072e+04	-170.92
3	5	-270.00	-2195.79	-227.22	966.77	1.405e+04	6386.65	-51.14
3	5	-231.67	-2357.29	2296.53	572.85	8118.93	5229.48	149.93
3	5	-231.67	-2357.29	2296.53	572.85	8118.93	5229.48	149.93
3	5	-193.33	-2361.43	1289.06	513.68	-1.732e+04	577.45	133.48
3	5	-193.33	-2361.43	1289.06	513.68	-1.732e+04	577.45	133.48
3	5	-155.00	-2075.57	-155.63	478.26	-2.582e+04	-1165.15	132.19
3	5	-116.67	-1610.13	-1288.59	402.99	-1.848e+04	-641.96	177.63
3	5	-116.67	-1610.13	-1288.59	402.99	-1.848e+04	-641.96	177.63
3	5	-80.00	-1031.02	-1670.45	253.71	-5022.19	357.33	244.34
3	5	-40.00	-315.49	-982.01	-131.43	3205.07	-4491.98	503.53
3	24	-305.00	-3151.34	-645.50	493.67	2929.83	-2.197e+04	-53.56
3	24	-270.00	-3324.01	-1104.58	800.70	3.163e+04	7097.68	2414.80
3	24	-231.67	-3289.39	1592.15	565.69	4.912e+04	5237.56	126.61
3	24	-231.67	-3289.39	1592.15	565.69	4.912e+04	5237.56	126.61
3	24	-193.33	-3474.95	1281.98	534.42	3.652e+04	855.88	566.82
3	24	-193.33	-3474.95	1281.98	534.42	3.652e+04	855.88	566.82
3	24	-155.00	-3222.79	46.73	486.32	3.026e+04	-224.49	335.51
3	24	-116.67	-2518.17	-801.12	373.30	3.314e+04	126.40	171.61
3	24	-116.67	-2518.17	-801.12	373.30	3.314e+04	126.40	171.61
3	24	-80.00	-1526.20	-514.80	141.85	2.780e+04	-1172.12	-352.17
3	24	-40.00	-532.95	794.32	-301.58	-6723.33	-1.273e+04	-82.22
3	37	-305.00	-4973.96	-882.75	839.27	8243.95	-2.557e+04	317.05

SCARICATORE IN VIA PUCCI

3	37	-270.00	-4832.78	-1341.83	1146.29	3.100e+04	3585.60	127.44
3	37	-231.67	-4875.69	624.33	630.84	3.404e+04	5446.98	-531.35
3	37	-231.67	-4875.69	624.33	630.84	3.404e+04	5446.98	-531.35
3	37	-193.33	-4809.58	-385.36	525.55	2.011e+04	1889.86	-820.71
3	37	-193.33	-4809.58	-385.36	525.55	2.011e+04	1889.86	-820.71
3	37	-155.00	-4209.60	-1633.82	484.44	1.912e+04	462.61	-811.01
3	37	-116.67	-3261.88	-2283.67	379.61	2.904e+04	786.04	-889.83
3	37	-116.67	-3261.88	-2283.67	379.61	2.904e+04	786.04	-889.83
3	37	-80.00	-2018.44	-1719.37	136.77	3.193e+04	-618.75	-742.69
3	37	-40.00	-795.78	-7.48	-300.19	-772.18	-1.217e+04	-672.92
3	56	-305.00	-3464.73	-716.16	560.48	4691.65	-2.268e+04	-46.99
3	56	-270.00	-3582.55	-1175.23	867.51	3.234e+04	6392.70	1929.16
3	56	-231.67	-3582.92	1421.76	578.80	4.683e+04	5239.97	38.51
3	56	-231.67	-3582.92	1421.76	578.80	4.683e+04	5239.97	38.51
3	56	-193.33	-3717.02	989.53	532.84	3.381e+04	1069.33	346.57
3	56	-193.33	-3717.02	989.53	532.84	3.381e+04	1069.33	346.57
3	56	-155.00	-3398.29	-249.07	485.90	2.833e+04	-80.23	154.18
3	56	-116.67	-2649.81	-1062.98	375.31	3.242e+04	262.42	13.55
3	56	-116.67	-2649.81	-1062.98	375.31	3.242e+04	262.42	13.55
3	56	-80.00	-1618.80	-728.81	140.94	2.822e+04	-1045.53	-340.46
3	56	-40.00	-582.44	647.60	-301.30	-5896.25	-1.259e+04	-177.34
3	69	-305.00	-4576.65	-865.59	779.85	8585.39	-2.496e+04	184.31
3	69	-270.00	-4506.38	-1324.67	1086.87	3.250e+04	4163.11	481.78
3	69	-231.67	-4551.42	815.22	620.11	3.808e+04	5363.14	-369.93
3	69	-231.67	-4551.42	815.22	620.11	3.808e+04	5363.14	-369.93
3	69	-193.33	-4537.75	-39.31	526.94	2.396e+04	1722.16	-515.86
3	69	-193.33	-4537.75	-39.31	526.94	2.396e+04	1722.16	-515.86
3	69	-155.00	-4013.31	-1285.25	485.01	2.154e+04	356.94	-546.11
3	69	-116.67	-3116.69	-1980.46	379.17	2.979e+04	676.81	-631.54
3	69	-116.67	-3116.69	-1980.46	379.17	2.979e+04	676.81	-631.54
3	69	-80.00	-1926.20	-1479.46	137.77	3.071e+04	-703.70	-561.39
3	69	-40.00	-745.66	142.30	-300.55	-2243.15	-1.224e+04	-546.52
3	73	-305.00	-2595.66	-408.81	588.13	1.152e+04	-2.095e+04	-150.65
3	73	-270.00	-2290.60	-250.37	972.67	1.462e+04	6375.83	-25.17
3	73	-231.67	-2411.36	2257.74	572.64	7231.70	5243.11	151.20
3	73	-231.67	-2411.36	2257.74	572.64	7231.70	5243.11	151.20
3	73	-193.33	-2398.53	1246.30	513.46	-1.819e+04	584.76	140.15
3	73	-193.33	-2398.53	1246.30	513.46	-1.819e+04	584.76	140.15
3	73	-155.00	-2101.55	-199.13	478.18	-2.652e+04	-1162.81	142.70
3	73	-116.67	-1628.46	-1332.59	403.14	-1.895e+04	-637.03	189.85
3	73	-116.67	-1628.46	-1332.59	403.14	-1.895e+04	-637.03	189.85
3	73	-80.00	-1043.12	-1714.32	254.04	-5205.26	373.10	257.03
3	73	-40.00	-318.11	-1016.23	-131.84	3395.08	-4469.27	510.75
3	76	-305.00	-4314.24	-928.11	699.29	7292.73	-2.465e+04	7.74
3	76	-270.00	-4430.81	-1541.57	986.93	3.873e+04	4871.57	1386.53
3	76	-231.67	-4463.16	847.67	608.49	5.265e+04	5262.02	-189.77
3	76	-231.67	-4463.16	847.67	608.49	5.265e+04	5262.02	-189.77
3	76	-193.33	-4543.16	317.73	533.79	4.154e+04	1654.53	-81.68
3	76	-193.33	-4543.16	317.73	533.79	4.154e+04	1654.53	-81.68
3	76	-155.00	-4095.09	-876.55	487.40	3.813e+04	506.07	-220.21
3	76	-116.67	-3189.21	-1546.13	372.13	4.364e+04	775.56	-356.25
3	76	-116.67	-3189.21	-1546.13	372.13	4.364e+04	775.56	-356.25
3	76	-80.00	-1959.92	-940.09	110.63	3.737e+04	-1147.85	-458.04
3	76	-40.00	-752.70	744.02	-343.12	-6525.75	-1.434e+04	-553.30

M_S	N memb.	V memb.	V orto	M memb.	M orto	T
	-6372.13	-2285.44	-488.73	-3.517e+04	-3.300e+04	-924.87
	-315.49	2896.27	1291.76	7.664e+04	8277.77	2414.80

Macro	Tipo	Angolo 1-Z (gradi)
4	Setto	0.0

M_S	Cmb	Z cm	N memb. daN	V memb. daN	V orto daN	M memb. daN cm	M orto daN cm	T daN cm
4	4	-305.00	-5592.15	-1778.44	-1116.95	2.273e+04	3.708e+04	-1659.98
4	4	-270.00	-5626.03	-1941.82	-1531.82	6.382e+04	-9269.48	3694.19
4	4	-231.67	-4937.84	179.49	-796.68	3.499e+04	-5774.50	52.84
4	4	-231.67	-4937.84	179.49	-796.68	3.499e+04	-5774.50	52.84
4	4	-193.33	-4534.15	-607.79	-741.49	1.870e+04	-2716.71	64.45
4	4	-193.33	-4534.15	-607.79	-741.49	1.870e+04	-2716.71	64.45
4	4	-155.00	-3922.91	-1422.18	-592.48	2.118e+04	-1349.42	-137.72
4	4	-116.67	-3102.58	-1895.32	-411.47	3.599e+04	933.46	-600.69
4	4	-116.67	-3102.58	-1895.32	-411.47	3.599e+04	933.46	-600.69
4	4	-80.00	-1896.80	-1530.53	-220.11	4.065e+04	4061.62	-1881.21

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

4	4	-79.75	-1815.66	-1555.26	-109.74	4.400e+04	3817.34	-1636.91
4	4	-79.35	-1687.95	-1471.15	82.55	4.526e+04	3125.00	-1847.27
4	4	-78.95	-1456.17	-1442.90	275.38	3.955e+04	3180.43	-2590.68
4	4	-78.83	-1530.20	-1573.68	307.13	4.359e+04	2493.58	-2066.64
4	4	-40.00	-147.01	588.87	209.46	-1.505e+04	1.258e+04	-4099.30
4	6	-305.00	-4646.59	-1618.28	-879.99	1.945e+04	2.905e+04	-1403.90
4	6	-270.00	-4708.86	-1818.65	-1205.80	5.893e+04	-7441.79	3473.07
4	6	-231.67	-4184.45	102.65	-607.62	3.912e+04	-4188.74	231.45
4	6	-231.67	-4184.45	102.65	-607.62	3.912e+04	-4188.74	231.45
4	6	-193.33	-3896.76	-444.60	-572.94	2.623e+04	-1862.02	147.00
4	6	-193.33	-3896.76	-444.60	-572.94	2.623e+04	-1862.02	147.00
4	6	-155.00	-3407.53	-1077.13	-451.63	2.801e+04	-803.63	-195.35
4	6	-116.67	-2702.60	-1435.14	-305.03	3.982e+04	1262.09	-771.19
4	6	-116.67	-2702.60	-1435.14	-305.03	3.982e+04	1262.09	-771.19
4	6	-80.00	-1621.63	-1044.23	-162.00	4.100e+04	4056.50	-2002.84
4	6	-79.75	-1555.48	-1056.96	-78.28	4.368e+04	3853.78	-1833.36
4	6	-79.35	-1451.27	-973.87	68.45	4.463e+04	3298.05	-2091.94
4	6	-78.95	-1244.72	-938.50	218.84	3.945e+04	3463.76	-2711.48
4	6	-78.83	-1320.66	-1059.74	236.20	4.357e+04	2827.03	-2174.11
4	6	-40.00	-52.45	885.64	166.91	-1.616e+04	1.069e+04	-3924.85
4	24	-305.00	-2886.54	-1073.24	-919.87	1.914e+04	2.847e+04	-698.68
4	24	-270.00	-2933.73	-1101.58	-1234.19	4.279e+04	-5951.11	3105.22
4	24	-231.67	-2636.45	239.15	-641.55	1.368e+04	-4949.80	-86.51
4	24	-231.67	-2636.45	239.15	-641.55	1.368e+04	-4949.80	-86.51
4	24	-193.33	-2672.95	-483.41	-566.50	-6257.56	-2725.03	157.17
4	24	-193.33	-2672.95	-483.41	-566.50	-6257.56	-2725.03	157.17
4	24	-155.00	-2323.97	-1092.43	-458.19	-2696.53	-1609.47	188.58
4	24	-116.67	-1845.22	-1450.15	-324.71	9417.90	-196.25	-105.56
4	24	-116.67	-1845.22	-1450.15	-324.71	9417.90	-196.25	-105.56
4	24	-80.00	-1176.91	-1284.76	-171.28	1.673e+04	1812.97	-887.62
4	24	-79.75	-1105.04	-1302.81	-84.75	1.983e+04	1672.64	-678.81
4	24	-79.35	-1014.18	-1261.65	72.39	2.089e+04	1267.32	-747.93
4	24	-78.95	-909.45	-1267.80	217.96	1.841e+04	1295.16	-1316.40
4	24	-78.83	-982.37	-1348.49	244.46	2.238e+04	815.34	-1066.17
4	24	-40.00	-164.18	-21.96	158.22	-9847.07	8419.04	-2304.01
4	25	-305.00	-4576.58	-1479.41	-927.41	1.620e+04	2.873e+04	-1752.56
4	25	-270.00	-4539.33	-1507.76	-1241.73	4.052e+04	-5735.07	1866.87
4	25	-231.67	-3953.04	98.58	-618.76	1.889e+04	-5068.47	-396.90
4	25	-231.67	-3953.04	98.58	-618.76	1.889e+04	-5068.47	-396.90
4	25	-193.33	-3577.40	-614.18	-560.21	6468.58	-2601.29	-191.38
4	25	-193.33	-3577.40	-614.18	-560.21	6468.58	-2601.29	-191.38
4	25	-155.00	-2953.63	-1192.67	-455.66	8743.84	-1309.56	-106.51
4	25	-116.67	-2237.08	-1512.90	-326.54	2.223e+04	423.89	-187.30
4	25	-116.67	-2237.08	-1512.90	-326.54	2.223e+04	423.89	-187.30
4	25	-80.00	-1210.52	-1144.47	-175.98	2.770e+04	2453.28	-950.68
4	25	-79.75	-1194.54	-1176.43	-88.37	2.812e+04	2284.71	-734.09
4	25	-79.35	-1128.33	-1135.58	56.65	2.867e+04	1621.44	-807.44
4	25	-78.95	-965.83	-1061.94	181.25	2.452e+04	1250.97	-1305.53
4	25	-78.83	-997.80	-1122.61	204.90	2.631e+04	737.51	-1025.16
4	25	-40.00	-108.39	205.01	118.65	-8568.32	8287.78	-2139.11
4	31	-305.00	-4208.94	-1454.14	-997.15	1.700e+04	2.950e+04	-1564.10
4	31	-270.00	-4189.23	-1482.49	-1311.48	4.116e+04	-4976.29	2197.69
4	31	-231.67	-3685.35	54.08	-635.18	1.571e+04	-5182.97	-392.40
4	31	-231.67	-3685.35	54.08	-635.18	1.571e+04	-5182.97	-392.40
4	31	-193.33	-3424.30	-732.94	-558.44	1257.25	-2900.75	-151.34
4	31	-193.33	-3424.30	-732.94	-558.44	1257.25	-2900.75	-151.34
4	31	-155.00	-2888.22	-1317.15	-453.56	3156.10	-1509.45	-143.58
4	31	-116.67	-2185.97	-1610.61	-324.34	1.804e+04	243.95	-225.37
4	31	-116.67	-2185.97	-1610.61	-324.34	1.804e+04	243.95	-225.37
4	31	-80.00	-1177.11	-1214.09	-171.69	2.480e+04	2277.65	-1001.20
4	31	-79.75	-1150.32	-1244.26	-83.10	2.573e+04	2129.59	-784.55
4	31	-79.35	-1084.63	-1206.19	65.97	2.636e+04	1492.19	-864.99
4	31	-78.95	-945.16	-1131.36	185.56	2.281e+04	1118.48	-1372.70
4	31	-78.83	-990.00	-1185.07	204.35	2.528e+04	545.47	-1097.61
4	31	-40.00	-92.89	143.14	118.11	-1.011e+04	8132.47	-2098.06
4	35	-305.00	-4179.87	-1290.14	-951.97	1.396e+04	2.913e+04	-1479.21
4	35	-270.00	-4136.22	-1318.49	-1266.29	3.804e+04	-5400.82	2019.51
4	35	-231.67	-3672.32	195.09	-631.81	1.441e+04	-4921.60	-559.00
4	35	-231.67	-3672.32	195.09	-631.81	1.441e+04	-4921.60	-559.00
4	35	-193.33	-3329.89	-597.29	-561.05	2077.60	-2755.78	-379.92
4	35	-193.33	-3329.89	-597.29	-561.05	2077.60	-2755.78	-379.92
4	35	-155.00	-2860.89	-1213.19	-454.21	2464.70	-1386.31	-414.32
4	35	-116.67	-2229.02	-1484.83	-324.16	1.416e+04	294.21	-456.16
4	35	-116.67	-2229.02	-1484.83	-324.16	1.416e+04	294.21	-456.16
4	35	-80.00	-1302.70	-1190.67	-170.96	1.975e+04	2340.75	-1211.27
4	35	-79.75	-1215.66	-1221.16	-81.86	2.356e+04	2193.67	-999.38
4	35	-79.35	-1119.43	-1177.05	66.27	2.481e+04	1550.55	-1082.20
4	35	-78.95	-976.41	-1115.17	185.44	2.124e+04	1163.72	-1524.51
4	35	-78.83	-1014.01	-1169.54	204.88	2.333e+04	592.85	-1225.78

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

4	35	-40.00	-82.39	158.79	118.63	-1.026e+04	8168.54	-2222.74
4	56	-305.00	-3175.53	-1080.13	-881.96	1.765e+04	2.805e+04	-860.86
4	56	-270.00	-3204.06	-1108.47	-1196.29	4.140e+04	-6371.78	2788.29
4	56	-231.67	-2859.17	282.94	-631.49	1.520e+04	-4846.81	-133.31
4	56	-231.67	-2859.17	282.94	-631.49	1.520e+04	-4846.81	-133.31
4	56	-193.33	-2775.13	-410.60	-567.22	-2140.31	-2550.63	62.29
4	56	-193.33	-2775.13	-410.60	-567.22	-2140.31	-2550.63	62.29
4	56	-155.00	-2398.19	-1024.09	-458.94	581.28	-1470.85	90.40
4	56	-116.67	-1899.21	-1388.86	-325.94	1.198e+04	-47.55	-141.62
4	56	-116.67	-1899.21	-1388.86	-325.94	1.198e+04	-47.55	-141.62
4	56	-80.00	-1200.99	-1228.75	-173.69	1.850e+04	1961.16	-898.75
4	56	-79.75	-1134.25	-1249.43	-87.46	2.136e+04	1807.88	-690.85
4	56	-79.35	-1043.40	-1206.69	66.66	2.238e+04	1368.16	-756.99
4	56	-78.95	-922.15	-1207.40	213.13	1.948e+04	1363.51	-1307.92
4	56	-78.83	-981.95	-1288.14	241.77	2.274e+04	910.17	-1051.01
4	56	-40.00	-162.76	38.30	155.53	-9010.58	8475.88	-2331.94
4	57	-305.00	-4234.76	-1330.40	-882.86	1.582e+04	2.817e+04	-1512.68
4	57	-270.00	-4210.59	-1358.75	-1197.18	4.002e+04	-6279.69	2020.94
4	57	-231.67	-3684.42	197.22	-616.73	1.869e+04	-4905.94	-324.18
4	57	-231.67	-3684.42	197.22	-616.73	1.869e+04	-4905.94	-324.18
4	57	-193.33	-3339.05	-486.36	-563.37	6052.94	-2454.23	-155.49
4	57	-193.33	-3339.05	-486.36	-563.37	6052.94	-2454.23	-155.49
4	57	-155.00	-2793.15	-1081.56	-457.45	7916.46	-1274.32	-87.44
4	57	-116.67	-2148.01	-1426.00	-327.09	2.004e+04	342.05	-187.82
4	57	-116.67	-2148.01	-1426.00	-327.09	2.004e+04	342.05	-187.82
4	57	-80.00	-1224.35	-1144.08	-176.71	2.536e+04	2363.15	-938.01
4	57	-79.75	-1191.54	-1173.28	-89.88	2.659e+04	2191.60	-725.23
4	57	-79.35	-1115.93	-1129.84	56.47	2.730e+04	1588.96	-793.97
4	57	-78.95	-957.56	-1079.81	190.00	2.333e+04	1337.17	-1300.57
4	57	-78.83	-990.65	-1148.42	217.04	2.517e+04	864.73	-1024.16
4	57	-40.00	-127.01	178.67	130.80	-8212.44	8399.91	-2231.95
4	63	-305.00	-3999.93	-1313.15	-924.71	1.631e+04	2.862e+04	-1392.95
4	63	-270.00	-3986.91	-1341.50	-1239.04	4.040e+04	-5839.09	2225.05
4	63	-231.67	-3513.66	171.69	-626.59	1.667e+04	-4977.53	-315.63
4	63	-231.67	-3513.66	171.69	-626.59	1.667e+04	-4977.53	-315.63
4	63	-193.33	-3240.71	-555.24	-562.36	2753.86	-2635.38	-128.05
4	63	-193.33	-3240.71	-555.24	-562.36	2753.86	-2635.38	-128.05
4	63	-155.00	-2750.01	-1153.68	-456.21	4392.17	-1397.45	-109.33
4	63	-116.67	-2114.22	-1482.54	-325.75	1.740e+04	229.56	-210.85
4	63	-116.67	-2114.22	-1482.54	-325.75	1.740e+04	229.56	-210.85
4	63	-80.00	-1202.39	-1185.10	-174.14	2.354e+04	2252.95	-967.10
4	63	-79.75	-1163.00	-1213.21	-86.74	2.508e+04	2093.83	-754.59
4	63	-79.35	-1087.86	-1171.68	62.12	2.584e+04	1510.21	-827.09
4	63	-78.95	-944.17	-1121.16	193.00	2.225e+04	1260.93	-1339.70
4	63	-78.83	-985.48	-1185.64	217.26	2.453e+04	754.36	-1067.12
4	63	-40.00	-118.28	141.79	131.01	-9136.26	8310.41	-2210.16
4	67	-305.00	-3985.37	-1218.60	-899.79	1.446e+04	2.841e+04	-1344.74
4	67	-270.00	-3957.66	-1246.94	-1214.12	3.851e+04	-6075.51	2122.51
4	67	-231.67	-3507.28	251.30	-624.90	1.586e+04	-4823.65	-415.36
4	67	-231.67	-3507.28	251.30	-624.90	1.586e+04	-4823.65	-415.36
4	67	-193.33	-3183.38	-480.03	-563.93	3307.28	-2556.94	-265.14
4	67	-193.33	-3183.38	-480.03	-563.93	3307.28	-2556.94	-265.14
4	67	-155.00	-2734.26	-1096.43	-456.54	3988.88	-1327.92	-272.03
4	67	-116.67	-2140.90	-1411.11	-325.60	1.506e+04	261.33	-349.85
4	67	-116.67	-2140.90	-1411.11	-325.60	1.506e+04	261.33	-349.85
4	67	-80.00	-1279.89	-1171.91	-173.68	2.046e+04	2290.92	-1090.57
4	67	-79.75	-1203.89	-1200.46	-85.90	2.375e+04	2132.31	-880.02
4	67	-79.35	-1109.79	-1155.67	62.44	2.490e+04	1544.54	-954.64
4	67	-78.95	-963.83	-1112.27	192.94	2.129e+04	1286.22	-1429.93
4	67	-78.83	-1000.62	-1176.89	217.55	2.333e+04	780.01	-1143.59
4	67	-40.00	-112.28	150.61	131.31	-9212.69	8329.83	-2281.48
4	74	-305.00	-3958.77	-1249.01	-842.11	1.646e+04	2.794e+04	-1213.61
4	74	-270.00	-3974.01	-1326.88	-1159.67	4.484e+04	-7089.48	2625.47
4	74	-231.67	-3514.91	268.62	-614.01	2.395e+04	-4535.51	-89.87
4	74	-231.67	-3514.91	268.62	-614.01	2.395e+04	-4535.51	-89.87
4	74	-193.33	-3224.36	-356.64	-569.46	1.104e+04	-2162.30	-27.43
4	74	-193.33	-3224.36	-356.64	-569.46	1.104e+04	-2162.30	-27.43
4	74	-155.00	-2783.01	-980.37	-457.54	1.242e+04	-1120.75	-99.24
4	74	-116.67	-2200.29	-1349.02	-321.33	2.305e+04	503.39	-357.38
4	74	-116.67	-2200.29	-1349.02	-321.33	2.305e+04	503.39	-357.38
4	74	-80.00	-1354.10	-1122.80	-173.03	2.707e+04	2736.56	-1227.42
4	74	-79.75	-1293.11	-1144.24	-87.74	2.961e+04	2554.44	-1030.19
4	74	-79.35	-1197.98	-1087.33	60.67	3.059e+04	2033.45	-1149.03
4	74	-78.95	-1031.48	-1068.81	208.24	2.650e+04	2029.03	-1700.44
4	74	-78.83	-1079.39	-1160.46	235.72	2.912e+04	1548.10	-1354.64
4	74	-40.00	-128.07	343.63	154.41	-1.013e+04	9164.62	-2808.09
4	76	-305.00	-3992.89	-1250.42	-843.52	1.648e+04	2.800e+04	-1214.85
4	76	-270.00	-4007.19	-1330.92	-1160.83	4.482e+04	-7071.93	2613.88
4	76	-231.67	-3535.04	247.96	-614.22	2.351e+04	-4538.92	-81.64

SCARICATORE IN VIA PUCCI

4	76	-231.67	-3535.04	247.96	-614.22	2.351e+04	-4538.92	-81.64
4	76	-193.33	-3239.07	-378.43	-569.42	1.069e+04	-2167.47	-21.36
4	76	-193.33	-3239.07	-378.43	-569.42	1.069e+04	-2167.47	-21.36
4	76	-155.00	-2794.05	-1002.17	-457.55	1.218e+04	-1124.61	-93.30
4	76	-116.67	-2208.54	-1370.45	-321.38	2.292e+04	498.51	-351.49
4	76	-116.67	-2208.54	-1370.45	-321.38	2.292e+04	498.51	-351.49
4	76	-80.00	-1359.99	-1143.26	-172.94	2.705e+04	2731.79	-1222.50
4	76	-79.75	-1299.05	-1164.77	-87.63	2.959e+04	2549.81	-1025.47
4	76	-79.35	-1203.83	-1107.93	60.78	3.057e+04	2028.59	-1144.30
4	76	-78.95	-1037.47	-1089.92	208.32	2.649e+04	2022.79	-1695.58
4	76	-78.83	-1085.49	-1181.53	235.82	2.911e+04	1542.00	-1350.21
4	76	-40.00	-130.22	328.70	155.16	-1.003e+04	9174.98	-2808.50

M_S	N memb.	V memb.	V orto	M memb.	M orto	T
	-5626.03	-1941.82	-1531.82	-1.616e+04	-9269.48	-4099.30
	-52.45	885.64	307.13	6.382e+04	3.708e+04	3694.19

Macro	Tipo	Angolo 1-Z (gradi)
5	Setto	0.0

M_S	Cmb	Z cm	N memb. daN	V memb. daN	V orto daN	M memb. daN cm	M orto daN cm	T daN cm
5	3	-305.00	-3587.30	-385.23	-1126.68	3786.64	3.819e+04	-336.68
5	3	-270.00	-3649.18	-446.91	-1504.40	-1271.08	-7836.56	624.24
5	3	-231.67	-3618.58	-458.39	-965.93	1789.03	-9508.27	1057.67
5	3	-231.67	-3618.58	-458.39	-965.93	1789.03	-9508.27	1057.67
5	3	-193.33	-3598.27	-408.05	-821.53	8628.35	-5856.43	1098.13
5	3	-193.33	-3598.27	-408.05	-821.53	8628.35	-5856.43	1098.13
5	3	-155.00	-3277.98	-314.87	-690.03	1.354e+04	-3920.60	529.55
5	3	-116.67	-2558.03	-220.95	-511.98	1.253e+04	-2499.38	-199.04
5	3	-116.67	-2558.03	-220.95	-511.98	1.253e+04	-2499.38	-199.04
5	3	-80.00	-1649.48	-170.20	-237.86	7086.30	242.57	-560.26
5	3	-40.00	-830.50	-180.15	343.34	518.92	1.383e+04	-274.06
5	4	-305.00	-5504.91	-55.34	-938.82	8493.79	3.497e+04	-1046.53
5	4	-270.00	-5032.37	-99.60	-1446.63	3465.22	-6753.40	-1611.37
5	4	-231.67	-4229.94	-132.90	-941.67	-517.44	-7062.61	-1037.59
5	4	-231.67	-4229.94	-132.90	-941.67	-517.44	-7062.61	-1037.59
5	4	-193.33	-3637.40	-166.00	-810.28	-1766.45	-2744.30	-333.63
5	4	-193.33	-3637.40	-166.00	-810.28	-1766.45	-2744.30	-333.63
5	4	-155.00	-3066.05	-195.70	-687.99	-1174.51	-550.98	221.00
5	4	-116.67	-2499.58	-228.30	-515.06	-890.62	829.84	652.76
5	4	-116.67	-2499.58	-228.30	-515.06	-890.62	829.84	652.76
5	4	-80.00	-2157.32	-239.53	-211.03	-476.48	3842.47	974.12
5	4	-40.00	-2026.02	-192.25	393.24	-503.73	1.945e+04	937.30
5	5	-305.00	-2536.86	-286.10	-864.05	2750.03	2.920e+04	-257.65
5	5	-270.00	-2591.77	-332.75	-1152.39	-836.30	-6083.31	460.90
5	5	-231.67	-2584.93	-341.20	-741.44	1582.54	-7238.51	766.98
5	5	-231.67	-2584.93	-341.20	-741.44	1582.54	-7238.51	766.98
5	5	-193.33	-2599.51	-302.21	-632.22	6740.49	-4412.07	783.59
5	5	-193.33	-2599.51	-302.21	-632.22	6740.49	-4412.07	783.59
5	5	-155.00	-2393.62	-230.74	-531.56	1.039e+04	-2948.76	345.76
5	5	-116.67	-1885.49	-159.02	-395.11	9547.81	-1896.71	-208.46
5	5	-116.67	-1885.49	-159.02	-395.11	9547.81	-1896.71	-208.46
5	5	-80.00	-1229.55	-120.36	-186.11	5338.15	133.95	-477.71
5	5	-40.00	-631.48	-126.94	254.46	386.79	1.035e+04	-229.01
5	6	-305.00	-4454.46	43.80	-676.20	7457.18	2.597e+04	-967.51
5	6	-270.00	-3974.96	14.57	-1094.62	3899.99	-5000.15	-1774.71
5	6	-231.67	-3196.30	-15.71	-717.18	-723.93	-4792.85	-1328.29
5	6	-231.67	-3196.30	-15.71	-717.18	-723.93	-4792.85	-1328.29
5	6	-193.33	-2638.63	-60.16	-620.96	-3654.31	-1299.94	-648.18
5	6	-193.33	-2638.63	-60.16	-620.96	-3654.31	-1299.94	-648.18
5	6	-155.00	-2181.68	-111.57	-529.52	-4315.83	420.87	37.22
5	6	-116.67	-1827.05	-166.37	-398.19	-3876.55	1432.52	643.35
5	6	-116.67	-1827.05	-166.37	-398.19	-3876.55	1432.52	643.35
5	6	-80.00	-1737.40	-189.70	-159.28	-2224.63	3733.85	1056.67
5	6	-40.00	-1827.00	-139.04	304.36	-635.86	1.597e+04	982.34
5	15	-305.00	-3491.27	-340.06	-750.95	1.787e+04	2.718e+04	-1056.60
5	15	-270.00	-3269.22	-377.90	-1109.98	1.332e+04	-5797.16	-1157.44
5	15	-231.67	-2742.44	-381.08	-729.84	-5377.59	-6038.53	-830.16
5	15	-231.67	-2742.44	-381.08	-729.84	-5377.59	-6038.53	-830.16
5	15	-193.33	-2634.08	-336.46	-626.71	-1.047e+04	-2856.57	-500.21
5	15	-193.33	-2634.08	-336.46	-626.71	-1.047e+04	-2856.57	-500.21
5	15	-155.00	-2475.39	-289.29	-527.84	-8888.18	-1197.63	-431.40
5	15	-116.67	-1997.57	-246.49	-392.36	-5374.53	-12.22	-336.84

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

5	15	-116.67	-1997.57	-246.49	-392.36	-5374.53	-12.22	-336.84
5	15	-80.00	-1574.08	-172.17	-169.00	-4485.50	1920.45	-114.64
5	15	-40.00	-1291.28	-10.09	261.67	-3087.86	1.329e+04	183.43
5	24	-305.00	-2844.20	-624.19	-767.68	1.701e+04	2.764e+04	-1068.65
5	24	-270.00	-2649.53	-662.02	-1126.71	1.273e+04	-5434.08	-1091.97
5	24	-231.67	-2159.44	-673.10	-729.38	-8541.17	-6084.84	-576.13
5	24	-231.67	-2159.44	-673.10	-729.38	-8541.17	-6084.84	-576.13
5	24	-193.33	-2191.77	-623.22	-628.63	-1.601e+04	-2846.54	-115.32
5	24	-193.33	-2191.77	-623.22	-628.63	-1.601e+04	-2846.54	-115.32
5	24	-155.00	-2099.29	-544.04	-533.94	-1.236e+04	-1289.83	204.27
5	24	-116.67	-1732.92	-466.93	-399.12	-7825.14	-238.63	647.33
5	24	-116.67	-1732.92	-466.93	-399.12	-7825.14	-238.63	647.33
5	24	-80.00	-1452.35	-386.01	-175.11	-3791.23	1820.83	957.49
5	24	-40.00	-1252.46	-113.55	273.39	-1870.74	1.321e+04	394.07
5	37	-305.00	-4881.54	247.53	-712.97	4043.92	2.666e+04	-541.27
5	37	-270.00	-4588.98	209.70	-1072.00	177.05	-6377.60	-667.68
5	37	-231.67	-4114.55	188.09	-724.83	6486.58	-5744.28	-537.33
5	37	-231.67	-4114.55	188.09	-724.83	6486.58	-5744.28	-537.33
5	37	-193.33	-3574.35	172.47	-622.96	9931.58	-2510.67	-424.60
5	37	-193.33	-3574.35	172.47	-622.96	9931.58	-2510.67	-424.60
5	37	-155.00	-2965.83	139.39	-525.48	9551.37	-857.91	-425.53
5	37	-116.67	-2321.05	114.53	-390.62	6544.45	256.25	-486.48
5	37	-116.67	-2321.05	114.53	-390.62	6544.45	256.25	-486.48
5	37	-80.00	-1704.70	73.38	-170.66	-214.34	2586.61	-268.14
5	37	-40.00	-1326.04	9.54	272.10	-2370.55	1.366e+04	212.77
5	40	-305.00	-2501.07	-479.95	-817.86	6669.73	2.851e+04	-732.78
5	40	-270.00	-2324.75	-517.79	-1176.89	3034.99	-4568.34	-772.34
5	40	-231.67	-1942.45	-536.81	-734.04	-6025.95	-6213.44	-108.49
5	40	-231.67	-1942.45	-536.81	-734.04	-6025.95	-6213.44	-108.49
5	40	-193.33	-1865.68	-532.52	-629.15	-7660.63	-3103.78	536.90
5	40	-193.33	-1865.68	-532.52	-629.15	-7660.63	-3103.78	536.90
5	40	-155.00	-1746.71	-487.33	-534.55	-4432.30	-1524.73	860.82
5	40	-116.67	-1484.90	-453.35	-401.38	-1657.46	-529.14	1043.66
5	40	-116.67	-1484.90	-453.35	-401.38	-1657.46	-529.14	1043.66
5	40	-80.00	-1342.59	-400.56	-169.22	2957.23	1583.48	1004.71
5	40	-40.00	-1220.86	-290.10	301.46	2067.95	1.337e+04	642.86
5	44	-305.00	-3192.54	-329.41	-778.87	1.228e+04	2.771e+04	-891.74
5	44	-270.00	-2985.39	-367.25	-1137.89	8091.93	-5303.40	-984.96
5	44	-231.67	-2532.41	-371.13	-731.62	-4337.97	-6117.17	-542.64
5	44	-231.67	-2532.41	-371.13	-731.62	-4337.97	-6117.17	-542.64
5	44	-193.33	-2399.86	-349.12	-627.24	-7211.38	-2966.13	-81.01
5	44	-193.33	-2399.86	-349.12	-627.24	-7211.38	-2966.13	-81.01
5	44	-155.00	-2224.68	-311.19	-529.86	-5286.24	-1330.30	74.12
5	44	-116.67	-1830.47	-284.11	-395.64	-3348.92	-217.83	160.30
5	44	-116.67	-1830.47	-284.11	-395.64	-3348.92	-217.83	160.30
5	44	-80.00	-1490.47	-227.86	-168.48	-1785.15	1801.47	268.46
5	44	-40.00	-1274.29	-116.36	281.06	-980.85	1.337e+04	378.50
5	56	-305.00	-3165.92	-434.86	-767.33	1.268e+04	2.763e+04	-905.04
5	56	-270.00	-2955.84	-472.69	-1126.35	8587.92	-5441.26	-950.56
5	56	-231.67	-2495.01	-486.69	-729.54	-5066.84	-6049.15	-473.90
5	56	-231.67	-2495.01	-486.69	-729.54	-5066.84	-6049.15	-473.90
5	56	-193.33	-2395.16	-457.34	-627.62	-9480.60	-2834.64	-44.21
5	56	-193.33	-2395.16	-457.34	-627.62	-9480.60	-2834.64	-44.21
5	56	-155.00	-2195.50	-406.05	-532.39	-6732.75	-1253.97	206.64
5	56	-116.67	-1794.27	-356.51	-397.91	-3981.41	-202.62	504.69
5	56	-116.67	-1794.27	-356.51	-397.91	-3981.41	-202.62	504.69
5	56	-80.00	-1477.06	-303.46	-172.94	-1837.19	1926.28	721.50
5	56	-40.00	-1259.61	-123.35	279.12	-1203.71	1.332e+04	409.39
5	69	-305.00	-4411.99	114.81	-731.90	4195.02	2.700e+04	-565.93
5	69	-270.00	-4142.18	76.98	-1090.92	371.34	-6052.57	-677.90
5	69	-231.67	-3684.63	55.81	-726.16	3843.17	-5825.77	-443.40
5	69	-231.67	-3684.63	55.81	-726.16	3843.17	-5825.77	-443.40
5	69	-193.33	-3236.35	42.21	-624.28	6466.07	-2614.06	-221.72
5	69	-193.33	-3236.35	42.21	-624.28	6466.07	-2614.06	-221.72
5	69	-155.00	-2726.39	23.10	-527.37	6905.98	-978.56	-157.91
5	69	-116.67	-2158.98	7.85	-392.86	5092.84	105.81	-176.99
5	69	-116.67	-2158.98	7.85	-392.86	5092.84	105.81	-176.99
5	69	-80.00	-1633.81	-17.40	-170.64	448.47	2383.86	-6.78
5	69	-40.00	-1305.37	-52.00	277.81	-1511.86	1.360e+04	303.31
5	72	-305.00	-2970.61	-347.23	-798.94	6518.63	2.818e+04	-708.13
5	72	-270.00	-2771.55	-385.06	-1157.97	2840.71	-4893.37	-762.12
5	72	-231.67	-2372.37	-404.53	-732.71	-3382.54	-6131.95	-202.42
5	72	-231.67	-2372.37	-404.53	-732.71	-3382.54	-6131.95	-202.42
5	72	-193.33	-2203.68	-402.26	-627.83	-4195.13	-3000.39	334.02
5	72	-193.33	-2203.68	-402.26	-627.83	-4195.13	-3000.39	334.02
5	72	-155.00	-1986.15	-371.03	-532.66	-1786.92	-1404.09	593.19
5	72	-116.67	-1646.96	-346.67	-399.14	-205.85	-378.70	734.17
5	72	-116.67	-1646.96	-346.67	-399.14	-205.85	-378.70	734.17
5	72	-80.00	-1413.48	-309.77	-169.24	2294.42	1786.23	743.35

SCARICATORE IN VIA PUCCI

5	72	-40.00	-1241.53	-228.56	295.75	1209.27	1.343e+04	552.31
5	73	-305.00	-2636.65	-290.68	-865.23	2823.00	2.928e+04	-258.25
5	73	-270.00	-2688.28	-337.69	-1154.56	-899.71	-6058.57	469.55
5	73	-231.67	-2673.96	-346.32	-742.15	1490.03	-7272.37	787.88
5	73	-231.67	-2673.96	-346.32	-742.15	1490.03	-7272.37	787.88
5	73	-193.33	-2674.99	-307.44	-632.10	6694.18	-4453.70	810.99
5	73	-193.33	-2674.99	-307.44	-632.10	6694.18	-4453.70	810.99
5	73	-155.00	-2450.96	-235.88	-531.22	1.040e+04	-2978.83	373.37
5	73	-116.67	-1922.35	-163.92	-394.54	9589.74	-1908.32	-183.64
5	73	-116.67	-1922.35	-163.92	-394.54	9589.74	-1908.32	-183.64
5	73	-80.00	-1247.16	-125.10	-184.70	5388.74	157.55	-456.75
5	73	-40.00	-634.78	-132.16	258.78	392.34	1.048e+04	-220.85
5	74	-305.00	-3915.05	-70.76	-739.99	5961.10	2.713e+04	-731.49
5	74	-270.00	-3610.40	-106.15	-1116.05	2257.82	-5336.46	-1020.86
5	74	-231.67	-3081.53	-129.32	-725.98	-47.61	-5641.93	-608.97
5	74	-231.67	-3081.53	-129.32	-725.98	-47.61	-5641.93	-608.97
5	74	-193.33	-2701.08	-146.08	-624.59	-235.68	-2378.95	-143.52
5	74	-193.33	-2701.08	-146.08	-624.59	-235.68	-2378.95	-143.52
5	74	-155.00	-2309.67	-156.43	-529.85	595.59	-732.42	167.67
5	74	-116.67	-1883.39	-168.82	-396.59	640.16	311.17	384.22
5	74	-116.67	-1883.39	-168.82	-396.59	640.16	311.17	384.22
5	74	-80.00	-1585.72	-171.32	-166.82	346.89	2557.48	566.16
5	74	-40.00	-1431.80	-140.23	292.05	-289.43	1.422e+04	586.72
5	75	-305.00	-2676.56	-292.52	-865.70	2852.19	2.931e+04	-258.49
5	75	-270.00	-2726.88	-339.67	-1155.43	-925.07	-6048.67	473.00
5	75	-231.67	-2709.56	-348.36	-742.43	1453.03	-7285.92	796.23
5	75	-231.67	-2709.56	-348.36	-742.43	1453.03	-7285.92	796.23
5	75	-193.33	-2705.19	-309.53	-632.05	6675.66	-4470.36	821.95
5	75	-193.33	-2705.19	-309.53	-632.05	6675.66	-4470.36	821.95
5	75	-155.00	-2473.89	-237.94	-531.08	1.041e+04	-2990.86	384.41
5	75	-116.67	-1937.09	-165.88	-394.31	9606.51	-1912.96	-173.72
5	75	-116.67	-1937.09	-165.88	-394.31	9606.51	-1912.96	-173.72
5	75	-80.00	-1254.20	-126.99	-184.14	5408.97	166.99	-448.37
5	75	-40.00	-636.10	-134.25	260.51	394.56	1.053e+04	-217.59
5	76	-305.00	-3954.97	-72.59	-740.46	5990.28	2.716e+04	-731.72
5	76	-270.00	-3649.01	-108.13	-1116.92	2232.46	-5326.57	-1017.40
5	76	-231.67	-3117.14	-131.37	-726.26	-84.62	-5655.48	-600.61
5	76	-231.67	-3117.14	-131.37	-726.26	-84.62	-5655.48	-600.61
5	76	-193.33	-2731.27	-148.17	-624.54	-254.20	-2395.60	-132.56
5	76	-193.33	-2731.27	-148.17	-624.54	-254.20	-2395.60	-132.56
5	76	-155.00	-2332.60	-158.49	-529.72	598.75	-744.45	178.71
5	76	-116.67	-1898.13	-170.79	-396.36	656.94	306.52	394.15
5	76	-116.67	-1898.13	-170.79	-396.36	656.94	306.52	394.15
5	76	-80.00	-1592.77	-173.21	-166.25	367.12	2566.92	574.55
5	76	-40.00	-1433.12	-142.31	293.78	-287.21	1.428e+04	589.98

M_S	N memb.	V memb.	V orto	M memb.	M orto	T
	-5504.91	-673.10	-1504.40	-1.601e+04	-9508.27	-1774.71
	-631.48	247.53	393.24	1.787e+04	3.819e+04	1098.13

Macro	Tipo	Angolo 1-Z (gradi)
7	Setto	0.0

M_S	Cmb	Z	N memb.	V memb.	V orto	M memb.	M orto	T
		cm	daN	daN	daN	daN cm	daN cm	daN cm
7	4	-270.00	-3.536e+04	-3349.80	1.184e+04	4.511e+05	-4.985e+05	1.379e+04
7	4	-231.67	-3.477e+04	-3523.64	1.146e+04	2.709e+05	-5.178e+04	2.303e+04
7	4	-231.67	-3.477e+04	-3523.64	1.146e+04	2.709e+05	-5.178e+04	2.303e+04
7	4	-193.33	-3.295e+04	-3507.43	5053.96	1.210e+05	1.173e+05	1.231e+04
7	4	-193.33	-3.295e+04	-3507.43	5053.96	1.210e+05	1.173e+05	1.231e+04
7	4	-155.00	-3.099e+04	-3309.41	345.55	-3.036e+04	1.010e+05	5018.98
7	4	-116.67	-2.900e+04	-3076.86	-3666.21	-1.659e+05	-5.608e+04	-4533.97
7	4	-116.67	-2.900e+04	-3076.86	-3666.21	-1.659e+05	-5.608e+04	-4533.97
7	4	-80.00	-2.767e+04	-2918.26	-7496.85	-1.529e+05	-3.252e+05	-1.666e+04
7	4	-79.86	-2.763e+04	-3040.32	-7644.94	-1.614e+05	-3.258e+05	-1.535e+04
7	4	-79.73	-2.757e+04	-2976.83	-7854.14	-1.710e+05	-3.261e+05	-1.199e+04
7	4	-79.59	-2.748e+04	-2937.98	-8087.81	-1.828e+05	-3.266e+05	-8677.28
7	4	-79.46	-2.739e+04	-2916.52	-8327.90	-1.915e+05	-3.275e+05	-6239.10
7	4	-79.32	-2.729e+04	-2906.54	-8568.47	-1.968e+05	-3.287e+05	-4940.66
7	4	-79.18	-2.720e+04	-2903.78	-8809.30	-1.984e+05	-3.300e+05	-4841.03
7	4	-79.04	-2.710e+04	-2904.49	-9039.57	-1.963e+05	-3.315e+05	-5981.82
7	4	-78.95	-2.705e+04	-2918.32	-9203.44	-1.937e+05	-3.323e+05	-7363.39
7	4	-78.90	-2.700e+04	-2916.15	-9335.41	-1.896e+05	-3.327e+05	-8310.06
7	4	-78.76	-2.691e+04	-2915.11	-9533.22	-1.803e+05	-3.341e+05	-1.157e+04

SCARICATORE IN VIA PUCCI

7	4	-78.66	-2.686e+04	-2925.47	-9691.45	-1.733e+05	-3.348e+05	-1.415e+04
7	4	-78.62	-2.686e+04	-2925.47	-9691.45	-1.733e+05	-3.348e+05	-1.415e+04
7	4	-78.53	-2.678e+04	-2935.89	-9919.89	-1.596e+05	-3.357e+05	-1.807e+04
7	4	-78.47	-2.674e+04	-2933.46	-1.004e+04	-1.527e+05	-3.360e+05	-1.962e+04
7	4	-78.33	-2.660e+04	-2880.16	-1.017e+04	-1.198e+05	-3.370e+05	-2.180e+04
7	4	-40.00	-2.727e+04	-2843.17	-1.129e+04	-3.354e+04	-7.479e+05	-1.331e+04
7	7	-270.00	-1.238e+04	-2265.55	9583.19	2.059e+05	-3.844e+05	1837.22
7	7	-231.67	-1.247e+04	-2344.29	9373.17	1.975e+05	-2.108e+04	1625.19
7	7	-231.67	-1.247e+04	-2344.29	9373.17	1.975e+05	-2.108e+04	1625.19
7	7	-193.33	-1.168e+04	-2239.40	4589.81	2.185e+05	1.326e+05	758.79
7	7	-193.33	-1.168e+04	-2239.40	4589.81	2.185e+05	1.326e+05	758.79
7	7	-155.00	-1.062e+04	-1978.39	1242.28	1.935e+05	1.517e+05	1732.03
7	7	-116.67	-9295.96	-1707.80	-1390.65	1.170e+05	7.632e+04	2056.42
7	7	-116.67	-9295.96	-1707.80	-1390.65	1.170e+05	7.632e+04	2056.42
7	7	-80.00	-8005.65	-1567.66	-3699.23	4.530e+04	-6.701e+04	227.33
7	7	-79.86	-7923.33	-1624.00	-3819.89	2.765e+04	-6.752e+04	-265.22
7	7	-79.73	-7853.41	-1615.37	-3981.89	1.548e+04	-6.773e+04	-430.34
7	7	-79.59	-7782.35	-1609.56	-4149.86	5744.33	-6.793e+04	-371.51
7	7	-79.46	-7711.08	-1605.64	-4320.15	-1339.65	-6.827e+04	-216.02
7	7	-79.32	-7638.98	-1603.33	-4491.44	-5799.07	-6.875e+04	-83.45
7	7	-79.18	-7566.76	-1602.46	-4663.54	-7559.18	-6.932e+04	-48.33
7	7	-79.04	-7492.73	-1602.49	-4827.44	-6559.83	-6.997e+04	-131.70
7	7	-78.95	-7448.44	-1605.68	-4945.61	-4608.02	-7.032e+04	-241.97
7	7	-78.90	-7410.10	-1604.59	-5042.29	-2040.74	-7.045e+04	-301.24
7	7	-78.76	-7344.40	-1602.35	-5182.28	4187.72	-7.103e+04	-406.79
7	7	-78.66	-7299.79	-1602.08	-5297.11	9725.77	-7.130e+04	-407.47
7	7	-78.62	-7299.79	-1602.08	-5297.11	9725.77	-7.130e+04	-407.47
7	7	-78.53	-7227.18	-1597.77	-5466.37	2.107e+04	-7.169e+04	-226.67
7	7	-78.47	-7190.70	-1592.58	-5561.97	2.780e+04	-7.186e+04	-121.01
7	7	-78.33	-7100.98	-1558.97	-5675.70	4.689e+04	-7.269e+04	177.86
7	7	-40.00	-7037.70	-1575.55	-5888.06	2.434e+04	-2.942e+05	-1040.42
7	15	-270.00	-2.150e+04	-5568.23	9551.94	5.410e+05	-3.989e+05	1.014e+04
7	15	-231.67	-2.112e+04	-5683.79	9279.59	4.213e+05	-4.895e+04	1.390e+04
7	15	-231.67	-2.112e+04	-5683.79	9279.59	4.213e+05	-4.895e+04	1.390e+04
7	15	-193.33	-2.018e+04	-5488.98	4287.01	2.994e+05	9.615e+04	6291.54
7	15	-193.33	-2.018e+04	-5488.98	4287.01	2.994e+05	9.615e+04	6291.54
7	15	-155.00	-1.910e+04	-5107.19	722.33	1.886e+05	9.747e+04	1280.02
7	15	-116.67	-1.784e+04	-4628.03	-2264.20	5.651e+04	-1.030e+04	-3532.89
7	15	-116.67	-1.784e+04	-4628.03	-2264.20	5.651e+04	-1.030e+04	-3532.89
7	15	-80.00	-1.724e+04	-4177.74	-5073.40	8.508e+04	-1.844e+05	-1.040e+04
7	15	-79.86	-1.711e+04	-4166.30	-5205.67	5.744e+04	-1.855e+05	-9840.84
7	15	-79.73	-1.707e+04	-4101.12	-5379.70	4.996e+04	-1.859e+05	-8049.29
7	15	-79.59	-1.699e+04	-4052.28	-5559.36	4.006e+04	-1.862e+05	-6217.67
7	15	-79.46	-1.690e+04	-4013.03	-5748.14	3.150e+04	-1.866e+05	-4903.22
7	15	-79.32	-1.682e+04	-3979.93	-5937.63	2.637e+04	-1.873e+05	-4151.29
7	15	-79.18	-1.675e+04	-3950.62	-6126.14	2.491e+04	-1.881e+05	-4045.39
7	15	-79.04	-1.668e+04	-3922.24	-6301.35	2.614e+04	-1.891e+05	-4624.33
7	15	-78.95	-1.666e+04	-3915.49	-6423.27	2.730e+04	-1.891e+05	-5361.33
7	15	-78.90	-1.663e+04	-3916.64	-6521.73	2.949e+04	-1.886e+05	-5864.73
7	15	-78.76	-1.660e+04	-3921.96	-6665.06	3.300e+04	-1.878e+05	-7587.84
7	15	-78.66	-1.658e+04	-3915.34	-6781.36	3.503e+04	-1.873e+05	-8890.98
7	15	-78.62	-1.658e+04	-3915.34	-6781.36	3.503e+04	-1.873e+05	-8890.98
7	15	-78.53	-1.655e+04	-3899.18	-6951.46	3.993e+04	-1.867e+05	-1.079e+04
7	15	-78.47	-1.654e+04	-3886.23	-7045.11	4.303e+04	-1.867e+05	-1.151e+04
7	15	-78.33	-1.645e+04	-3812.39	-7147.21	6.216e+04	-1.876e+05	-1.236e+04
7	15	-40.00	-1.681e+04	-3798.95	-7812.22	1.339e+05	-4.746e+05	-7646.63
7	24	-270.00	-2.314e+04	-4349.10	9107.68	5.617e+05	-3.815e+05	1.187e+04
7	24	-231.67	-2.283e+04	-4464.66	8835.32	4.450e+05	-3.154e+04	1.766e+04
7	24	-231.67	-2.283e+04	-4464.66	8835.32	4.450e+05	-3.154e+04	1.766e+04
7	24	-193.33	-2.170e+04	-4524.57	4056.19	3.095e+05	1.026e+05	1.235e+04
7	24	-193.33	-2.170e+04	-4524.57	4056.19	3.095e+05	1.026e+05	1.235e+04
7	24	-155.00	-2.018e+04	-4253.20	536.74	1.633e+05	9.515e+04	5414.80
7	24	-116.67	-1.841e+04	-3875.45	-2398.21	9773.40	-1.904e+04	-450.33
7	24	-116.67	-1.841e+04	-3875.45	-2398.21	9773.40	-1.904e+04	-450.33
7	24	-80.00	-1.721e+04	-3528.67	-5096.28	-4.774e+04	-2.081e+05	-8729.95
7	24	-79.86	-1.720e+04	-3599.64	-5182.96	-4.902e+04	-2.079e+05	-8141.77
7	24	-79.73	-1.705e+04	-3553.77	-5330.65	-7.482e+04	-2.072e+05	-6307.69
7	24	-79.59	-1.693e+04	-3521.95	-5505.83	-9.052e+04	-2.052e+05	-4416.33
7	24	-79.46	-1.683e+04	-3498.84	-5683.92	-1.007e+05	-2.047e+05	-3083.35
7	24	-79.32	-1.673e+04	-3481.01	-5861.34	-1.065e+05	-2.055e+05	-2352.11
7	24	-79.18	-1.665e+04	-3465.51	-6037.34	-1.082e+05	-2.064e+05	-2294.81
7	24	-79.04	-1.657e+04	-3449.30	-6208.19	-1.066e+05	-2.074e+05	-2941.65
7	24	-78.95	-1.654e+04	-3443.82	-6333.46	-1.049e+05	-2.079e+05	-3725.99
7	24	-78.90	-1.650e+04	-3422.76	-6435.07	-1.022e+05	-2.081e+05	-4256.72
7	24	-78.76	-1.645e+04	-3370.66	-6582.17	-9.674e+04	-2.089e+05	-6043.04
7	24	-78.66	-1.642e+04	-3357.07	-6696.20	-9.284e+04	-2.088e+05	-7435.75
7	24	-78.62	-1.642e+04	-3357.07	-6696.20	-9.284e+04	-2.088e+05	-7435.75
7	24	-78.53	-1.637e+04	-3324.22	-6863.12	-8.478e+04	-2.089e+05	-9435.84
7	24	-78.47	-1.635e+04	-3302.49	-6955.80	-8.027e+04	-2.091e+05	-1.020e+04

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

7	24	-78.33	-1.628e+04	-3204.34	-7068.24	-6.325e+04	-2.101e+05	-1.127e+04
7	24	-40.00	-1.675e+04	-3189.96	-7733.30	4.500e+04	-4.961e+05	-6645.06
7	25	-270.00	-1.939e+04	-1991.31	9823.20	2.220e+05	-4.075e+05	6996.89
7	25	-231.67	-1.940e+04	-2106.87	9550.85	1.236e+05	-5.744e+04	9853.03
7	25	-231.67	-1.940e+04	-2106.87	9550.85	1.236e+05	-5.744e+04	9853.03
7	25	-193.33	-1.872e+04	-2020.35	4435.54	8.724e+04	9.696e+04	2921.88
7	25	-193.33	-1.872e+04	-2020.35	4435.54	8.724e+04	9.696e+04	2921.88
7	25	-155.00	-1.802e+04	-1837.84	776.17	5.238e+04	1.067e+05	-542.20
7	25	-116.67	-1.722e+04	-1706.08	-2253.12	7181.83	7016.58	-4843.99
7	25	-116.67	-1.722e+04	-1706.08	-2253.12	7181.83	7016.58	-4843.99
7	25	-80.00	-1.651e+04	-1672.13	-5135.17	-1.302e+04	-1.808e+05	-1.028e+04
7	25	-79.86	-1.641e+04	-1658.07	-5283.97	-3.533e+04	-1.816e+05	-9703.83
7	25	-79.73	-1.638e+04	-1601.35	-5454.41	-4.064e+04	-1.820e+05	-8045.41
7	25	-79.59	-1.638e+04	-1558.69	-5640.33	-3.987e+04	-1.823e+05	-6375.41
7	25	-79.46	-1.634e+04	-1527.59	-5838.56	-4.350e+04	-1.828e+05	-5058.12
7	25	-79.32	-1.630e+04	-1506.79	-6037.26	-4.595e+04	-1.835e+05	-4308.12
7	25	-79.18	-1.624e+04	-1445.13	-6236.26	-4.686e+04	-1.843e+05	-4197.34
7	25	-79.04	-1.619e+04	-1453.44	-6422.44	-4.573e+04	-1.853e+05	-4759.30
7	25	-78.95	-1.616e+04	-1540.24	-6551.62	-4.441e+04	-1.862e+05	-5476.38
7	25	-78.90	-1.613e+04	-1547.66	-6655.88	-4.201e+04	-1.867e+05	-5967.25
7	25	-78.76	-1.609e+04	-1572.90	-6816.90	-3.730e+04	-1.883e+05	-7600.62
7	25	-78.66	-1.606e+04	-1602.04	-6944.02	-3.381e+04	-1.891e+05	-8817.42
7	25	-78.62	-1.606e+04	-1602.04	-6944.02	-3.381e+04	-1.891e+05	-8817.42
7	25	-78.53	-1.602e+04	-1655.25	-7125.66	-2.602e+04	-1.901e+05	-1.073e+04
7	25	-78.47	-1.599e+04	-1677.27	-7220.66	-2.153e+04	-1.904e+05	-1.146e+04
7	25	-78.33	-1.593e+04	-1714.21	-7304.09	-6848.20	-1.910e+05	-1.236e+04
7	25	-40.00	-1.631e+04	-1700.76	-7969.01	6.159e+04	-4.779e+05	-8033.56
7	38	-270.00	-2.605e+04	-740.54	8606.96	2.435e+05	-3.555e+05	7765.85
7	38	-231.67	-2.553e+04	-856.10	8334.61	1.556e+05	-5472.67	1.524e+04
7	38	-231.67	-2.553e+04	-856.10	8334.61	1.556e+05	-5472.67	1.524e+04
7	38	-193.33	-2.367e+04	-1080.07	3702.50	7.481e+04	1.120e+05	9915.52
7	38	-193.33	-2.367e+04	-1080.07	3702.50	7.481e+04	1.120e+05	9915.52
7	38	-155.00	-2.158e+04	-971.53	299.12	-4.905e+04	9.604e+04	7683.33
7	38	-116.67	-1.946e+04	-864.35	-2547.62	-1.746e+05	-1.613e+04	1930.06
7	38	-116.67	-1.946e+04	-864.35	-2547.62	-1.746e+05	-1.613e+04	1930.06
7	38	-80.00	-1.785e+04	-853.63	-5152.31	-1.865e+05	-2.069e+05	-6729.37
7	38	-79.86	-1.790e+04	-1073.67	-5231.08	-1.770e+05	-2.068e+05	-6251.89
7	38	-79.73	-1.781e+04	-1070.19	-5378.96	-1.916e+05	-2.068e+05	-4475.28
7	38	-79.59	-1.768e+04	-1078.93	-5544.17	-2.088e+05	-2.078e+05	-2617.27
7	38	-79.46	-1.759e+04	-1095.65	-5703.90	-2.173e+05	-2.088e+05	-1227.08
7	38	-79.32	-1.751e+04	-1115.66	-5862.88	-2.225e+05	-2.096e+05	-518.73
7	38	-79.18	-1.741e+04	-1135.99	-6022.31	-2.243e+05	-2.105e+05	-518.27
7	38	-79.04	-1.732e+04	-1156.23	-6180.92	-2.224e+05	-2.114e+05	-1243.39
7	38	-78.95	-1.725e+04	-1166.70	-6299.66	-2.194e+05	-2.120e+05	-2076.97
7	38	-78.90	-1.720e+04	-1128.50	-6396.17	-2.156e+05	-2.122e+05	-2638.42
7	38	-78.76	-1.709e+04	-1033.80	-6536.23	-2.049e+05	-2.130e+05	-4545.33
7	38	-78.66	-1.702e+04	-1029.76	-6652.47	-1.958e+05	-2.136e+05	-6086.02
7	38	-78.62	-1.702e+04	-1029.76	-6652.47	-1.958e+05	-2.136e+05	-6086.02
7	38	-78.53	-1.692e+04	-1010.77	-6819.21	-1.791e+05	-2.144e+05	-8309.39
7	38	-78.47	-1.688e+04	-995.64	-6910.89	-1.708e+05	-2.147e+05	-9201.44
7	38	-78.33	-1.672e+04	-920.17	-7027.69	-1.351e+05	-2.156e+05	-1.050e+04
7	38	-40.00	-1.702e+04	-905.08	-7692.76	-5.650e+04	-5.028e+05	-7026.45
7	47	-270.00	-2.205e+04	-4323.61	9427.95	4.408e+05	-3.925e+05	9268.96
7	47	-231.67	-2.171e+04	-4439.17	9155.59	3.304e+05	-4.251e+04	1.347e+04
7	47	-231.67	-2.171e+04	-4439.17	9155.59	3.304e+05	-4.251e+04	1.347e+04
7	47	-193.33	-2.064e+04	-4299.02	4208.68	2.288e+05	9.915e+04	6471.01
7	47	-193.33	-2.064e+04	-4299.02	4208.68	2.288e+05	9.915e+04	6471.01
7	47	-155.00	-1.943e+04	-3989.09	656.26	1.268e+05	9.852e+04	2091.42
7	47	-116.67	-1.807e+04	-3614.39	-2313.01	1.053e+04	-8832.12	-2788.44
7	47	-116.67	-1.807e+04	-3614.39	-2313.01	1.053e+04	-8832.12	-2788.44
7	47	-80.00	-1.725e+04	-3292.41	-5097.43	2.207e+04	-1.882e+05	-9711.36
7	47	-79.86	-1.716e+04	-3322.88	-5222.56	1845.35	-1.890e+05	-9162.62
7	47	-79.73	-1.711e+04	-3270.97	-5391.07	-6103.10	-1.894e+05	-7390.85
7	47	-79.59	-1.704e+04	-3234.28	-5569.13	-1.579e+04	-1.897e+05	-5576.41
7	47	-79.46	-1.696e+04	-3207.15	-5754.27	-2.374e+04	-1.902e+05	-4249.11
7	47	-79.32	-1.687e+04	-3186.03	-5940.02	-2.855e+04	-1.909e+05	-3506.44
7	47	-79.18	-1.680e+04	-3168.22	-6125.36	-3.000e+04	-1.917e+05	-3421.42
7	47	-79.04	-1.673e+04	-3150.96	-6299.42	-2.867e+04	-1.927e+05	-4028.70
7	47	-78.95	-1.670e+04	-3149.54	-6421.83	-2.714e+04	-1.929e+05	-4784.00
7	47	-78.90	-1.667e+04	-3149.27	-6520.81	-2.460e+04	-1.928e+05	-5297.96
7	47	-78.76	-1.662e+04	-3150.87	-6665.85	-1.956e+04	-1.927e+05	-7041.66
7	47	-78.66	-1.659e+04	-3148.29	-6783.23	-1.601e+04	-1.925e+05	-8376.32
7	47	-78.62	-1.659e+04	-3148.29	-6783.23	-1.601e+04	-1.925e+05	-8376.32
7	47	-78.53	-1.655e+04	-3138.87	-6954.40	-8514.52	-1.925e+05	-1.033e+04
7	47	-78.47	-1.653e+04	-3129.29	-7048.25	-4248.83	-1.925e+05	-1.108e+04
7	47	-78.33	-1.643e+04	-3067.55	-7150.80	1.686e+04	-1.934e+05	-1.203e+04
7	47	-40.00	-1.678e+04	-3053.80	-7815.81	8.970e+04	-4.803e+05	-7561.90
7	56	-270.00	-2.302e+04	-3617.41	9164.38	4.584e+05	-3.823e+05	1.033e+04
7	56	-231.67	-2.271e+04	-3732.97	8892.03	3.493e+05	-3.230e+04	1.577e+04

SCARICATORE IN VIA PUCCI

7	56	-231.67	-2.271e+04	-3732.97	8892.03	3.493e+05	-3.230e+04	1.577e+04
7	56	-193.33	-2.154e+04	-3751.43	4073.25	2.387e+05	1.029e+05	1.016e+04
7	56	-193.33	-2.154e+04	-3751.43	4073.25	2.387e+05	1.029e+05	1.016e+04
7	56	-155.00	-2.006e+04	-3511.26	548.04	1.152e+05	9.707e+04	4507.99
7	56	-116.67	-1.840e+04	-3197.67	-2390.45	-1.558e+04	-1.415e+04	-975.69
7	56	-116.67	-1.840e+04	-3197.67	-2390.45	-1.558e+04	-1.415e+04	-975.69
7	56	-80.00	-1.723e+04	-2935.05	-5109.67	-5.533e+04	-2.024e+05	-8752.91
7	56	-79.86	-1.721e+04	-3012.58	-5207.74	-5.997e+04	-2.024e+05	-8178.90
7	56	-79.73	-1.710e+04	-2971.51	-5360.73	-7.908e+04	-2.021e+05	-6382.44
7	56	-79.59	-1.700e+04	-2944.30	-5536.05	-9.247e+04	-2.010e+05	-4532.18
7	56	-79.46	-1.691e+04	-2926.17	-5714.71	-1.014e+05	-2.009e+05	-3193.79
7	56	-79.32	-1.682e+04	-2913.62	-5893.23	-1.067e+05	-2.018e+05	-2462.82
7	56	-79.18	-1.674e+04	-2903.78	-6071.09	-1.083e+05	-2.027e+05	-2405.57
7	56	-79.04	-1.666e+04	-2893.97	-6242.72	-1.068e+05	-2.036e+05	-3051.24
7	56	-78.95	-1.662e+04	-2893.50	-6367.32	-1.049e+05	-2.041e+05	-3832.77
7	56	-78.90	-1.658e+04	-2879.78	-6468.29	-1.021e+05	-2.043e+05	-4361.70
7	56	-78.76	-1.653e+04	-2846.15	-6615.80	-9.593e+04	-2.052e+05	-6138.65
7	56	-78.66	-1.649e+04	-2838.80	-6731.85	-9.132e+04	-2.053e+05	-7527.34
7	56	-78.62	-1.649e+04	-2838.80	-6731.85	-9.132e+04	-2.053e+05	-7527.34
7	56	-78.53	-1.644e+04	-2818.93	-6901.09	-8.204e+04	-2.056e+05	-9543.05
7	56	-78.47	-1.641e+04	-2804.02	-6994.37	-7.699e+04	-2.058e+05	-1.032e+04
7	56	-78.33	-1.633e+04	-2727.53	-7102.66	-5.738e+04	-2.067e+05	-1.139e+04
7	56	-40.00	-1.674e+04	-2713.22	-7767.69	-3.788e+04	-4.930e+05	-6970.86
7	57	-270.00	-2.070e+04	-2130.70	9606.60	2.427e+05	-3.983e+05	7315.82
7	57	-231.67	-2.059e+04	-2246.25	9334.24	1.454e+05	-4.830e+04	1.096e+04
7	57	-231.67	-2.059e+04	-2246.25	9334.24	1.454e+05	-4.830e+04	1.096e+04
7	57	-193.33	-1.970e+04	-2168.13	4305.71	9.691e+04	9.948e+04	4427.61
7	57	-193.33	-1.970e+04	-2168.13	4305.71	9.691e+04	9.948e+04	4427.61
7	57	-155.00	-1.873e+04	-1980.41	691.68	4.254e+04	1.043e+05	940.96
7	57	-116.67	-1.766e+04	-1819.63	-2305.67	-2.055e+04	1666.69	-3611.90
7	57	-116.67	-1.766e+04	-1819.63	-2305.67	-2.055e+04	1666.69	-3611.90
7	57	-80.00	-1.679e+04	-1754.76	-5133.80	-3.745e+04	-1.861e+05	-9682.80
7	57	-79.86	-1.671e+04	-1781.13	-5269.37	-5.475e+04	-1.868e+05	-9113.24
7	57	-79.73	-1.667e+04	-1733.60	-5436.32	-6.140e+04	-1.871e+05	-7422.13
7	57	-79.59	-1.665e+04	-1700.05	-5618.53	-6.426e+04	-1.874e+05	-5703.95
7	57	-79.46	-1.660e+04	-1677.45	-5809.74	-6.904e+04	-1.880e+05	-4373.64
7	57	-79.32	-1.654e+04	-1663.70	-6001.54	-7.211e+04	-1.887e+05	-3630.17
7	57	-79.18	-1.648e+04	-1626.75	-6193.78	-7.322e+04	-1.896e+05	-3538.23
7	57	-79.04	-1.642e+04	-1631.63	-6375.06	-7.195e+04	-1.906e+05	-4129.56
7	57	-78.95	-1.639e+04	-1687.94	-6502.13	-7.035e+04	-1.913e+05	-4868.82
7	57	-78.90	-1.635e+04	-1692.36	-6604.71	-6.771e+04	-1.917e+05	-5373.06
7	57	-78.76	-1.630e+04	-1708.82	-6760.81	-6.205e+04	-1.931e+05	-7060.90
7	57	-78.66	-1.627e+04	-1729.45	-6885.06	-5.769e+04	-1.938e+05	-8343.95
7	57	-78.62	-1.627e+04	-1729.45	-6885.06	-5.769e+04	-1.938e+05	-8343.95
7	57	-78.53	-1.621e+04	-1764.12	-7063.87	-4.857e+04	-1.946e+05	-1.031e+04
7	57	-78.47	-1.618e+04	-1776.57	-7158.71	-4.352e+04	-1.948e+05	-1.106e+04
7	57	-78.33	-1.610e+04	-1784.55	-7250.07	-2.516e+04	-1.955e+05	-1.204e+04
7	57	-40.00	-1.646e+04	-1770.79	-7915.03	4.589e+04	-4.824e+05	-7770.14
7	70	-270.00	-2.460e+04	-1478.09	8869.62	2.755e+05	-3.674e+05	7834.64
7	70	-231.67	-2.418e+04	-1593.65	8597.26	1.828e+05	-1.744e+04	1.425e+04
7	70	-231.67	-2.418e+04	-1593.65	8597.26	1.828e+05	-1.744e+04	1.425e+04
7	70	-193.33	-2.259e+04	-1720.19	3866.69	1.033e+05	1.081e+05	8625.84
7	70	-193.33	-2.259e+04	-1720.19	3866.69	1.033e+05	1.081e+05	8625.84
7	70	-155.00	-2.081e+04	-1586.79	411.19	-6500.43	9.767e+04	5805.13
7	70	-116.67	-1.897e+04	-1441.01	-2475.80	-1.210e+05	-1.220e+04	337.42
7	70	-116.67	-1.897e+04	-1441.01	-2475.80	-1.210e+05	-1.220e+04	337.42
7	70	-80.00	-1.759e+04	-1377.79	-5141.23	-1.349e+05	-2.015e+05	-7639.40
7	70	-79.86	-1.759e+04	-1538.51	-5235.52	-1.334e+05	-2.016e+05	-7133.14
7	70	-79.73	-1.752e+04	-1520.18	-5389.01	-1.461e+05	-2.017e+05	-5374.29
7	70	-79.59	-1.741e+04	-1515.00	-5558.46	-1.604e+05	-2.025e+05	-3545.90
7	70	-79.46	-1.733e+04	-1518.51	-5726.12	-1.683e+05	-2.033e+05	-2172.72
7	70	-79.32	-1.725e+04	-1526.77	-5893.57	-1.731e+05	-2.041e+05	-1453.41
7	70	-79.18	-1.716e+04	-1537.54	-6061.40	-1.748e+05	-2.049e+05	-1424.48
7	70	-79.04	-1.707e+04	-1550.10	-6225.48	-1.731e+05	-2.059e+05	-2108.09
7	70	-78.95	-1.702e+04	-1560.18	-6346.05	-1.705e+05	-2.064e+05	-2912.27
7	70	-78.90	-1.697e+04	-1536.59	-6443.93	-1.671e+05	-2.067e+05	-3456.00
7	70	-78.76	-1.688e+04	-1478.28	-6587.19	-1.581e+05	-2.075e+05	-5307.00
7	70	-78.66	-1.683e+04	-1477.17	-6704.62	-1.506e+05	-2.081e+05	-6782.21
7	70	-78.62	-1.683e+04	-1477.17	-6704.62	-1.506e+05	-2.081e+05	-6782.21
7	70	-78.53	-1.674e+04	-1466.63	-6873.96	-1.366e+05	-2.088e+05	-8924.01
7	70	-78.47	-1.670e+04	-1456.15	-6966.69	-1.294e+05	-2.090e+05	-9773.76
7	70	-78.33	-1.657e+04	-1394.58	-7077.52	-9.896e+04	-2.099e+05	-1.097e+04
7	70	-40.00	-1.689e+04	-1379.82	-7742.56	-2.155e+04	-4.970e+05	-7199.59
7	75	-270.00	-1.247e+04	-2312.13	9561.67	2.163e+05	-3.828e+05	1863.02
7	75	-231.67	-1.256e+04	-2393.42	9359.06	2.059e+05	-2.014e+04	1761.50
7	75	-231.67	-1.256e+04	-2393.42	9359.06	2.059e+05	-2.014e+04	1761.50
7	75	-193.33	-1.174e+04	-2289.30	4579.18	2.241e+05	1.331e+05	927.96
7	75	-193.33	-1.174e+04	-2289.30	4579.18	2.241e+05	1.331e+05	927.96
7	75	-155.00	-1.066e+04	-2027.94	1233.05	1.960e+05	1.518e+05	1908.22

SCARICATORE IN VIA PUCCI

7	75	-116.67	-9311.76	-1756.70	-1399.51	1.167e+05	7.608e+04	2200.07
7	75	-116.67	-9311.76	-1756.70	-1399.51	1.167e+05	7.608e+04	2200.07
7	75	-80.00	-8006.52	-1615.93	-3707.33	4.343e+04	-6.757e+04	293.92
7	75	-79.86	-7924.65	-1672.82	-3827.90	2.588e+04	-6.807e+04	-202.35
7	75	-79.73	-7854.83	-1663.80	-3989.82	1.373e+04	-6.828e+04	-368.15
7	75	-79.59	-7783.68	-1657.77	-4157.79	3986.25	-6.848e+04	-308.34
7	75	-79.46	-7712.32	-1653.78	-4328.08	-3103.40	-6.883e+04	-152.29
7	75	-79.32	-7640.16	-1651.46	-4499.38	-7563.60	-6.931e+04	-19.90
7	75	-79.18	-7567.90	-1650.59	-4671.48	-9322.12	-6.988e+04	14.63
7	75	-79.04	-7493.85	-1650.63	-4835.38	-8320.52	-7.053e+04	-69.42
7	75	-78.95	-7449.55	-1653.82	-4953.55	-6367.28	-7.088e+04	-180.02
7	75	-78.90	-7411.20	-1652.73	-5050.22	-3799.18	-7.101e+04	-239.43
7	75	-78.76	-7345.47	-1650.48	-5190.21	2432.82	-7.159e+04	-345.16
7	75	-78.66	-7300.82	-1650.19	-5305.04	7974.58	-7.186e+04	-345.88
7	75	-78.62	-7300.82	-1650.19	-5305.04	7974.58	-7.186e+04	-345.88
7	75	-78.53	-7228.14	-1645.86	-5474.31	1.933e+04	-7.225e+04	-165.35
7	75	-78.47	-7191.63	-1640.66	-5569.91	2.606e+04	-7.242e+04	-59.96
7	75	-78.33	-7101.73	-1607.22	-5683.62	4.519e+04	-7.325e+04	238.67
7	75	-40.00	-7036.69	-1622.98	-5896.19	2.268e+04	-2.951e+05	-1029.66
7	76	-270.00	-2.515e+04	-2499.56	9190.53	3.203e+05	-3.848e+05	9421.22
7	76	-231.67	-2.478e+04	-2624.00	8901.67	2.005e+05	-3.805e+04	1.546e+04
7	76	-231.67	-2.478e+04	-2624.00	8901.67	2.005e+05	-3.805e+04	1.546e+04
7	76	-193.33	-2.348e+04	-2598.62	3989.43	1.055e+05	9.548e+04	8175.15
7	76	-193.33	-2.348e+04	-2598.62	3989.43	1.055e+05	9.548e+04	8175.15
7	76	-155.00	-2.205e+04	-2432.07	403.08	3595.93	8.749e+04	3441.85
7	76	-116.67	-2.056e+04	-2241.46	-2622.76	-9.480e+04	-2.703e+04	-2858.60
7	76	-116.67	-2.056e+04	-2241.46	-2622.76	-9.480e+04	-2.703e+04	-2858.60
7	76	-80.00	-1.951e+04	-2117.52	-5484.92	-9.447e+04	-2.253e+05	-1.113e+04
7	76	-79.86	-1.947e+04	-2205.99	-5599.81	-1.026e+05	-2.258e+05	-1.031e+04
7	76	-79.73	-1.943e+04	-2162.80	-5760.93	-1.106e+05	-2.260e+05	-8101.59
7	76	-79.59	-1.936e+04	-2136.30	-5939.12	-1.197e+05	-2.264e+05	-5882.82
7	76	-79.46	-1.929e+04	-2121.53	-6121.87	-1.265e+05	-2.270e+05	-4237.06
7	76	-79.32	-1.921e+04	-2114.57	-6305.08	-1.306e+05	-2.279e+05	-3353.63
7	76	-79.18	-1.914e+04	-2112.61	-6488.58	-1.320e+05	-2.288e+05	-3282.07
7	76	-79.04	-1.906e+04	-2113.09	-6663.95	-1.304e+05	-2.299e+05	-4053.19
7	76	-78.95	-1.903e+04	-2122.73	-6788.96	-1.284e+05	-2.305e+05	-4988.68
7	76	-78.90	-1.898e+04	-2121.14	-6889.83	-1.253e+05	-2.308e+05	-5627.59
7	76	-78.76	-1.892e+04	-2120.16	-7040.37	-1.183e+05	-2.318e+05	-7813.39
7	76	-78.66	-1.888e+04	-2127.04	-7161.17	-1.129e+05	-2.323e+05	-9537.03
7	76	-78.62	-1.888e+04	-2127.04	-7161.17	-1.129e+05	-2.323e+05	-9537.03
7	76	-78.53	-1.881e+04	-2133.43	-7336.03	-1.023e+05	-2.329e+05	-1.212e+04
7	76	-78.47	-1.879e+04	-2131.13	-7430.05	-9.679e+04	-2.331e+05	-1.314e+04
7	76	-78.33	-1.868e+04	-2090.98	-7529.74	-7.233e+04	-2.339e+05	-1.455e+04
7	76	-40.00	-1.912e+04	-2069.16	-8307.88	2.687e+04	-5.371e+05	-9019.35

M_S	N memb.	V memb.	V orto	M memb.	M orto	T
	-3.536e+04	-5683.79	-1.129e+04	-2.243e+05	-7.479e+05	-2.180e+04
	-7036.69	-740.54	1.184e+04	5.617e+05	1.518e+05	2.303e+04

Macro	Tipo	Angolo 1-Z (gradi)
8	Setto	0.0

M_S	Cmb	Z cm	N memb. daN	V memb. daN	V orto daN	M memb. daN cm	M orto daN cm	T daN cm
8	2	-270.00	-1.629e+04	826.42	2120.96	-4.777e+04	-7.529e+04	-1981.73
8	2	-231.67	-1.675e+04	975.98	1810.93	-2.833e+04	70.57	977.83
8	2	-231.67	-1.675e+04	975.98	1810.93	-2.833e+04	70.57	977.83
8	2	-193.33	-1.657e+04	1038.32	885.29	2.015e+04	9717.87	2415.69
8	2	-193.33	-1.657e+04	1038.32	885.29	2.015e+04	9717.87	2415.69
8	2	-155.00	-1.651e+04	1069.18	558.09	7.640e+04	5519.99	1963.69
8	2	-116.67	-1.653e+04	1083.05	-31.97	1.185e+05	-7719.60	596.72
8	2	-116.67	-1.653e+04	1083.05	-31.97	1.185e+05	-7719.60	596.72
8	2	-80.00	-1.563e+04	1008.26	-1264.46	1.159e+05	-4.666e+04	-2483.86
8	2	-40.00	-1.312e+04	637.10	-3388.25	6.131e+04	-1.656e+05	6591.08
8	4	-270.00	-1.629e+04	851.41	2118.36	-4.979e+04	-7.520e+04	-2031.74
8	4	-231.67	-1.674e+04	1006.76	1809.83	-2.995e+04	92.30	1007.21
8	4	-231.67	-1.674e+04	1006.76	1809.83	-2.995e+04	92.30	1007.21
8	4	-193.33	-1.657e+04	1070.82	885.04	2.023e+04	9716.78	2477.32
8	4	-193.33	-1.657e+04	1070.82	885.04	2.023e+04	9716.78	2477.32
8	4	-155.00	-1.651e+04	1102.12	558.07	7.848e+04	5514.86	2016.20
8	4	-116.67	-1.653e+04	1116.14	-32.03	1.223e+05	-7725.49	629.50
8	4	-116.67	-1.653e+04	1116.14	-32.03	1.223e+05	-7725.49	629.50
8	4	-80.00	-1.563e+04	1043.33	-1264.81	1.199e+05	-4.667e+04	-2485.62
8	4	-40.00	-1.313e+04	674.17	-3388.89	6.272e+04	-1.656e+05	6672.41

SCARICATORE IN VIA PUCCI

8	5	-270.00	-5255.59	281.42	1167.60	-6320.13	-4.000e+04	-927.67
8	5	-231.67	-4699.12	325.94	1168.75	-322.92	4786.46	97.93
8	5	-231.67	-4699.12	325.94	1168.75	-322.92	4786.46	97.93
8	5	-193.33	-3684.61	341.83	575.60	1.417e+04	6025.25	823.16
8	5	-193.33	-3684.61	341.83	575.60	1.417e+04	6025.25	823.16
8	5	-155.00	-3133.91	348.05	455.09	3.257e+04	996.82	751.46
8	5	-116.67	-3145.01	337.15	328.38	4.729e+04	-2857.89	426.81
8	5	-116.67	-3145.01	337.15	328.38	4.729e+04	-2857.89	426.81
8	5	-80.00	-3274.90	271.07	30.35	4.726e+04	-8874.70	-571.04
8	5	-40.00	-2788.28	115.51	-911.76	3.014e+04	-4.528e+04	2261.91
8	14	-270.00	-8021.79	961.00	1599.70	-7.582e+04	-5.498e+04	-1812.12
8	14	-231.67	-8248.15	1055.32	1434.94	-5.140e+04	-1048.27	313.95
8	14	-231.67	-8248.15	1055.32	1434.94	-5.140e+04	-1048.27	313.95
8	14	-193.33	-8177.94	1116.18	671.59	-2.193e+04	7520.67	1988.62
8	14	-193.33	-8177.94	1116.18	671.59	-2.193e+04	7520.67	1988.62
8	14	-155.00	-8539.95	1250.50	437.20	4.584e+04	3948.48	1848.05
8	14	-116.67	-8613.64	1248.90	73.11	1.169e+05	-4260.51	1699.63
8	14	-116.67	-8613.64	1248.90	73.11	1.169e+05	-4260.51	1699.63
8	14	-80.00	-7752.21	1036.89	-678.11	9.647e+04	-2.646e+04	-1053.93
8	14	-40.00	-7499.07	1384.72	-2181.61	4.897e+04	-1.034e+05	6979.95
8	19	-270.00	-1.265e+04	346.49	1382.05	-2.483e+04	-4.981e+04	-1100.31
8	19	-231.67	-1.257e+04	440.81	1217.29	-2.117e+04	4092.70	635.92
8	19	-231.67	-1.257e+04	440.81	1217.29	-2.117e+04	4092.70	635.92
8	19	-193.33	-1.181e+04	429.61	626.38	2.245e+04	6553.95	1217.24
8	19	-193.33	-1.181e+04	429.61	626.38	2.245e+04	6553.95	1217.24
8	19	-155.00	-1.110e+04	519.99	437.12	6.196e+04	2608.74	1038.27
8	19	-116.67	-1.101e+04	390.05	77.33	5.935e+04	-5676.58	633.82
8	19	-116.67	-1.101e+04	390.05	77.33	5.935e+04	-5676.58	633.82
8	19	-80.00	-1.084e+04	320.62	-651.86	2.717e+04	-2.876e+04	-1544.87
8	19	-40.00	-8347.86	1252.01	-2023.21	5.670e+04	-1.028e+05	4471.64
8	21	-270.00	-8057.53	-6.15	1583.95	7.984e+04	-5.465e+04	-473.57
8	21	-231.67	-8151.64	88.18	1419.19	7.849e+04	-730.85	813.53
8	21	-231.67	-8151.64	88.18	1419.19	7.849e+04	-730.85	813.53
8	21	-193.33	-8198.99	98.82	665.29	8.667e+04	7544.12	1049.35
8	21	-193.33	-8198.99	98.82	665.29	8.667e+04	7544.12	1049.35
8	21	-155.00	-8139.47	71.51	436.43	5.842e+04	3873.59	718.16
8	21	-116.67	-8528.43	245.62	90.78	3.613e+04	-4349.92	-365.48
8	21	-116.67	-8528.43	245.62	90.78	3.613e+04	-4349.92	-365.48
8	21	-80.00	-7798.57	222.77	-672.21	3.616e+04	-2.638e+04	-1579.89
8	21	-40.00	-7290.13	-1139.63	-2142.11	3.991e+04	-1.010e+05	3402.99
8	40	-270.00	-1.084e+04	1903.92	1478.59	-2.385e+05	-5.229e+04	-3459.34
8	40	-231.67	-1.110e+04	1998.24	1313.83	-1.873e+05	1643.81	-125.87
8	40	-231.67	-1.110e+04	1998.24	1313.83	-1.873e+05	1643.81	-125.87
8	40	-193.33	-1.043e+04	2166.68	652.42	-1.317e+05	6807.00	3013.62
8	40	-193.33	-1.043e+04	2166.68	652.42	-1.317e+05	6807.00	3013.62
8	40	-155.00	-1.082e+04	2143.67	438.72	3.505e+04	3093.73	2797.11
8	40	-116.67	-1.022e+04	2022.70	79.85	1.882e+05	-5124.53	1806.80
8	40	-116.67	-1.022e+04	2022.70	79.85	1.882e+05	-5124.53	1806.80
8	40	-80.00	-9894.64	1894.75	-672.64	2.363e+05	-2.813e+04	-1228.88
8	40	-40.00	-8153.46	1879.66	-2085.91	2.351e+04	-1.036e+05	5498.18
8	46	-270.00	-8945.62	753.52	1555.77	-5.155e+04	-5.395e+04	-1593.49
8	46	-231.67	-9108.50	847.84	1391.01	-3.235e+04	-24.36	410.87
8	46	-231.67	-9108.50	847.84	1391.01	-3.235e+04	-24.36	410.87
8	46	-193.33	-8893.18	901.91	662.29	-4111.73	7328.31	1761.00
8	46	-193.33	-8893.18	901.91	662.29	-4111.73	7328.31	1761.00
8	46	-155.00	-9012.27	992.10	437.13	4.745e+04	3678.22	1571.06
8	46	-116.67	-9076.83	995.13	76.83	9.730e+04	-4554.84	1191.39
8	46	-116.67	-9076.83	995.13	76.83	9.730e+04	-4554.84	1191.39
8	46	-80.00	-8405.24	853.05	-673.12	8.483e+04	-2.693e+04	-1230.71
8	46	-40.00	-7650.77	965.70	-2142.35	4.687e+04	-1.029e+05	5857.24
8	53	-270.00	-8918.77	175.30	1547.83	4.415e+04	-5.380e+04	-798.49
8	53	-231.67	-9003.37	269.62	1383.07	4.765e+04	119.97	718.14
8	53	-231.67	-9003.37	269.62	1383.07	4.765e+04	119.97	718.14
8	53	-193.33	-8871.00	295.03	658.94	6.280e+04	7350.96	1203.09
8	53	-193.33	-8871.00	295.03	658.94	6.280e+04	7350.96	1203.09
8	53	-155.00	-8763.08	289.63	436.76	5.549e+04	3639.12	895.38
8	53	-116.67	-8998.11	402.61	88.05	4.871e+04	-4595.75	-55.00
8	53	-116.67	-8998.11	402.61	88.05	4.871e+04	-4595.75	-55.00
8	53	-80.00	-8391.51	372.71	-669.87	4.906e+04	-2.685e+04	-1548.14
8	53	-40.00	-7485.28	-524.14	-2120.18	4.108e+04	-1.014e+05	3781.63
8	56	-270.00	-1.168e+04	886.59	1429.84	-9.961e+04	-5.102e+04	-1899.89
8	56	-231.67	-1.174e+04	980.92	1265.08	-7.857e+04	2897.77	394.08
8	56	-231.67	-1.174e+04	980.92	1265.08	-7.857e+04	2897.77	394.08
8	56	-193.33	-1.107e+04	1032.28	638.33	-3.259e+04	6709.92	1897.70
8	56	-193.33	-1.107e+04	1032.28	638.33	-3.259e+04	6709.92	1897.70
8	56	-155.00	-1.077e+04	1074.54	437.65	4.664e+04	2858.66	1676.45
8	56	-116.67	-1.057e+04	969.72	79.24	1.079e+05	-5393.17	963.48
8	56	-116.67	-1.057e+04	969.72	79.24	1.079e+05	-5393.17	963.48
8	56	-80.00	-1.029e+04	879.94	-660.38	1.048e+05	-2.837e+04	-1452.10

SCARICATORE IN VIA PUCCI

8	56	-40.00	-8223.89	1286.09	-2053.36	4.324e+04	-1.030e+05	4661.46
8	72	-270.00	-1.070e+04	1356.37	1479.99	-1.579e+05	-5.229e+04	-2610.98
8	72	-231.67	-1.089e+04	1450.69	1315.23	-1.217e+05	1643.47	137.29
8	72	-231.67	-1.089e+04	1450.69	1315.23	-1.217e+05	1643.47	137.29
8	72	-193.33	-1.031e+04	1564.41	650.26	-7.587e+04	6883.65	2433.61
8	72	-193.33	-1.031e+04	1564.41	650.26	-7.587e+04	6883.65	2433.61
8	72	-155.00	-1.042e+04	1555.68	437.97	4.077e+04	3139.43	2196.40
8	72	-116.67	-1.010e+04	1482.73	81.13	1.452e+05	-5097.20	1261.44
8	72	-116.67	-1.010e+04	1482.73	81.13	1.452e+05	-5097.20	1261.44
8	72	-80.00	-9709.94	1379.34	-669.66	1.720e+05	-2.797e+04	-1339.61
8	72	-40.00	-8057.59	1266.11	-2084.94	3.057e+04	-1.031e+05	4936.08
8	73	-270.00	-5248.77	323.07	1163.27	-9677.41	-3.984e+04	-1011.02
8	73	-231.67	-4692.18	377.25	1166.91	-3014.23	4822.67	146.89
8	73	-231.67	-4692.18	377.25	1166.91	-3014.23	4822.67	146.89
8	73	-193.33	-3678.74	396.00	575.18	1.430e+04	6023.44	925.87
8	73	-193.33	-3678.74	396.00	575.18	1.430e+04	6023.44	925.87
8	73	-155.00	-3130.38	402.96	455.04	3.604e+04	988.26	838.98
8	73	-116.67	-3144.43	392.30	328.28	5.365e+04	-2867.71	481.44
8	73	-116.67	-3144.43	392.30	328.28	5.365e+04	-2867.71	481.44
8	73	-80.00	-3277.35	329.53	29.77	5.393e+04	-8895.44	-573.97
8	73	-40.00	-2793.25	177.29	-912.84	3.249e+04	-4.534e+04	2397.46
8	74	-270.00	-1.157e+04	566.25	1571.96	-3.090e+04	-5.561e+04	-1400.39
8	74	-231.67	-1.179e+04	666.75	1364.11	-1.750e+04	665.93	638.83
8	74	-231.67	-1.179e+04	666.75	1364.11	-1.750e+04	665.93	638.83
8	74	-193.33	-1.154e+04	708.90	667.17	1.525e+04	7282.91	1665.44
8	74	-193.33	-1.154e+04	708.90	667.17	1.525e+04	7282.91	1665.44
8	74	-155.00	-1.143e+04	729.91	432.76	5.343e+04	3817.46	1362.64
8	74	-116.67	-1.144e+04	737.57	22.53	8.189e+04	-5522.22	425.59
8	74	-116.67	-1.144e+04	737.57	22.53	8.189e+04	-5522.22	425.59
8	74	-80.00	-1.086e+04	677.14	-838.61	8.001e+04	-3.228e+04	-1730.48
8	74	-40.00	-9117.93	407.19	-2379.83	4.364e+04	-1.164e+05	4623.34
8	76	-270.00	-1.156e+04	582.91	1570.23	-3.224e+04	-5.555e+04	-1433.73
8	76	-231.67	-1.179e+04	687.27	1363.37	-1.857e+04	680.42	658.42
8	76	-231.67	-1.179e+04	687.27	1363.37	-1.857e+04	680.42	658.42
8	76	-193.33	-1.154e+04	730.56	667.00	1.531e+04	7282.19	1706.52
8	76	-193.33	-1.154e+04	730.56	667.00	1.531e+04	7282.19	1706.52
8	76	-155.00	-1.143e+04	751.87	432.75	5.482e+04	3814.04	1397.65
8	76	-116.67	-1.144e+04	759.63	22.48	8.444e+04	-5526.15	447.44
8	76	-116.67	-1.144e+04	759.63	22.48	8.444e+04	-5526.15	447.44
8	76	-80.00	-1.086e+04	700.52	-838.85	8.267e+04	-3.229e+04	-1731.66
8	76	-40.00	-9119.92	431.90	-2380.26	4.458e+04	-1.164e+05	4677.56
M_S			N memb.	V memb.	V orto	M memb.	M orto	T
			-1.675e+04	-1139.63	-3388.89	-2.385e+05	-1.656e+05	-3459.34
			-2788.28	2166.68	2120.96	2.363e+05	9717.87	6979.95

Macro	Tipo	Angolo 1-Z (gradi)
9	Setto	0.0

M_S	Cmb	Z	N memb.	V memb.	V orto	M memb.	M orto	T
		cm	daN	daN	daN	daN cm	daN cm	daN cm
9	2	-270.00	-1.453e+04	252.59	-8210.69	1.158e+05	3.297e+05	1256.97
9	2	-231.67	-1.506e+04	170.90	-7682.96	8.190e+04	2.512e+04	3302.56
9	2	-231.67	-1.506e+04	170.90	-7682.96	8.190e+04	2.512e+04	3302.56
9	2	-193.33	-1.507e+04	251.35	-3575.39	3.652e+04	-8.518e+04	2222.68
9	2	-193.33	-1.507e+04	251.35	-3575.39	3.652e+04	-8.518e+04	2222.68
9	2	-155.00	-1.500e+04	504.36	-867.94	1.632e+04	-8.584e+04	1799.77
9	2	-116.67	-1.481e+04	586.82	1484.77	1.711e+04	-8982.79	1665.12
9	2	-116.67	-1.481e+04	586.82	1484.77	1.711e+04	-8982.79	1665.12
9	2	-78.33	-1.452e+04	332.94	4139.20	3.356e+04	1.455e+05	1843.04
9	2	-78.33	-1.452e+04	332.94	4139.20	3.356e+04	1.455e+05	1843.04
9	2	-40.00	-1.411e+04	170.27	6927.56	4.076e+04	3.909e+05	1521.90
9	3	-270.00	-5850.51	-135.12	-7597.85	5.527e+04	2.927e+05	917.52
9	3	-231.67	-6295.18	-271.90	-7394.86	4.776e+04	5368.26	2785.10
9	3	-231.67	-6295.18	-271.90	-7394.86	4.776e+04	5368.26	2785.10
9	3	-193.33	-6178.10	-107.35	-3603.01	3.003e+04	-9.977e+04	1702.23
9	3	-193.33	-6178.10	-107.35	-3603.01	3.003e+04	-9.977e+04	1702.23
9	3	-155.00	-5988.62	281.91	-1303.12	2.029e+04	-1.088e+05	1093.41
9	3	-116.67	-5718.13	583.39	444.44	1.019e+04	-5.948e+04	652.39
9	3	-116.67	-5718.13	583.39	444.44	1.019e+04	-5.948e+04	652.39
9	3	-78.33	-5361.34	624.24	2223.66	-2407.64	3.923e+04	498.54
9	3	-78.33	-5361.34	624.24	2223.66	-2407.64	3.923e+04	498.54
9	3	-40.00	-4871.85	484.38	4203.79	-2.093e+04	1.940e+05	704.64
9	4	-270.00	-1.446e+04	266.85	-8206.49	1.199e+05	3.294e+05	1307.67

SCARICATORE IN VIA PUCCI

9	4	-231.67	-1.499e+04	185.49	-7679.88	8.517e+04	2.496e+04	3394.98
9	4	-231.67	-1.499e+04	185.49	-7679.88	8.517e+04	2.496e+04	3394.98
9	4	-193.33	-1.502e+04	267.38	-3573.82	3.896e+04	-8.525e+04	2299.37
9	4	-193.33	-1.502e+04	267.38	-3573.82	3.896e+04	-8.525e+04	2299.37
9	4	-155.00	-1.496e+04	520.92	-867.30	1.799e+04	-8.587e+04	1876.16
9	4	-116.67	-1.479e+04	602.84	1484.75	1.812e+04	-8999.84	1742.54
9	4	-116.67	-1.479e+04	602.84	1484.75	1.812e+04	-8999.84	1742.54
9	4	-78.33	-1.451e+04	347.55	4138.56	3.398e+04	1.455e+05	1919.87
9	4	-78.33	-1.451e+04	347.55	4138.56	3.398e+04	1.455e+05	1919.87
9	4	-40.00	-1.410e+04	183.86	6926.17	4.063e+04	3.908e+05	1567.99
9	7	-270.00	-4709.30	-142.70	-5855.91	3.150e+04	2.260e+05	567.99
9	7	-231.67	-5025.60	-248.83	-5696.73	2.785e+04	4557.03	1891.20
9	7	-231.67	-5025.60	-248.83	-5696.73	2.785e+04	4557.03	1891.20
9	7	-193.33	-4896.21	-126.13	-2775.81	1.649e+04	-7.656e+04	1100.95
9	7	-193.33	-4896.21	-126.13	-2775.81	1.649e+04	-7.656e+04	1100.95
9	7	-155.00	-4709.49	171.85	-1004.14	1.107e+04	-8.365e+04	633.47
9	7	-116.67	-4462.59	405.23	341.93	5086.02	-4.571e+04	291.41
9	7	-116.67	-4462.59	405.23	341.93	5086.02	-4.571e+04	291.41
9	7	-78.33	-4154.64	440.48	1712.25	-3007.53	3.026e+04	174.65
9	7	-78.33	-4154.64	440.48	1712.25	-3007.53	3.026e+04	174.65
9	7	-40.00	-3756.72	335.66	3237.47	-1.576e+04	1.494e+05	416.75
9	18	-270.00	-1.141e+04	1591.88	-5951.86	1.152e+05	2.399e+05	2376.52
9	18	-231.67	-1.162e+04	1515.71	-5621.42	9.594e+04	9559.64	3267.74
9	18	-231.67	-1.162e+04	1515.71	-5621.42	9.594e+04	9559.64	3267.74
9	18	-193.33	-1.124e+04	1417.71	-2665.25	5.261e+04	-6.678e+04	2144.58
9	18	-193.33	-1.124e+04	1417.71	-2665.25	5.261e+04	-6.678e+04	2144.58
9	18	-155.00	-1.074e+04	1552.57	-729.91	5.163e+04	-6.703e+04	1355.42
9	18	-116.67	-1.023e+04	1475.07	868.81	4.197e+04	-1.403e+04	1702.90
9	18	-116.67	-1.023e+04	1475.07	868.81	4.197e+04	-1.403e+04	1702.90
9	18	-78.33	-9679.26	1317.81	2680.89	3.749e+04	9.087e+04	2100.74
9	18	-78.33	-9679.26	1317.81	2680.89	3.749e+04	9.087e+04	2100.74
9	18	-40.00	-8990.20	1082.15	4592.74	3.044e+04	2.535e+05	2315.20
9	19	-270.00	-7006.97	-1414.28	-6399.10	2.646e+04	2.505e+05	-702.70
9	19	-231.67	-7547.48	-1490.45	-6068.66	7503.98	2.008e+04	1387.00
9	19	-231.67	-7547.48	-1490.45	-6068.66	7503.98	2.008e+04	1387.00
9	19	-193.33	-7857.79	-1231.81	-2851.47	-4280.10	-7.101e+04	878.34
9	19	-193.33	-7857.79	-1231.81	-2851.47	-4280.10	-7.101e+04	878.34
9	19	-155.00	-8156.61	-914.18	-811.96	-2.793e+04	-7.583e+04	929.78
9	19	-116.67	-8318.54	-605.43	924.66	-2.091e+04	-2.358e+04	228.56
9	19	-116.67	-8318.54	-605.43	924.66	-2.091e+04	-2.358e+04	228.56
9	19	-78.33	-8357.10	-696.93	2784.63	-3668.27	8.291e+04	-50.93
9	19	-78.33	-8357.10	-696.93	2784.63	-3668.27	8.291e+04	-50.93
9	19	-40.00	-8360.39	-698.77	4782.73	3414.34	2.551e+05	-450.17
9	30	-270.00	-1.090e+04	2779.46	-6165.77	1.812e+05	2.462e+05	4699.73
9	30	-231.67	-1.106e+04	2703.29	-5835.33	1.679e+05	1.577e+04	5589.99
9	30	-231.67	-1.106e+04	2703.29	-5835.33	1.679e+05	1.577e+04	5589.99
9	30	-193.33	-1.098e+04	2725.57	-2768.71	9.510e+04	-6.716e+04	4726.26
9	30	-193.33	-1.098e+04	2725.57	-2768.71	9.510e+04	-6.716e+04	4726.26
9	30	-155.00	-1.057e+04	2790.62	-765.03	7.305e+04	-6.833e+04	3558.93
9	30	-116.67	-1.010e+04	2669.40	891.94	5.730e+04	-1.643e+04	3350.55
9	30	-116.67	-1.010e+04	2669.40	891.94	5.730e+04	-1.643e+04	3350.55
9	30	-78.33	-9628.85	2323.08	2731.39	4.450e+04	8.914e+04	4268.12
9	30	-78.33	-9628.85	2323.08	2731.39	4.450e+04	8.914e+04	4268.12
9	30	-40.00	-9038.47	1944.32	4757.56	2.695e+04	2.551e+05	4448.77
9	34	-270.00	-1.086e+04	2214.67	-6155.06	1.801e+05	2.457e+05	5081.34
9	34	-231.67	-1.102e+04	2138.50	-5824.61	1.653e+05	1.531e+04	6095.46
9	34	-231.67	-1.102e+04	2138.50	-5824.61	1.653e+05	1.531e+04	6095.46
9	34	-193.33	-1.096e+04	2219.14	-2735.76	9.480e+04	-6.716e+04	5283.02
9	34	-193.33	-1.096e+04	2219.14	-2735.76	9.480e+04	-6.716e+04	5283.02
9	34	-155.00	-1.055e+04	2370.09	-762.77	6.869e+04	-6.818e+04	4176.33
9	34	-116.67	-1.008e+04	2337.08	890.68	5.301e+04	-1.627e+04	3846.44
9	34	-116.67	-1.008e+04	2337.08	890.68	5.301e+04	-1.627e+04	3846.44
9	34	-78.33	-9619.76	2032.83	2744.54	4.229e+04	8.922e+04	4675.52
9	34	-78.33	-9619.76	2032.83	2744.54	4.229e+04	8.922e+04	4675.52
9	34	-40.00	-8986.15	1635.87	4755.00	2.318e+04	2.557e+05	4696.84
9	50	-270.00	-1.047e+04	943.44	-6035.90	9.270e+04	2.419e+05	1653.75
9	50	-231.67	-1.075e+04	867.27	-5705.46	7.367e+04	1.153e+04	2769.03
9	50	-231.67	-1.075e+04	867.27	-5705.46	7.367e+04	1.153e+04	2769.03
9	50	-193.33	-1.051e+04	829.65	-2700.26	3.801e+04	-6.767e+04	1762.90
9	50	-193.33	-1.051e+04	829.65	-2700.26	3.801e+04	-6.767e+04	1762.90
9	50	-155.00	-1.019e+04	1000.06	-745.95	3.383e+04	-6.876e+04	1171.29
9	50	-116.67	-9816.68	1003.87	879.29	2.810e+04	-1.593e+04	1376.97
9	50	-116.67	-9816.68	1003.87	879.29	2.810e+04	-1.593e+04	1376.97
9	50	-78.33	-9397.26	867.35	2699.41	2.849e+04	8.922e+04	1557.72
9	50	-78.33	-9397.26	867.35	2699.41	2.849e+04	8.922e+04	1557.72
9	50	-40.00	-8857.20	690.55	4627.40	2.481e+04	2.537e+05	1649.49
9	51	-270.00	-7949.02	-765.85	-6315.07	4.896e+04	2.485e+05	20.06
9	51	-231.67	-8418.07	-842.01	-5984.62	2.978e+04	1.810e+04	1885.71
9	51	-231.67	-8418.07	-842.01	-5984.62	2.978e+04	1.810e+04	1885.71

SCARICATORE IN VIA PUCCI

9	51	-193.33	-8581.31	-643.75	-2816.46	1.032e+04	-7.013e+04	1260.02
9	51	-193.33	-8581.31	-643.75	-2816.46	1.032e+04	-7.013e+04	1260.02
9	51	-155.00	-8713.68	-361.67	-795.92	-1.013e+04	-7.410e+04	1113.91
9	51	-116.67	-8729.06	-134.23	914.18	-7037.62	-2.169e+04	554.49
9	51	-116.67	-8729.06	-134.23	914.18	-7037.62	-2.169e+04	554.49
9	51	-78.33	-8639.10	-246.47	2766.10	5331.02	8.456e+04	492.09
9	51	-78.33	-8639.10	-246.47	2766.10	5331.02	8.456e+04	492.09
9	51	-40.00	-8493.38	-307.17	4748.07	9041.27	2.548e+05	215.55
9	62	-270.00	-1.014e+04	1656.35	-6171.36	1.330e+05	2.458e+05	3058.39
9	62	-231.67	-1.039e+04	1580.18	-5840.92	1.175e+05	1.544e+04	4204.03
9	62	-231.67	-1.039e+04	1580.18	-5840.92	1.175e+05	1.544e+04	4204.03
9	62	-193.33	-1.034e+04	1620.31	-2765.37	6.397e+04	-6.792e+04	3376.63
9	62	-193.33	-1.034e+04	1620.31	-2765.37	6.397e+04	-6.792e+04	3376.63
9	62	-155.00	-1.007e+04	1750.07	-767.93	4.671e+04	-6.961e+04	2548.37
9	62	-116.67	-9733.20	1726.23	893.21	3.729e+04	-1.744e+04	2363.17
9	62	-116.67	-9733.20	1726.23	893.21	3.729e+04	-1.744e+04	2363.17
9	62	-78.33	-9359.79	1473.36	2731.02	3.266e+04	8.814e+04	2902.22
9	62	-78.33	-9359.79	1473.36	2731.02	3.266e+04	8.814e+04	2902.22
9	62	-40.00	-8881.72	1205.41	4729.54	2.269e+04	2.547e+05	2967.89
9	66	-270.00	-1.012e+04	1338.06	-6164.03	1.327e+05	2.455e+05	3301.15
9	66	-231.67	-1.037e+04	1261.89	-5833.59	1.164e+05	1.516e+04	4512.19
9	66	-231.67	-1.037e+04	1261.89	-5833.59	1.164e+05	1.516e+04	4512.19
9	66	-193.33	-1.033e+04	1335.87	-2745.03	6.398e+04	-6.792e+04	3708.84
9	66	-193.33	-1.033e+04	1335.87	-2745.03	6.398e+04	-6.792e+04	3708.84
9	66	-155.00	-1.006e+04	1515.76	-766.44	4.417e+04	-6.952e+04	2915.74
9	66	-116.67	-9720.48	1543.18	892.50	3.479e+04	-1.733e+04	2663.55
9	66	-116.67	-9720.48	1543.18	892.50	3.479e+04	-1.733e+04	2663.55
9	66	-78.33	-9355.82	1313.99	2739.21	3.144e+04	8.820e+04	3150.77
9	66	-78.33	-9355.82	1313.99	2739.21	3.144e+04	8.820e+04	3150.77
9	66	-40.00	-8851.44	1033.82	4727.63	2.054e+04	2.551e+05	3124.97
9	74	-270.00	-1.040e+04	134.79	-6258.87	7.728e+04	2.503e+05	861.89
9	74	-231.67	-1.078e+04	65.83	-5884.68	5.497e+04	1.751e+04	2359.40
9	74	-231.67	-1.078e+04	65.83	-5884.68	5.497e+04	1.751e+04	2359.40
9	74	-193.33	-1.075e+04	134.37	-2755.30	2.406e+04	-6.692e+04	1550.18
9	74	-193.33	-1.075e+04	134.37	-2755.30	2.406e+04	-6.692e+04	1550.18
9	74	-155.00	-1.067e+04	342.23	-713.17	1.065e+04	-6.835e+04	1206.23
9	74	-116.67	-1.050e+04	428.87	1035.45	1.105e+04	-1.207e+04	1069.79
9	74	-116.67	-1.050e+04	428.87	1035.45	1.105e+04	-1.207e+04	1069.79
9	74	-78.33	-1.024e+04	265.76	2988.42	2.153e+04	1.011e+05	1173.44
9	74	-78.33	-1.024e+04	265.76	2988.42	2.153e+04	1.011e+05	1173.44
9	74	-40.00	-9907.74	144.37	5051.46	2.520e+04	2.806e+05	1023.05
9	75	-270.00	-4606.81	-123.68	-5850.31	3.690e+04	2.256e+05	635.59
9	75	-231.67	-4935.75	-229.37	-5692.62	3.221e+04	4347.26	2014.42
9	75	-231.67	-4935.75	-229.37	-5692.62	3.221e+04	4347.26	2014.42
9	75	-193.33	-4825.65	-104.76	-2773.72	1.973e+04	-7.665e+04	1203.21
9	75	-193.33	-4825.65	-104.76	-2773.72	1.973e+04	-7.665e+04	1203.21
9	75	-155.00	-4659.03	193.93	-1003.28	1.330e+04	-8.369e+04	735.32
9	75	-116.67	-4431.18	426.59	341.90	6434.68	-4.573e+04	394.64
9	75	-116.67	-4431.18	426.59	341.90	6434.68	-4.573e+04	394.64
9	75	-78.33	-4139.66	459.96	1711.39	-2440.68	3.022e+04	277.10
9	75	-78.33	-4139.66	459.96	1711.39	-2440.68	3.022e+04	277.10
9	75	-40.00	-3752.24	353.78	3235.61	-1.593e+04	1.493e+05	478.21
9	76	-270.00	-1.035e+04	144.29	-6256.07	7.998e+04	2.501e+05	895.69
9	76	-231.67	-1.073e+04	75.56	-5882.63	5.715e+04	1.741e+04	2421.01
9	76	-231.67	-1.073e+04	75.56	-5882.63	5.715e+04	1.741e+04	2421.01
9	76	-193.33	-1.072e+04	145.05	-2754.26	2.568e+04	-6.697e+04	1601.31
9	76	-193.33	-1.072e+04	145.05	-2754.26	2.568e+04	-6.697e+04	1601.31
9	76	-155.00	-1.064e+04	353.27	-712.74	1.176e+04	-6.837e+04	1257.15
9	76	-116.67	-1.048e+04	439.55	1035.44	1.173e+04	-1.208e+04	1121.41
9	76	-116.67	-1.048e+04	439.55	1035.44	1.173e+04	-1.208e+04	1121.41
9	76	-78.33	-1.024e+04	275.50	2987.99	2.182e+04	1.011e+05	1224.66
9	76	-78.33	-1.024e+04	275.50	2987.99	2.182e+04	1.011e+05	1224.66
9	76	-40.00	-9905.50	153.43	5050.53	2.512e+04	2.805e+05	1053.78

M_S

N memb.

V memb.

V orto

M memb.

M orto

T

-1.507e+04
-3752.24-1490.45
2790.62-8210.69
6927.56-2.793e+04
1.812e+05-1.088e+05
3.909e+05-702.70
6095.46

Macro	Tipo	Angolo 1-X (gradi)
1	Guscio	0.0

M_G	Cmb	Nodo	N max daN/cm	N min daN/cm	N 1 daN/cm	N 2 daN/cm	N 1-2 daN/cm	M max daN	M min daN	M 1 daN	M 2 daN	M 1-2 daN
1	4	1	4.87	-20.42	-1.37	-14.18	-10.90	-186.59	-297.60	-188.00	-296.19	-12.40

SCARICATORE IN VIA PUCCI

1	69	28	22.86	-7.65	2.25	12.96	14.29	-66.42	-82.41	-71.27	-77.55	7.35
1	69	29	-10.70	-13.60	-11.28	-13.03	1.16	102.42	-112.92	87.74	-98.23	54.28
1	69	30	-21.66	-33.17	-33.14	-21.70	-0.63	368.42	-243.62	368.34	-243.54	7.02
1	69	31	-21.63	-32.91	-30.75	-23.78	4.44	373.27	-230.20	371.25	-228.18	-34.87
1	69	32	-14.14	-21.67	-21.03	-14.78	2.11	211.29	-148.77	207.07	-144.55	-38.74
1	69	33	15.60	-10.30	1.57	3.73	-12.90	-37.16	-100.30	-85.14	-52.32	-26.97
1	76	1	4.10	-17.23	-0.99	-12.14	-9.09	-133.63	-215.77	-134.10	-215.29	-6.23
1	76	2	12.08	-2.37	-2.31	12.03	-0.89	75.55	-171.10	73.07	-168.63	-24.57
1	76	3	9.89	-7.30	-7.18	9.78	-1.40	321.93	-206.49	321.50	-206.06	-15.00
1	76	4	3.26	-16.70	-14.49	1.05	6.26	469.30	-288.37	469.01	-288.09	-14.66
1	76	5	7.95	-20.78	-11.38	-1.44	13.48	349.64	-269.53	349.61	-269.49	4.70
1	76	6	12.99	-12.81	0.13	4.45e-02	12.90	143.41	-244.58	141.48	-242.65	27.29
1	76	7	3.06	-17.15	-3.92	-10.17	9.61	-114.39	-216.65	-129.11	-201.94	-35.89
1	76	8	14.33	-13.25	-13.24	14.32	0.52	-105.97	-154.87	-141.78	-119.06	-21.65
1	76	9	11.33	-12.68	-9.81	8.46	-7.79	290.19	-78.94	184.79	26.46	-166.72
1	76	10	6.65	-10.34	-10.33	6.64	-0.36	503.65	51.53	421.43	133.75	-174.40
1	76	11	1.84	-15.97	-11.94	-2.19	7.45	567.93	168.73	564.02	172.65	-39.34
1	76	12	2.84	-17.04	-11.45	-2.76	8.94	465.41	128.08	463.61	129.88	24.63
1	76	13	3.64	-16.96	-10.56	-2.76	9.54	417.69	120.00	408.21	129.48	52.28
1	76	14	5.75	-17.52	-11.37	-0.40	10.26	285.53	40.83	240.34	86.02	94.95
1	76	15	13.19	-15.90	-8.52	5.82	12.65	-82.54	-315.43	-273.67	-124.30	89.34
1	76	16	-1.24	-32.77	-23.55	-10.45	-14.34	258.85	-302.03	-302.02	258.84	2.40
1	76	17	1.48	-25.12	-22.55	-1.09	-7.87	377.50	215.76	227.71	365.56	-42.31
1	76	18	-2.29	-18.85	-18.32	-2.83	-2.92	686.10	525.49	640.63	570.96	-72.35
1	76	19	-3.37	-18.82	-15.02	-7.17	6.65	825.45	667.50	777.48	715.47	-72.63
1	76	20	-0.85	-24.12	-18.90	-6.07	9.71	526.71	451.54	478.52	499.73	-36.06
1	76	21	-3.40	-36.22	-26.27	-13.35	15.09	296.91	-326.09	-325.11	295.93	-24.63
1	76	22	1.83	-22.77	-15.90	-5.04	-11.03	165.33	-184.99	-184.75	165.08	9.28
1	76	23	0.41	-22.41	-15.84	-6.17	-10.34	308.73	123.44	178.54	253.63	84.69
1	76	24	-11.50	-22.09	-18.24	-15.36	-5.10	563.11	366.64	548.95	380.79	50.80
1	76	25	-13.03	-21.43	-18.81	-15.66	3.89	648.70	299.56	569.97	378.29	-145.91
1	76	26	-2.93	-27.26	-16.43	-13.76	12.09	529.38	153.08	371.59	310.87	-185.68
1	76	27	2.61	-22.60	-16.78	-3.22	10.62	122.79	-230.06	-225.84	118.58	-38.33
1	76	28	22.14	-6.53	3.02	12.59	13.51	-77.91	-93.24	-79.91	-91.24	-5.17
1	76	29	-11.66	-13.50	-11.95	-13.21	0.67	94.86	-121.30	87.45	-113.89	39.33
1	76	30	-21.14	-35.34	-35.12	-21.35	-1.72	358.93	-281.14	358.93	-281.14	3.70e-02
1	76	31	-22.54	-33.38	-32.53	-23.39	2.91	338.91	-286.63	337.13	-284.84	-33.37
1	76	32	-14.15	-22.62	-22.57	-14.20	0.66	184.63	-193.48	181.57	-190.42	-33.85
1	76	33	17.60	-10.46	2.04	5.11	-13.94	-79.04	-133.15	-124.18	-88.02	-20.12

M_G	N max	N min	N 1	N 2	N 1-2	M max	M min	M 1	M 2	M 1-2
	29.12	-49.57	-49.44	-30.57	-20.57	1176.18	-430.42	-429.08	-376.92	-262.86
			4.17	20.94	21.47			1106.48	1021.18	134.73

Macro	Tipo	Angolo 1-X (gradi)
6	Guscio	0.0

M_G	Cmb	Nodo	N max daN/cm	N min daN/cm	N 1 daN/cm	N 2 daN/cm	N 1-2 daN/cm	M max daN	M min daN	M 1 daN	M 2 daN	M 1-2 daN
6	2	34	9.72	-27.39	-14.99	-2.68	-17.50	-362.35	-627.08	-465.69	-523.75	-129.15
6	2	35	-22.82	-49.53	-45.92	-26.43	-9.13	571.32	-803.01	473.36	-705.06	-353.59
6	2	36	-38.34	-54.30	-54.14	-38.50	-1.60	820.14	-1104.53	803.67	-1088.06	-177.29
6	2	37	-39.16	-52.99	-51.11	-41.04	4.74	616.38	-1265.73	610.23	-1259.57	-107.48
6	2	38	-34.46	-51.27	-44.55	-41.19	8.24	437.02	-1326.45	435.97	-1325.40	-43.05
6	2	39	-30.53	-49.53	-39.21	-40.85	9.47	322.98	-1340.37	322.64	-1340.02	23.88
6	2	40	-28.89	-48.60	-36.73	-40.75	9.65	263.77	-1339.73	258.42	-1334.38	92.46
6	2	41	-31.19	-48.42	-37.56	-42.05	8.31	268.20	-1344.25	251.18	-1327.23	164.78
6	2	42	-31.93	-49.62	-40.26	-41.28	8.83	314.14	-1340.86	285.70	-1312.42	215.07
6	2	43	-33.66	-51.62	-41.36	-43.92	8.89	300.57	-1325.82	269.27	-1294.52	223.45
6	2	44	-34.00	-49.38	-41.10	-42.29	7.67	319.91	-1249.94	263.28	-1193.31	292.74
6	2	45	-30.80	-49.68	-40.44	-40.05	9.44	330.84	-1154.51	254.25	-1077.92	328.47
6	2	46	-30.38	-47.81	-38.78	-39.40	8.71	294.08	-1079.15	210.32	-995.39	328.64
6	2	47	-23.16	-40.65	-30.98	-32.84	8.70	172.63	-921.77	41.37	-790.51	355.56
6	2	48	-16.80	-33.30	-23.38	-26.71	8.08	-11.24	-860.69	-272.08	-599.86	391.83
6	2	49	11.00	-32.99	-9.86	-12.13	21.96	-415.69	-601.21	-565.55	-451.35	73.11
6	2	50	26.59	-29.90	-28.29	24.98	9.40	23.54	-1109.25	-394.16	-691.54	-546.53
6	2	51	-18.35	-29.54	-18.49	-29.40	1.22	1905.06	-258.39	1299.48	347.20	-971.30
6	2	52	-28.56	-40.82	-28.68	-40.71	1.19	1889.88	628.29	1337.34	1180.84	-625.92
6	2	53	-32.75	-44.29	-33.19	-43.85	2.20	1793.01	917.07	1231.38	1478.70	-420.15
6	2	54	-32.75	-44.92	-34.48	-43.19	4.25	1635.91	1045.66	1098.63	1582.95	-168.69
6	2	55	-30.98	-45.32	-34.43	-41.87	6.13	1613.83	969.78	992.94	1590.66	119.93
6	2	56	-29.75	-45.39	-34.37	-40.77	7.13	1748.52	699.11	917.45	1530.17	425.98
6	2	57	-27.86	-47.48	-34.30	-41.05	9.21	1938.68	357.83	888.23	1408.27	746.43
6	2	58	-29.21	-47.82	-33.92	-43.11	8.09	2076.84	132.80	905.28	1304.37	951.32

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

13	46	727	0.93	-4.39	-1.44	-2.02	2.65	21.48	5.05	20.83	5.70	-3.20
13	46	731	-0.21	-2.94	-2.22	-0.93	-1.21	3.92	-7.33	-1.85	-1.57	-5.62
13	46	732	-0.69	-2.17	-1.14	-1.72	0.68	44.46	13.25	13.72	43.98	-3.83
13	46	733	0.28	-6.74	-2.71	-3.74	3.47	9.43	-3.22	2.30	3.91	6.27
13	60	718	3.03	-3.79	-2.79	2.04	2.41	4.80	-7.10	-1.84	-0.45	5.91
13	60	719	0.98	-4.94	-3.16	-0.80	2.72	44.90	9.91	10.08	44.73	2.45
13	60	720	-0.12	-6.12	-3.87	-2.37	2.91	15.21	3.37	7.27	11.31	-5.56
13	60	721	-9.11e-02	-4.48	-2.83	-1.74	2.13	0.69	5.05e-02	0.21	0.53	0.28
13	60	725	1.47	-5.19	-5.08	1.36	0.85	81.27	24.98	81.27	24.98	-1.50e-02
13	60	726	0.37	-4.24	-3.26	-0.61	1.89	-60.45	-68.43	-67.81	-61.07	2.14
13	60	727	6.04e-02	-4.61	-2.27	-2.27	2.33	21.47	5.05	20.82	5.70	-3.20
13	60	731	-0.20	-3.27	-2.28	-1.18	-1.44	3.92	-7.33	-1.85	-1.57	-5.62
13	60	732	-1.01	-2.30	-1.17	-2.14	0.43	44.46	13.24	13.72	43.98	-3.83
13	60	733	9.13e-02	-6.37	-2.60	-3.68	3.19	9.43	-3.22	2.30	3.91	6.27
13	74	718	6.05	-1.38	-0.71	5.38	2.13	5.75	-8.47	-2.20	-0.52	7.06
13	74	719	2.81	-3.09	-1.63	1.35	2.54	53.64	11.85	12.06	53.43	2.92
13	74	720	1.41	-4.66	-2.50	-0.74	2.90	18.17	4.04	8.69	13.52	-6.64
13	74	721	1.97	-2.91	-0.91	-3.30e-02	2.40	0.83	6.29e-02	0.25	0.64	0.33
13	74	725	2.57	-5.43	-5.43	2.56	-0.17	97.02	29.83	97.02	29.83	-9.69e-03
13	74	726	1.37	-3.66	-3.12	0.83	1.57	-72.17	-81.71	-80.96	-72.92	2.56
13	74	727	0.99	-3.82	-1.25	-1.58	2.40	25.64	6.03	24.86	6.81	-3.83
13	74	731	0.64	-4.96	-2.93	-1.39	-2.69	4.67	-8.77	-2.21	-1.88	-6.72
13	74	732	-0.94	-1.77	-1.31	-1.40	-0.41	53.05	15.79	16.36	52.48	-4.57
13	74	733	0.21	-6.06	-2.70	-3.15	3.12	11.25	-3.86	2.74	4.65	7.50
13	76	718	5.99	-1.46	-0.75	5.28	2.18	5.75	-8.47	-2.20	-0.53	7.06
13	76	719	2.79	-3.15	-1.64	1.29	2.59	53.64	11.85	12.05	53.43	2.92
13	76	720	1.38	-4.70	-2.50	-0.82	2.92	18.16	4.04	8.69	13.52	-6.64
13	76	721	1.91	-2.93	-0.92	-0.10	2.38	0.83	6.28e-02	0.25	0.64	0.33
13	76	725	2.53	-5.43	-5.43	2.52	-0.11	97.02	29.83	97.02	29.83	-9.99e-03
13	76	726	1.35	-3.69	-3.12	0.78	1.60	-72.17	-81.71	-80.96	-72.92	2.56
13	76	727	0.97	-3.85	-1.26	-1.62	2.40	25.64	6.03	24.86	6.81	-3.83
13	76	731	0.61	-4.90	-2.91	-1.38	-2.65	4.67	-8.77	-2.21	-1.88	-6.72
13	76	732	-0.99	-1.74	-1.30	-1.42	-0.37	53.05	15.79	16.36	52.48	-4.57
13	76	733	0.20	-6.08	-2.70	-3.17	3.13	11.26	-3.86	2.74	4.66	7.49
M_G			N max	N min	N 1	N 2	N 1-2	M max	M min	M 1	M 2	M 1-2
				-8.51	-7.70	-4.13	-4.31		-119.50	-118.41	-106.64	-9.82
			10.40		-0.13	9.89	4.51	141.88		141.88	78.15	10.97

VERIFICHE ELEMENTI PARETE E/O GUSCIO IN C.A.

LEGENDA TABELLA VERIFICHE ELEMENTI PARETE E GUSCIO IN C.A.

Per le pareti in c.a., in ottemperanza al cap. 7 del DM 17-01-18, viene effettuata una doppia progettazione: sia come *Singolo Elemento* sia come *Parete Sismica* o *Parete Debolmente Armata*.

Per la progettazione come *Singolo Elemento* di ogni elemento vengono riportati il codice dello stato di verifica con le sigle **Ok** e **NV**, il rapporto x/d , la verifica per sollecitazioni ultime (verifica a compressione media gli sforzi membranali, verifica a presso-flessionale e verifica a sollecitazioni taglianti), gli sforzi membranali e flessionali, il quantitativo di armatura nella direzione principale e secondaria sia inferiore che superiore e il quantitativo di armatura a taglio.

Per la progettazione come *Parete Sismica* o *Parete Debolmente Armata* vengono riportate invece le caratteristiche geometriche della parete e delle zone dissipative (quest'ultime solo nel caso di parete sismica), i coefficienti di verifica a compressione assiale, pressoflessione e sollecitazioni taglianti.

Inoltre vengono riportate per ogni quota significativa l'armatura principale e secondaria, l'armatura in zona confinata (solo per parete sismica) e non confinata, l'armatura concentrata all'estremità (per pareti debolmente armate), lo sforzo assiale aggiuntivo per q superiore a 2 e i valori di involuppo di taglio e momento. Per le pareti debolmente armate viene riportato anche lo stato di verifica relativo alla snellezza. Le azioni derivate dall'analisi, in ogni combinazione di calcolo, sono elaborate come previsto al punto 7.4.4.5.1: traslazione del momento, incremento e variazione diagramma taglio, incremento e decremento sforzo assiale. La progettazione nel caso dei gusci viene effettuata una progettazione come *Singolo Elemento*, riportando in tabella il rapporto x/d , la verifica per sollecitazioni ultime, (verifica a compressione media gli sforzi membranali, verifica a presso-flessionale e verifica a sollecitazioni taglianti) di ogni elemento.

Per ogni elemento, viene riportata inoltre la maglia di armatura necessaria in relazione alle risultanze della progettazione dei nodi dell'elemento stesso. Le quantità di armature necessarie sono armature (disposte rispettivamente in direzione principale e secondaria, inferiore e superiore) distribuite nell'elemento ed espresse in centimetri quadri per sviluppo lineare pari ad un metro.

Nel caso dei gusci viene effettuata, inoltre, la verifica a punzonamento, riportando in tabella il codice dello stato di verifica, il coefficiente di verifica per piastre prive di armature a taglio lungo il perimetro resistente e lungo il perimetro del pilastro, coefficiente di incremento dovuto ai momenti flettenti, fattore di amplificazione per le fondazioni, il fattore di amplificazione dell'altezza utile per individuare il perimetro di verifica lungo il quale l'armatura a taglio non è richiesta, il quantitativo di armatura a punzonamento, il numero di serie di armature, il numero di braccia di armatura ed il riferimento alla combinazione più gravosa.

Simbologia adottata nelle tabelle di verifica

Per gli elementi con progettazione "*Singolo Elemento* ..." è presente una tabella con i simboli di seguito descritti:

Macro Guscio	Numero del macroelemento di tipo guscio (elementi non verticali contigui ed analoghi per proprietà)
Macro Setto	Numero del macroelemento di tipo setto (elementi verticali contigui ed analoghi per proprietà)
Spessore	Spessore della parete
Id Materiale	Codice del materiale assegnato all'elemento
Id Criterio	Codice del criterio di progetto assegnato all'elemento
Progettazione	Sigla tipo di Elemento: - Singolo Elemento; - Singolo Elemento FONDAZIONE; - Singolo Elemento NON DISSIPATIVO

Per gli elementi con progettazione “*Parete Sismica o Parete Debolmente Armata*” è presente una tabella con i simboli di seguito descritti:

Parete	Numero della PARETE SISMICA
Parete PDA	Numero della PARETE DEBOLMENTE ARMATA
H totale	Altezza complessiva della parete
Spessore	Spessore della parete
H critica	Altezza come da punto 7.4.4.5.1 per traslazione momento (solo in Parete Sismica)
H critica V	Altezza della zona dissipativa (solo in Parete Sismica)
L totale	Larghezza di base della parete
L confinata	Lunghezza della zona dissipativa (solo in Parete Sismica)
Verif. N	Verifica di cui al punto 7.4.4.5.1 compressione semplice
Verif. N-M	Verifica di cui al punto 7.4.4.5.1 pressoflessione
Fattore V	Fattore di amplificazione del taglio di cui al punto 7.4.4.5.1
Diagramma V	Diagramma elaborato per effetto modi superiori come da fig. 7.4.4
Verif. V	Verifica di cui al punto 7.4.4.5.1 taglio (compressione cls, trazione acciaio, scorrimento in zona critica) (solo in Parete Sismica)
Verifica Snellezza	Verifica di cui al punto 7.4.4.5.1 limitazione compressione per prevenire l'instabilità (solo in Parete Debolmente Armata)
Prog. composta	Sigla per la progettazione composta

Per le verifiche degli elementi con progettazione “*Singolo Elemento ...*” e *Progettazione Composta* è presente una tabella con i simboli di seguito descritti:

Nodo	numero del nodo
Stato	codice di verifica dell'elemento ok o NV
x/d	rapporto tra posizione dell'asse neutro e altezza utile alla rottura della sezione (per sola flessione)
V N/M	Verifica delle sollecitazioni Normali (momento e sforzo normale)
Ver. rid	Rapporto Nd/Nu (Nu ottenuto con riduzione del 25% di fcd)

Af pr+	quantità di armatura richiesta in direzione principale relativa alla faccia positiva (estradosso piastre) (valore derivante da calcolo o minimo normativo)
Af pr-	quantità di armatura richiesta in direzione principale relativa alla faccia negativa (intradosso piastre) (valore derivante da calcolo o minimo normativo)
Af sec+	quantità di armatura richiesta in direzione secondaria relativa alla faccia positiva (estradosso piastre) (valore derivante da calcolo o minimo normativo)
Af sec-	quantità di armatura richiesta in direzione secondaria relativa alla faccia negativa (intradosso piastre) (valore derivante da calcolo o minimo normativo)
Nz No Nzo	Sforzi membranali per pareti e/o setti verticali
Mz Mo Mzo	Sforzi flessionali per pareti e/o setti verticali
Nx Ny Nxy	Sforzi membranali per gusci orizzontali
Mx Mx Mxy	Sforzi flessionali per gusci orizzontali

Nodo	numero del nodo
Stato	codice di verifica dell'elemento ok o NV
Max tau	Tensione tangenziale Massima
Ver V pr	Verifica a taglio nella direzione principale lato calcestruzzo
Ver V sec	Verifica a taglio nella direzione secondaria lato calcestruzzo
Af V pr	Armatura nella direzione principale
V pr-	Verifica dell'armatura nella direzione principale
Af V sec	Armatura nella direzione secondaria
V sec-	Verifica dell'armatura nella direzione secondaria

Per le verifiche degli elementi con progettazione “*Parete Sismica o Parete Debolmente Armata*”, oltre alla tabella con le verifiche per gli elementi con progettazione “*Singolo Elemento ...*”, è presente una tabella con i simboli di seguito descritti:

Quota	Ascissa verticale di riferimento
Af conf.	Numero e diametro armatura presente in una zona confinata
Af std	Diametro e passo armatura in zona non confinata (doppia maglia)
Af estremi	Diametro dei ferri di estremità del pannello; se posto uguale 0, viene utilizzato il diametro standard
Af V (ori)	Diametro e passo armatura orizzontale (doppia maglia)
Ver. N	Rapporto tra azione di calcolo e resistenza a compressione (normalizzato a 1 in quanto da confrontare con 40% in CDB e 35 % in CDA)
Ver. N/M	Rapporto tra azione di calcolo e resistenza a pressoflessione
Ver. V acc(7)	Rapporto tra azione di calcolo e resistenza a taglio-trazione per α_S minore di 2 secondo paragrafo 7.4.4.5.1
Ver. V cls	Rapporto tra azione di calcolo e resistenza a taglio-compressione

Ver. V acc	Rapporto tra azione di calcolo e resistenza a taglio-trazione
Ver. V scorr.	Rapporto tra azione di calcolo e resistenza a taglio scorrimento
N add	Sforzo assiale di cui al punto 7.4.4.5.1 da sommare e sottrarre nelle verifiche quando q supera 2
N invil M invil	Inviluppo del Momento e Sforzo Normale come al punto 7.4.4.5.1 (informativo) (solo in Parete Sismica)

Quota	Ascissa verticale di riferimento
N v.N	Valore dello sforzo assiale per cui Ver. N attinge il massimo valore
N v.M/N, M v.M/N	Valore dello sforzo assiale e momento per cui Ver. N/M attinge il massimo valore
N v.M/N, M v.M/N Mo v.M/N	Valore dello sforzo assiale e dei momenti per cui Ver. N/M attinge il massimo valore (per le pareti estese debolmente armate)
N v.Vcls, V v.Vcls,	Valore dello sforzo assiale e taglio per cui Ver. V. cls attinge il massimo valore
N v.Vacc, M v.Vacc, V v.Vacc,	Valore dello sforzo assiale, momento e taglio per cui Ver. V. acc attinge il massimo valore
N v.Vscorr, M v.Vscorr, V v.Vscorr,	Valore dello sforzo assiale, momento e taglio per cui Ver. V. scorr.e attinge il massimo valore
N v.N	Valore dello sforzo assiale per cui Ver. N attinge il massimo valore
N v.M/N, M v.M/N	Valore dello sforzo assiale e momento per cui Ver. N/M attinge il massimo valore
N v.M/N, M v.M/N Mo v.M/N	Valore dello sforzo assiale e dei momenti per cui Ver. N/M attinge il massimo valore (per le pareti estese debolmente armate)
N v.Vcls, V v.Vcls,	Valore dello sforzo assiale e taglio per cui Ver. V. cls attinge il massimo valore

Quota	Ascissa verticale di riferimento
CtgT Vcls	Valore di ctg(teta) adottato nella verifica V compressione cls
Vrsd Vcls	Valore della resistenza a taglio trazione (armatura di calcolo)
Vrcd Vcls	Valore della resistenza a taglio compressione
CtgT Vacc	Valore di ctg(teta) adottato nella verifica V trazione armatura
Vrsd Vacc	Valore della resistenza a taglio trazione (armatura presente)
Vrcd Vacc	Valore della resistenza a taglio compressione
Vdd	Valore del contributo alla resistenza allo scorrimento come da [7.4.20]
Vid	Valore del contributo alla resistenza allo scorrimento come da [7.4.21]
A s.i.	Somma delle aree di armature
Incli.	Angolo di inclinazione delle armature

Dist.	Distanza alla base tra le armature inclinate
Quota	Ascissa verticale di riferimento
V[7.4.16]	Verifica a taglio-trazione dell'armatura dell'anima (7.4.16)
N M V	Sollecitazioni di calcolo della condizione più gravosa
Alfas	Rapporto di Taglio
Vrd,c	Resistenza a taglio degli elementi non armati
VRd,s	Resistenza a taglio nei confronti dello scorrimento
V[7.4.17]	Verifica a taglio-trazione dell'armatura dell'anima (7.4.17)
roH	Rapporto tra l'armatura orizzontale e l'area della sezione relativa di calcestruzzo
roV	Rapporto tra l'armatura verticale e l'area della sezione relativa di calcestruzzo
roN	Sforzo normale adimensionalizzato $Ned/(bw f_{yd})$

Per la verifica a *Punzonamento* è presente una tabella con i simboli di seguito descritti:

Nodo	numero del nodo
Stato	codice di verifica dell'elemento ok o NV
V. 6.47	Fattore di sicurezza per la verifica per piastre prive di armature a taglio lungo il perimetro resistente U1
V. 6.53	Fattore di sicurezza per la verifica per piastre prive di armature a taglio lungo il perimetro del pilastro U0
Beta	Fattore di incremento dovuto ai momenti flettenti
f. a fon	fattore di amplificazione per le fondazioni (solo per gusci di fondazione)
f. Uout	fattore di amplificazione dell'altezza utile per individuare il perimetro di verifica lungo il quale l'armatura a taglio non è richiesta
Aw tot	Quantitativo di armatura per la verifica di piastre munite di armatura (formula 6.52 dell'EC2)
Asw,min	Quantitativo minimo di armatura previsto dai dettagli costruttivi (formula 9.11 dell'EC2)
n. x serie	Numero di serie di armature
n.ser 0(R)	Numero di braccia delle armature in direzione 0 (o numero di braccia radiale)
n.ser 90	Numero di braccia delle armature in direzione 90 (solo se armatura cruciforme)
Rif. cmb	Riferimento combinazioni da cui si generano le verifiche più gravose

PROGETTAZIONE DELLE FONDAZIONI

Il D.M.17/01/2018 - par: 7.2.5 prevede:

“Sia per CD“A” sia per CD“B” il dimensionamento delle strutture di fondazione e la verifica di sicurezza del complesso fondazione-terreno devono essere eseguiti assumendo come azione in fondazione, trasmessa dagli elementi soprastanti, una tra le seguenti:

quella derivante dall'analisi strutturale eseguita ipotizzando comportamento strutturale non dissipativo;
[...];

quella trasferita dagli elementi soprastanti nell'ipotesi di comportamento strutturale dissipativo, amplificata di un coefficiente pari a 1,30 in CD“A” e 1,10 in CD“B”;

Nel contesto visualizzazione risultati e nella stampa della relazione sulle fondazioni PRO_SAP mostra le sollecitazioni che derivano dall'analisi non incrementate sia in termini di pressioni sul terreno che in termini di sollecitazioni.

La progettazione degli elementi strutturali con proprietà fondazione è effettuata da PRO_SAP (per travi e platee) o da PRO_CAD Plinti (per plinti e pali di fondazione) incrementando le sollecitazioni delle combinazioni con sisma di un coefficiente pari 1.1 in CDB e 1.3 in CDA per pali, plinti, travi e platee.

Per i bicchieri dei plinti di fondazione prefabbricati l'incremento delle sollecitazioni ha un fattore pari a 1.2 in CDB e 1.35 in CDA.

N.B.: nel caso di comportamento strutturale non dissipativo la progettazione viene effettuata senza nessun incremento.

Le verifiche geotecniche vengono effettuate dal modulo geotecnico incrementando automaticamente le sollecitazioni del fattore 1.1 in CDB e 1.3 in CDA per pali, plinti, travi e platee.

N.B.: nel caso di comportamento strutturale non dissipativo le verifiche geotecniche vengono effettuate senza nessun incremento.

Macro Guscio	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
1	50.00	3	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x daN/cm	N y daN/cm	N xy daN/cm	M x daN	M y daN	M xy daN
1	ok	0.09	3.46e-02	5.35e-03	7.7	7.7	7.7	7.7	1.2	-10.3	-13.5	-254.2	-240.6	-52.7
2	ok	0.09	4.35e-02	1.18e-03	7.7	7.7	7.7	7.7	-1.6	17.4	-5.2	125.9	-208.3	-36.6
3	ok	0.09	3.82e-02	1.92e-03	7.7	7.7	7.7	7.7	-11.0	16.3	-3.6	493.0	-256.6	-30.1
4	ok	0.09	5.47e-02	3.74e-03	7.7	7.7	7.7	7.7	-20.5	3.8	8.4	734.1	-392.3	-35.1
5	ok	0.09	4.03e-02	4.26e-03	7.7	7.7	7.7	7.7	-15.2	-1.0	19.5	537.0	-338.3	35.8
6	ok	0.09	4.26e-02	3.78e-03	7.7	7.7	7.7	7.7	-6.3	-3.1	20.8	254.5	-336.8	32.5
7	ok	0.09	3.05e-02	3.37e-03	7.7	7.7	7.7	7.7	-1.8	-13.3	13.3	-224.1	-335.6	29.9
8	ok	0.09	7.05e-02	5.17e-03	7.7	7.7	7.7	7.7	-12.0	30.1	-22.4	-217.1	-191.0	-22.6
9	ok	0.09	5.45e-02	3.62e-03	7.7	7.7	7.7	7.7	-17.5	18.3	-16.8	310.2	165.5	-245.9
10	ok	0.09	6.09e-02	3.03e-03	7.7	7.7	7.7	7.7	-9.4	12.7	-0.3	721.2	374.9	-229.1
11	ok	0.09	6.51e-02	3.84e-03	7.7	7.7	7.7	7.7	-15.2	-2.8	12.7	878.0	398.6	-55.5
12	ok	0.09	5.63e-02	4.14e-03	7.7	7.7	7.7	7.7	-18.4	-1.9	15.8	759.4	311.2	31.6
13	ok	0.09	4.67e-02	3.54e-03	7.7	7.7	7.7	7.7	-12.3	-4.5	15.0	590.2	260.4	70.9
14	ok	0.09	3.94e-02	5.21e-03	7.7	7.7	7.7	7.7	-22.5	-3.4	20.1	370.2	219.6	145.0
15	ok	0.09	7.09e-02	5.47e-03	7.7	7.7	7.7	7.7	3.1	10.3	29.2	-400.5	-210.5	114.7
16	ok	0.09	3.27e-02	9.17e-03	7.7	7.7	7.7	7.7	-31.3	-13.2	-37.7	-408.3	397.2	25.5
17	ok	0.09	4.16e-02	5.84e-03	7.7	7.7	7.7	7.7	-29.8	3.5	-4.6	378.7	524.5	-96.7
18	ok	0.09	7.87e-02	4.05e-03	7.7	7.7	7.7	7.7	-22.9	-2.0	-1.7	995.2	837.7	-140.3
19	ok	0.09	8.87e-02	4.31e-03	7.7	7.7	7.7	7.7	-22.8	-8.0	11.7	1170.4	1056.3	-85.0
20	ok	0.09	6.28e-02	5.32e-03	7.7	7.7	7.7	7.7	-29.3	-3.5	12.8	728.1	737.9	-111.5
21	ok	0.09	3.67e-02	8.42e-03	7.7	7.7	7.7	7.7	-44.3	-14.3	7.9	-448.9	436.2	-34.0
22	ok	0.09	2.70e-02	8.25e-03	7.7	7.7	7.7	7.7	-25.3	-8.1	-38.3	-226.6	269.4	37.5
23	ok	0.09	3.96e-02	6.13e-03	7.7	7.7	7.7	7.7	-16.5	1.2	-11.4	335.5	435.0	132.3
24	ok	0.09	6.70e-02	4.73e-03	7.7	7.7	7.7	7.7	-17.8	-21.7	-6.4	887.5	658.0	73.7
25	ok	0.09	7.65e-02	5.45e-03	7.7	7.7	7.7	7.7	-19.9	-20.3	-6.1	911.5	669.7	-226.2
26	ok	0.09	6.34e-02	6.76e-03	7.7	7.7	7.7	7.7	-24.4	-13.5	7.9	562.1	530.8	-307.2
27	ok	0.09	2.80e-02	6.93e-03	7.7	7.7	7.7	7.7	-19.6	-3.3	-0.8	-306.0	197.3	-62.7
28	ok	0.09	5.13e-02	2.03e-03	7.7	7.7	7.7	7.7	4.2	17.4	17.1	-109.3	-114.1	-6.2
29	ok	0.09	1.89e-02	5.46e-03	7.7	7.7	7.7	7.7	-14.2	-7.2	14.8	157.0	-123.3	67.8
30	ok	0.09	4.37e-02	8.84e-03	7.7	7.7	7.7	7.7	-51.9	-25.4	-16.6	544.2	-364.6	-22.0

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31	ok	0.09	4.21e-02	9.63e-03	7.7	7.7	7.7	7.7	-48.0	-41.9	20.0	519.2	-378.5	-51.3
32	ok	0.09	2.55e-02	6.05e-03	7.7	7.7	7.7	7.7	-33.5	-13.6	-12.3	301.0	-248.1	-43.2
33	ok	0.09	4.85e-02	2.49e-03	7.7	7.7	7.7	7.7	2.8	7.2	-17.9	-167.9	-114.7	-28.3
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
		0.09	0.09	9.63e-03	7.70	7.70	7.70	7.70	-51.91	-41.92	-38.28	-448.89	-392.29	-307.25
									4.17	30.14	29.23	1170.42	1056.28	144.97

Nodo	Stato	Max tau daN/cm2	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr daN/cm	V sec daN/cm
1	ok	0.47						
2	ok	0.72						
3	ok	1.08						
4	ok	1.19						
5	ok	1.32						
6	ok	1.11						
7	ok	0.27						
8	ok	1.03						
9	ok	1.81						
10	ok	2.06						
11	ok	1.98						
12	ok	2.19						
13	ok	1.57						
14	ok	1.27						
15	ok	0.99						
16	ok	1.58						
17	ok	1.85						
18	ok	1.85						
19	ok	1.90						
20	ok	2.15						
21	ok	1.38						
22	ok	1.04						
23	ok	1.71						
24	ok	1.90						
25	ok	1.80						
26	ok	1.59						
27	ok	0.69						
28	ok	0.37						
29	ok	0.58						
30	ok	0.79						
31	ok	0.96						
32	ok	0.73						
33	ok	0.15						
Nodo		Max tau 2.19	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec

Macro Guscio	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
6	50.00	3	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x daN/cm	N y daN/cm	N xy daN/cm	M x daN	M y daN	M xy daN
34	ok	0.09	4.74e-02	4.04e-03	7.7	7.7	7.7	7.7	-4.5	-9.8	-16.4	-345.2	-755.1	-262.1
35	ok	0.09	6.19e-02	8.75e-03	7.7	7.7	7.7	7.7	-45.2	-24.2	-22.1	578.7	-754.2	-320.6
36	ok	0.09	8.17e-02	9.40e-03	7.7	7.7	7.7	7.7	-54.1	-39.6	12.5	833.2	-1086.4	-155.3
37	ok	0.09	9.28e-02	9.77e-03	7.7	7.7	7.7	7.7	-51.1	-40.7	-9.7	604.3	-1259.0	-125.6
38	ok	0.09	0.1	9.73e-03	7.7	7.7	7.7	7.7	-44.7	-41.0	-6.3	435.7	-1325.0	-59.1
39	ok	0.09	0.1	9.48e-03	7.7	7.7	7.7	7.7	-39.0	-40.9	24.1	322.0	-1339.7	39.1
40	ok	0.09	0.1	9.45e-03	7.7	7.7	7.7	7.7	-36.4	-40.4	24.0	261.7	-1332.8	107.7
41	ok	0.09	0.1	9.38e-03	7.7	7.7	7.7	7.7	-39.9	-45.1	-5.7	262.6	-1341.0	152.1
42	ok	0.09	0.1	9.32e-03	7.7	7.7	7.7	7.7	-41.6	-43.5	-2.6	288.0	-1320.9	214.1
43	ok	0.09	9.95e-02	1.03e-02	7.7	7.7	7.7	7.7	-43.9	-48.4	20.7	283.5	-1308.7	229.5
44	ok	0.09	9.14e-02	9.26e-03	7.7	7.7	7.7	7.7	-43.1	-44.5	-5.6	276.0	-1201.8	279.0
45	ok	0.09	8.51e-02	8.65e-03	7.7	7.7	7.7	7.7	-41.9	-43.5	-1.7	254.5	-1086.0	325.9
46	ok	0.09	8.01e-02	8.72e-03	7.7	7.7	7.7	7.7	-39.6	-41.3	18.4	209.7	-999.1	331.6
47	ok	0.09	6.90e-02	7.47e-03	7.7	7.7	7.7	7.7	-30.3	-31.9	19.4	40.0	-789.1	360.6
48	ok	0.09	6.63e-02	7.24e-03	7.7	7.7	7.7	7.7	-20.5	-23.7	-4.7	-382.7	-548.1	428.7
49	ok	0.09	5.79e-02	4.87e-03	7.7	7.7	7.7	7.7	-9.9	-12.1	22.0	-565.5	-451.4	73.1
50	ok	0.09	0.1	6.91e-03	7.7	7.7	7.7	7.7	-22.9	-5.1	-13.0	-376.8	-1415.3	-478.4
51	ok	0.09	0.2	5.24e-03	7.7	7.7	7.7	7.7	-14.1	-31.3	-5.9	1352.9	408.8	-1198.8
52	ok	0.09	0.1	6.76e-03	7.7	7.7	7.7	7.7	-25.7	-40.7	-2.6	1331.7	1237.4	-683.9
53	ok	0.09	0.1	7.41e-03	7.7	7.7	7.7	7.7	-30.8	-43.5	-1.7	1219.8	1516.8	-459.2

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133	ok	0.09	0.2	6.65e-03	7.7	7.7	7.7	7.7	-14.5	-42.1	6.3	1834.6	3357.4	7.7
134	ok	0.09	0.2	6.63e-03	7.7	7.7	7.7	7.7	-17.0	-42.2	5.7	1851.3	3526.8	-72.7
135	ok	0.09	0.2	6.50e-03	7.7	7.7	7.7	7.7	-19.6	-41.6	4.2	1803.1	3526.9	-248.0
136	ok	0.09	0.2	6.83e-03	7.7	7.7	7.7	7.7	-21.5	-42.0	2.2	1730.3	3375.9	-461.2
137	ok	0.09	0.2	7.44e-03	7.7	7.7	7.7	7.7	-25.4	-42.9	1.3	1686.7	3078.4	-689.0
138	ok	0.09	0.2	7.32e-03	7.7	7.7	7.7	7.7	-27.4	-40.3	2.3	1640.6	2816.6	-822.2
139	ok	0.09	0.2	7.06e-03	7.7	7.7	7.7	7.7	-28.6	-38.2	2.1	1610.8	2657.6	-907.0
140	ok	0.09	0.2	6.17e-03	7.7	7.7	7.7	7.7	-33.7	-34.6	-2.7	1422.2	2125.7	-1074.6
141	ok	0.09	0.2	5.81e-03	7.7	7.7	7.7	7.7	-32.7	-35.8	-4.1	1218.2	1728.4	-1148.3
142	ok	0.09	0.2	5.70e-03	7.7	7.7	7.7	7.7	-31.5	-36.2	-2.3	1059.5	1511.4	-1185.7
143	ok	0.09	0.1	5.79e-03	7.7	7.7	7.7	7.7	-25.2	-28.9	-2.0	726.3	1122.9	-1119.4
144	ok	0.09	0.1	6.49e-03	7.7	7.7	7.7	7.7	-27.8	-25.7	-5.4	465.8	817.7	-1263.6
145	ok	0.09	8.93e-02	7.34e-03	7.7	7.7	7.7	7.7	-31.9	-22.1	10.0	-909.1	345.8	-289.4
146	ok	0.09	0.1	1.85e-02	7.7	7.7	7.7	7.7	-12.9	-36.1	27.3	60.3	-1593.3	-202.8
147	ok	0.09	0.2	7.20e-03	7.7	7.7	7.7	7.7	-22.2	-41.4	-3.2	2061.8	466.8	-286.1
148	ok	0.09	0.1	6.28e-03	7.7	7.7	7.7	7.7	-15.8	-41.0	4.6	1636.6	1839.9	205.5
149	ok	0.09	0.2	6.58e-03	7.7	7.7	7.7	7.7	-16.7	-42.1	5.9	1589.6	2346.3	175.7
150	ok	0.09	0.2	6.55e-03	7.7	7.7	7.7	7.7	-20.6	-41.9	7.3	1511.5	2542.3	-22.5
151	ok	0.09	0.2	6.23e-03	7.7	7.7	7.7	7.7	-23.6	-39.9	3.8	1424.3	2571.1	-274.2
152	ok	0.09	0.2	6.62e-03	7.7	7.7	7.7	7.7	-24.7	-42.0	-0.2	1336.6	2440.6	-568.9
153	ok	0.09	0.2	8.02e-03	7.7	7.7	7.7	7.7	-23.7	-45.3	1.6	1303.5	2158.3	-862.1
154	ok	0.09	0.2	8.03e-03	7.7	7.7	7.7	7.7	-26.7	-41.5	4.8	1287.3	1936.0	-1024.6
155	ok	0.09	0.2	7.61e-03	7.7	7.7	7.7	7.7	-29.0	-37.7	4.8	1266.9	1803.2	-1117.0
156	ok	0.09	0.2	5.98e-03	7.7	7.7	7.7	7.7	-36.0	-30.8	-3.7	1154.4	1414.0	-1311.3
157	ok	0.09	0.2	6.24e-03	7.7	7.7	7.7	7.7	-32.7	-36.4	-7.5	1010.0	1126.7	-1394.2
158	ok	0.09	0.2	6.46e-03	7.7	7.7	7.7	7.7	-29.3	-39.5	-6.1	883.9	971.1	-1426.8
159	ok	0.09	0.1	6.09e-03	7.7	7.7	7.7	7.7	-20.9	-33.6	-2.1	595.8	724.9	-1341.7
160	ok	0.09	0.1	6.89e-03	7.7	7.7	7.7	7.7	-22.7	-30.9	-0.8	345.9	523.3	-1501.7
161	ok	0.09	8.05e-02	6.40e-03	7.7	7.7	7.7	7.7	-27.4	-15.1	-6.4	-784.2	146.0	-340.8
162	ok	0.09	0.2	9.25e-03	7.7	7.7	7.7	7.7	-37.2	14.9	20.6	-474.9	-1861.4	726.7
163	ok	0.09	0.2	6.10e-03	7.7	7.7	7.7	7.7	-8.0	-37.8	2.2	1694.8	-749.4	1142.6
164	ok	0.09	0.1	6.24e-03	7.7	7.7	7.7	7.7	-19.3	-40.0	5.0	1310.5	664.7	630.6
165	ok	0.09	0.1	6.57e-03	7.7	7.7	7.7	7.7	-16.8	-32.4	5.2	1107.8	1172.0	352.9
166	ok	0.09	9.72e-02	6.65e-03	7.7	7.7	7.7	7.7	-16.3	-31.1	4.8	972.9	1320.6	79.1
167	ok	0.09	0.1	6.18e-03	7.7	7.7	7.7	7.7	-23.5	-37.7	4.1	897.0	1278.2	-276.1
168	ok	0.09	0.1	6.05e-03	7.7	7.7	7.7	7.7	-29.1	-37.6	-3.2	784.9	1210.5	-652.7
169	ok	0.09	0.1	9.74e-03	7.7	7.7	7.7	7.7	-19.1	-53.4	1.2	816.3	861.0	-1033.7
170	ok	0.09	0.1	1.01e-02	7.7	7.7	7.7	7.7	-21.8	-47.3	9.6	852.8	662.6	-1180.3
171	ok	0.09	0.1	9.44e-03	7.7	7.7	7.7	7.7	-31.2	-37.4	13.7	859.9	565.5	-1231.8
172	ok	0.09	0.1	6.15e-03	7.7	7.7	7.7	7.7	-40.4	-20.3	-5.2	803.6	470.1	-1430.4
173	ok	0.09	0.2	7.75e-03	7.7	7.7	7.7	7.7	-37.9	-33.5	-16.6	751.0	318.6	-1545.8
174	ok	0.09	0.1	8.91e-03	7.7	7.7	7.7	7.7	-29.5	-45.7	-16.8	705.5	220.8	-1558.9
175	ok	0.09	0.1	8.28e-03	7.7	7.7	7.7	7.7	-19.1	-53.6	-1.3	443.3	96.6	-1499.5
176	ok	0.09	0.1	8.09e-03	7.7	7.7	7.7	7.7	-19.3	-43.0	3.2	194.8	144.5	-1565.1
177	ok	0.09	6.91e-02	5.57e-03	7.7	7.7	7.7	7.7	-24.0	-0.2	13.3	-589.3	-205.3	-381.4
178	ok	0.09	0.1	5.68e-03	7.7	7.7	7.7	7.7	-18.5	-3.5	11.0	-480.8	-1235.5	500.7
179	ok	0.09	0.1	5.72e-03	7.7	7.7	7.7	7.7	-24.2	-31.6	2.5	540.1	-645.5	1263.6
180	ok	0.09	8.14e-02	6.61e-03	7.7	7.7	7.7	7.7	-27.4	-40.5	1.3	911.5	-515.1	570.4
181	ok	0.09	6.69e-02	6.80e-03	7.7	7.7	7.7	7.7	-24.9	-41.4	0.9	693.6	-454.6	277.4
182	ok	0.09	6.76e-02	6.94e-03	7.7	7.7	7.7	7.7	-23.1	-41.2	6.8	505.4	-429.8	62.0
183	ok	0.09	6.12e-02	6.70e-03	7.7	7.7	7.7	7.7	-18.0	-40.9	8.3	375.7	-398.7	-177.2
184	ok	0.09	4.89e-02	5.04e-03	7.7	7.7	7.7	7.7	-19.2	-28.9	4.1	329.4	-427.4	-394.1
185	ok	0.09	9.84e-02	1.57e-02	7.7	7.7	7.7	7.7	-27.7	-76.0	-7.8	255.9	-816.8	-921.1
186	ok	0.09	0.1	2.69e-02	7.7	7.7	7.7	7.7	-42.3	-91.4	45.1	510.3	-1487.5	-794.5
187	ok	0.09	0.1	9.87e-03	7.7	7.7	7.7	7.7	-32.7	-22.3	16.4	371.5	-1103.5	-729.8
188	ok	0.09	8.68e-02	5.44e-03	7.7	7.7	7.7	7.7	-28.0	-8.7	-0.8	467.3	-672.8	-925.2
189	ok	0.09	9.07e-02	7.33e-03	7.7	7.7	7.7	7.7	-38.0	-21.4	-10.4	451.6	-593.8	-1048.2
190	ok	0.09	0.1	1.32e-02	7.7	7.7	7.7	7.7	-49.3	-39.0	-26.3	456.4	-697.6	-1154.7
191	ok	0.09	9.11e-02	1.55e-02	7.7	7.7	7.7	7.7	-27.3	-99.3	-15.8	693.0	-741.1	-811.4
192	ok	0.09	9.02e-02	1.49e-02	7.7	7.7	7.7	7.7	-47.5	-33.7	-0.3	-61.3	-262.2	-1024.9
193	ok	0.09	6.16e-02	4.07e-03	7.7	7.7	7.7	7.7	-27.5	-0.1	-1.6	-508.5	-521.3	-233.7
194	ok	0.09	4.96e-02	5.96e-03	7.7	7.7	7.7	7.7	-18.5	-23.1	19.4	-664.2	-569.1	-26.0
195	ok	0.09	6.22e-02	8.42e-03	7.7	7.7	7.7	7.7	-29.3	-27.6	28.4	570.7	-835.0	24.8
196	ok	0.09	8.83e-02	8.95e-03	7.7	7.7	7.7	7.7	-37.1	-39.9	-15.8	827.2	-1205.5	77.6
197	ok	0.09	9.92e-02	8.64e-03	7.7	7.7	7.7	7.7	-31.7	-41.6	-18.8	570.2	-1364.6	52.7
198	ok	0.09	0.1	8.76e-03	7.7	7.7	7.7	7.7	-23.6	-41.0	-19.0	364.6	-1415.1	36.8
199	ok	0.09	0.1	8.62e-03	7.7	7.7	7.7	7.7	-16.7	-37.5	-16.6	239.5	-1407.6	15.5
200	ok	0.09	0.1	5.53e-03	7.7	7.7	7.7	7.7	-8.3	-22.1	-9.4	155.6	-1415.4	-48.4
201	ok	0.09	0.1	4.86e-02	7.7	7.7	7.7	7.7	-88.1	-194.8	39.6	31.3	-2219.6	-275.5
202	ok	0.09	0.2	1.32e-02	7.7	7.7	7.7	7.7	-48.5	15.1	16.8	-125.5	-2773.0	70.1
203	ok	0.09	0.1	6.23e-03	7.7	7.7	7.7	7.7	-22.9	-14.1	4.2	165.7	-1992.7	-28.8
204	ok	0.09	9.48e-02	3.71e-03	7.7	7.7	7.7	7.7	-9.5	-7.4	0.7	414.8	-1298.0	-62.9
205	ok	0.09	7.97e-02	5.14e-03	7.7	7.7	7.7	7.7	-27.0	-13.8	1.6	377.1	-1084.6	-73.8
206	ok	0.09	9.78e-02	7.79e-03	7.7	7.7	7.7	7.7	-40.8	15.8	15.8	357.2	-985.3	44.1
207	ok	0.09	9.41e-02	3.08e-02	7.7	7.7	7.7	7.7	-149.8	-151.4	58.4	1081.8	-681.8	-390.2
208	ok	0.09	0.1	1.23e-02	7.7	7.7	7.7	7.7	-43.9	-30.7	-3.1	-267.2	-513.5	-120.2
209	ok	0.09	6.46e-02	4.15e-03	7.7	7.7	7.7	7.7	-2.6	-11.4	-20.7	-683.7	-244.5	20.0
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy

SCARICATORE IN VIA PUCCI

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REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

107	ok	0.71							
108	ok	0.86							
109	ok	0.90							
110	ok	0.98							
111	ok	1.12							
112	ok	1.32							
113	ok	1.56							
114	ok	1.88							
115	ok	1.15							
116	ok	1.06							
117	ok	0.93							
118	ok	0.84							
119	ok	0.86							
120	ok	0.91							
121	ok	0.96							
122	ok	0.88							
123	ok	0.88							
124	ok	1.01							
125	ok	0.98							
126	ok	1.01							
127	ok	1.10							
128	ok	1.31							
129	ok	1.65							
130	ok	3.51							
131	ok	2.27							
132	ok	1.33							
133	ok	1.15							
134	ok	1.10							
135	ok	1.14							
136	ok	1.18							
137	ok	1.19							
138	ok	1.06							
139	ok	1.07							
140	ok	1.06							
141	ok	0.95							
142	ok	0.93							
143	ok	0.94							
144	ok	1.19							
145	ok	1.82							
146	ok Av	7.48	0.20	0.26	5.9	7.5	226.0	287.6	
147	ok	1.51							
148	ok	1.31							
149	ok	1.27							
150	ok	1.31							
151	ok	1.33							
152	ok	1.35							
153	ok	1.36							
154	ok	1.26							
155	ok	1.25							
156	ok	1.08							
157	ok	0.96							
158	ok	0.87							
159	ok	0.82							
160	ok	1.04							
161	ok	1.76							
162	ok Av	4.31	0.11	0.13	3.2	3.7	123.0	142.3	
163	ok	1.85							
164	ok	1.34							
165	ok	1.45							
166	ok	1.56							
167	ok	1.58							
168	ok	1.55							
169	ok	1.62							
170	ok	1.52							
171	ok	1.50							
172	ok	1.16							
173	ok	0.98							
174	ok	0.85							
175	ok	0.70							
176	ok	0.88							
177	ok	1.57							
178	ok	2.65							
179	ok	1.01							
180	ok	1.58							
181	ok	1.82							
182	ok	1.87							
183	ok	1.86							
184	ok	1.89							
185	ok	1.95							

SCARICATORE IN VIA PUCCI

186	ok	2.10
187	ok	2.05
188	ok	1.67
189	ok	1.46
190	ok	1.36
191	ok	0.96
192	ok	0.65
193	ok	1.37
194	ok	2.32
195	ok	1.84
196	ok	2.02
197	ok	2.00
198	ok	1.97
199	ok	1.99
200	ok	2.14
201	ok	2.96
202	ok	2.66
203	ok	2.49
204	ok	2.53
205	ok	2.61
206	ok	2.85
207	ok	2.11
208	ok	1.76
209	ok	1.60

Nodo	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
	7.48	0.20	0.26	5.89	7.49	226.00	287.57

Macro Guscio	Spessore	Id Materiale	Id Criterio	Progettazione
	cm			
10	30.00	3	1	Singolo elemento

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
									daN/cm	daN/cm	daN/cm	daN	daN	daN
521	ok	0.16	9.74e-02	7.22e-03	7.7	7.7	7.7	7.7	-28.8	-10.9	6.8	588.8	398.2	225.3
522	ok	0.16	0.2	1.19e-02	7.7	7.7	7.7	7.7	-41.1	-20.7	-17.5	-147.7	712.5	708.9
523	ok	0.16	0.2	7.01e-03	7.7	7.7	7.7	7.7	-19.6	-25.2	-7.2	31.4	1542.1	425.1
524	ok	0.16	0.3	7.11e-03	7.7	7.7	7.7	7.7	-8.5	-29.6	-2.9	153.2	1917.9	283.9
525	ok	0.16	0.3	7.23e-03	7.7	7.7	7.7	7.7	-2.1	-30.9	-2.5	247.7	2154.9	170.0
526	ok	0.16	0.3	7.39e-03	7.7	7.7	7.7	7.7	0.3	-31.2	-4.4	311.9	2276.1	66.0
527	ok	0.16	0.3	8.26e-03	7.7	7.7	7.7	7.7	0.6	-34.7	-5.5	353.7	2259.6	-43.5
528	ok	0.16	0.3	8.19e-03	7.7	7.7	7.7	7.7	-1.5	-31.2	-6.0	305.0	2222.9	-167.9
529	ok	0.16	0.3	8.63e-03	7.7	7.7	7.7	7.7	-3.8	-29.4	-7.7	283.1	2088.3	-204.1
530	ok	0.16	0.3	8.23e-03	7.7	7.7	7.7	7.7	-7.7	-30.2	-7.8	257.5	2035.7	-245.2
531	ok	0.16	0.2	8.08e-03	7.7	7.7	7.7	7.7	-6.2	-26.1	-10.7	252.3	1747.3	-426.3
532	ok	0.16	0.2	7.66e-03	7.7	7.7	7.7	7.7	-6.2	-25.3	-10.0	163.4	1477.0	-382.1
533	ok	0.16	0.2	7.00e-03	7.7	7.7	7.7	7.7	-6.1	-23.9	-9.6	128.3	1314.9	-398.3
534	ok	0.16	0.2	6.11e-03	7.7	7.7	7.7	7.7	-3.5	-19.1	-9.0	115.6	981.9	-427.8
535	ok	0.16	0.1	4.49e-03	7.7	7.7	7.7	7.7	0.3	-13.4	-10.8	251.5	681.7	-488.5
536	ok	0.16	6.37e-02	4.09e-03	7.7	7.7	7.7	7.7	-13.1	-16.8	0.4	339.2	348.7	-129.1
537	ok	0.16	0.2	6.68e-03	7.7	7.7	7.7	7.7	-20.1	74.4	29.9	629.3	705.0	265.6
538	ok	0.16	0.2	2.93e-03	7.7	7.7	7.7	7.7	-0.2	58.5	2.1	425.5	660.1	989.9
539	ok	0.16	0.2	8.17e-03	7.7	7.7	7.7	7.7	-0.5	-17.7	-15.0	-338.0	365.9	1483.5
540	ok	0.16	0.2	8.91e-03	7.7	7.7	7.7	7.7	-5.6	-32.9	-7.3	-474.2	34.9	1211.2
541	ok	0.16	0.2	7.77e-03	7.7	7.7	7.7	7.7	-7.2	-32.2	-5.8	-451.3	-38.7	926.5
542	ok	0.16	0.1	7.28e-03	7.7	7.7	7.7	7.7	-6.8	-30.9	-3.2	-368.1	-25.9	560.2
543	ok	0.16	6.06e-02	7.01e-03	7.7	7.7	7.7	7.7	-5.6	-24.0	-1.0	-367.1	-79.3	155.8
544	ok	0.16	6.26e-02	7.00e-03	7.7	7.7	7.7	7.7	-6.0	-23.3	-2.5	-368.5	-89.3	-129.4
545	ok	0.16	6.86e-02	6.95e-03	7.7	7.7	7.7	7.7	-6.3	-23.2	-2.9	-372.0	-101.5	-221.8
546	ok	0.16	9.63e-02	7.11e-03	7.7	7.7	7.7	7.7	-8.1	-28.4	-6.6	-302.6	-48.1	-516.5
547	ok	0.16	0.1	7.60e-03	7.7	7.7	7.7	7.7	-8.9	-29.5	-8.8	-309.9	-21.3	-758.7
548	ok	0.16	0.1	7.63e-03	7.7	7.7	7.7	7.7	-9.9	-26.3	-9.9	-302.7	57.6	-937.3
549	ok	0.16	0.2	7.48e-03	7.7	7.7	7.7	7.7	-10.5	-26.3	-10.7	-306.6	-20.1	-1103.0
550	ok	0.16	0.2	7.60e-03	7.7	7.7	7.7	7.7	-10.7	-25.7	-10.3	-279.2	-61.6	-1312.5
551	ok	0.16	0.2	7.55e-03	7.7	7.7	7.7	7.7	-11.4	-24.6	-13.0	-244.9	-58.9	-1383.3
552	ok	0.16	0.2	6.82e-03	7.7	7.7	7.7	7.7	-13.2	-22.0	-8.7	-129.9	-26.9	-1444.7
553	ok	0.16	0.2	6.40e-03	7.7	7.7	7.7	7.7	-16.5	-21.3	-6.3	23.2	-0.3	-1659.8
554	ok	0.16	0.1	5.53e-03	7.7	7.7	7.7	7.7	-13.3	-22.9	1.5	577.6	234.2	-530.6
555	ok	0.16	0.1	1.47e-02	7.7	7.7	7.7	7.7	-23.0	98.9	-55.5	914.9	496.8	89.6
556	ok	0.16	0.1	9.21e-03	7.7	7.7	7.7	7.7	-9.6	52.6	-35.3	438.6	420.3	661.5
557	ok	0.16	0.2	6.86e-03	7.7	7.7	7.7	7.7	12.2	-28.1	-7.4	-616.1	-270.8	1107.9
558	ok	0.16	0.2	9.18e-03	7.7	7.7	7.7	7.7	-4.0	-36.0	-3.2	-995.0	-994.6	884.4
559	ok	0.16	0.2	8.07e-03	7.7	7.7	7.7	7.7	-7.9	-34.5	-2.4	-1049.8	-1234.6	713.9
560	ok	0.16	0.2	7.35e-03	7.7	7.7	7.7	7.7	-10.3	-31.4	-1.9	-1016.5	-1425.6	441.7

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

728	ok	0.16	7.60e-02	4.90e-03	7.7	7.7	7.7	7.7	0.4	-0.7	3.7	52.2	408.9	-305.8
729	ok	0.16	3.65e-02	5.06e-03	7.7	7.7	7.7	7.7	-1.8	2.7	5.7	99.1	275.2	-37.2
730	ok	0.16	2.92e-02	4.01e-03	7.7	7.7	7.7	7.7	-6.8	3.4	-8.1	208.0	-96.4	-62.8
731	ok	0.16	3.99e-02	5.52e-03	7.7	7.7	7.7	7.7	-16.6	-3.8	-12.0	-67.1	-213.9	-120.4
732	ok	0.16	4.67e-02	1.86e-03	7.7	7.7	7.7	7.7	-5.3	0.3	-1.0	-258.7	81.6	-204.1
733	ok	0.16	6.00e-02	5.37e-03	7.7	7.7	7.7	7.7	-9.1	-15.4	9.3	-160.0	-418.7	38.0
734	ok	0.16	3.63e-02	3.83e-03	7.7	7.7	7.7	7.7	-8.8	-3.5	8.4	-102.2	-194.7	94.5
735	ok	0.16	1.87e-02	3.01e-03	7.7	7.7	7.7	7.7	-5.2	-1.7	4.3	135.1	-105.7	19.6
736	ok	0.16	1.00e-02	4.82e-04	7.7	7.7	7.7	7.7	0.3	1.6	2.1	75.4	57.5	2.4
737	ok	0.16	1.90e-02	1.60e-03	7.7	7.7	7.7	7.7	-2.0	-0.7	1.2	84.6	32.5	-69.4
738	ok	0.16	3.49e-02	5.35e-03	7.7	7.7	7.7	7.7	-20.9	-6.5	-6.0	-200.6	208.4	-62.3
739	ok	0.16	2.53e-02	3.86e-03	7.7	7.7	7.7	7.7	-11.4	-5.9	4.2	21.1	127.0	69.8
740	ok	0.16	1.85e-02	2.41e-03	7.7	7.7	7.7	7.7	-8.7	-2.7	5.71e-02	-20.2	95.2	49.2
741	ok	0.16	1.00e-02	3.25e-04	7.7	7.7	7.7	7.7	0.6	2.2	-0.9	64.4	35.3	16.6
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N x	N y	N xy	M x	M y	M xy
		0.16	0.80	0.04	7.70	7.70	7.70	7.70	-46.53	-174.36	-86.85	-2741.50	-5479.88	-2183.83
									56.87	134.10	83.30	2244.70	4102.21	3299.16

Nodo	Stato	Max tau daN/cm2	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr daN/cm	V sec daN/cm
521	ok	3.62						
522	ok	4.29						
523	ok	4.33						
524	ok	4.00						
525	ok	3.56						
526	ok	3.32						
527	ok	3.53						
528	ok	3.45						
529	ok	3.64						
530	ok	3.82						
531	ok	4.25						
532	ok	4.30						
533	ok	4.27						
534	ok	4.19						
535	ok	3.83						
536	ok	2.72						
537	ok Av	7.49	0.08	0.28	2.2	8.2	46.6	171.3
538	ok	3.89						
539	ok	3.23						
540	ok	2.74						
541	ok	2.67						
542	ok	3.01						
543	ok	3.14						
544	ok	3.45						
545	ok	3.15						
546	ok	3.00						
547	ok	2.90						
548	ok	2.76						
549	ok	2.44						
550	ok	2.42						
551	ok	2.23						
552	ok	2.07						
553	ok	2.99						
554	ok	3.44						
555	ok Av	5.10	0.16	0.12	4.6	3.6	94.6	74.6
556	ok	3.68						
557	ok	2.70						
558	ok	2.07						
559	ok	2.11						
560	ok	2.31						
561	ok	2.45						
562	ok	2.67						
563	ok	2.45						
564	ok	2.23						
565	ok	2.16						
566	ok	2.07						
567	ok	1.92						
568	ok	1.79						
569	ok	1.57						
570	ok	1.51						
571	ok	2.29						
572	ok	3.78						
573	ok	2.13						
574	ok	2.14						
575	ok	2.47						
576	ok	1.79						
577	ok	1.67						

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

578	ok	1.69							
579	ok	1.71							
580	ok	1.91							
581	ok	1.68							
582	ok	1.52							
583	ok	1.48							
584	ok	1.48							
585	ok	1.52							
586	ok	1.56							
587	ok	1.55							
588	ok	1.74							
589	ok	2.34							
590	ok	3.31							
591	ok	1.87							
592	ok	1.76							
593	ok	1.90							
594	ok	1.56							
595	ok	1.24							
596	ok	1.11							
597	ok	1.04							
598	ok	1.14							
599	ok	0.92							
600	ok	0.88							
601	ok	0.89							
602	ok	0.99							
603	ok	1.19							
604	ok	1.37							
605	ok	1.53							
606	ok	1.84							
607	ok	2.30							
608	ok	2.76							
609	ok	2.66							
610	ok	1.82							
611	ok	2.69							
612	ok	3.90							
613	ok	0.92							
614	ok	1.07							
615	ok	0.88							
616	ok	4.76							
617	ok	3.84							
618	ok	2.20							
619	ok	2.05							
620	ok	3.91							
621	ok	1.24							
622	ok	1.50							
623	ok	1.61							
624	ok	1.85							
625	ok	2.33							
626	ok	2.85							
627	ok	3.85							
628	ok Av	14.85	0.29	0.56	8.3	16.2	172.1	337.1	
629	ok	3.17							
630	ok	3.05							
631	ok	1.79							
632	ok	1.93							
633	ok	2.25							
634	ok Av	7.47	0.28	0.23	8.2	6.7	170.8	138.2	
635	ok Av	6.70	0.26	0.05	7.5	1.5	154.9	31.8	
636	ok	1.56							
637	ok	3.96							
638	ok Av	10.79	0.31	0.38	9.1	11.1	189.6	231.5	
639	ok	2.45							
640	ok	1.76							
641	ok	1.61							
642	ok	1.56							
643	ok	2.27							
644	ok	3.46							
645	ok	2.05							
646	ok	4.13							
648	ok	1.24							
649	ok	3.46							
650	ok	2.49							
651	ok	2.93							
652	ok	5.02							
656	ok Av	8.01	0.03	0.31	0.9	9.1	17.8	188.2	
657	ok	2.90							
658	ok	2.07							
659	ok	1.70							
660	ok	1.43							

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

661	ok	2.15						
662	ok	3.55						
663	ok	2.71						
664	ok	2.24						
666	ok	3.52						
667	ok	3.93						
668	ok	3.06						
669	ok	3.33						
670	ok Av	9.20	0.03	0.36	1.0	10.4	21.0	216.0
674	ok Av	9.72	0.08	0.37	2.5	10.8	51.2	223.7
675	ok	3.25						
676	ok	2.54						
677	ok	2.21						
678	ok	1.51						
679	ok	2.17						
680	ok	3.36						
681	ok	2.00						
682	ok	2.39						
683	ok	2.63						
684	ok Av	10.20	0.40	0.22	11.5	6.2	239.0	129.8
685	ok	3.19						
686	ok	3.58						
687	ok	3.56						
688	ok Av	17.53	0.62	0.34	18.0	9.7	374.4	202.2
689	ok Av	15.37	0.58	0.17	16.7	5.0	347.2	104.9
690	ok Av	6.65	0.25	0.06	7.4	1.7	152.8	35.7
691	ok	1.99						
692	ok Av	5.16	0.18	0.09	5.3	2.5	110.2	51.6
693	ok Av	17.44	0.65	0.50	18.8	14.6	389.7	303.4
694	ok	3.06						
695	ok	3.21						
696	ok	3.23						
697	ok	2.88						
698	ok	1.63						
699	ok	2.48						
700	ok	1.34						
701	ok	2.67						
702	ok Av	8.22	0.32	0.07	9.1	1.9	190.0	39.5
703	ok	4.16						
704	ok	4.01						
705	ok	4.49						
706	ok Av	12.09	0.47	0.20	13.6	5.9	281.9	123.1
707	ok Av	5.04	0.19	0.06	5.5	1.7	113.9	35.5
708	ok	4.19						
709	ok	3.48						
710	ok	4.07						
711	ok	3.44						
712	ok	3.40						
713	ok	3.59						
714	ok	3.36						
715	ok	4.14						
716	ok	2.92						
717	ok	1.61						
718	ok Av	7.74	0.30	0.02	8.8	0.7	182.1	13.9
719	ok Av	6.41	0.25	0.05	7.1	1.5	148.2	30.3
720	ok	4.79						
721	ok Av	7.42	0.28	0.08	8.1	2.3	168.4	47.9
722	ok	2.16						
723	ok	3.50						
724	ok	0.87						
725	ok	1.66						
727	ok Av	5.21	0.07	0.19	2.1	5.5	43.2	115.1
728	ok	2.29						
729	ok	0.78						
730	ok	1.01						
731	ok	1.25						
732	ok	2.80						
733	ok	1.62						
734	ok	0.94						
735	ok	0.42						
736	ok	0.23						
737	ok	0.42						
738	ok	1.08						
739	ok	0.91						
740	ok	0.51						
741	ok	0.19						
Nodo		Max tau 17.53	Ver V pr 0.65	Ver V sec 0.56	Af V pr 18.76	Af V sec 16.23	V pr 389.72	V sec 337.13

Parete	H totale	Spessore	H critica	H critica V	L totale	L confinata	Verif. N	Verif. N-M	Fattore V	Diagramma V	Verif. V	Prog. composta
	cm	cm	cm	cm	cm	cm						
2	265.00	20.00	40.00	40.00	465.00	30.00	ok	ok	1.50	SI	ok	SI

Quota	Af conf.	Af std	Af V (ori)	Ver. N	Ver. N/M	Ver. V cls	Ver. V acc	Ver. V acc(7)	Ver. V scorr.	N add	M invil	V invil
cm										daN	daN	daN
-305.0	4d14	14/20	14/30	0.03	2.73e-03	0.07	0.04	0.09	0.06	0.0	7.089e+05	5779.63
-270.0	4d14	14/20	14/30	0.03	8.97e-03	0.06	0.03	0.09	0.06	0.0	7.089e+05	5779.63
-231.7	0d0	14/20	14/30	0.03	8.77e-03	0.02	0.02	0.07	0.0	0.0	7.089e+05	5779.63
-193.3	0d0	14/20	14/30	0.03	5.71e-03	0.02	0.02	0.07	0.0	0.0	7.089e+05	5391.14
-155.0	0d0	14/20	14/30	0.03	4.63e-03	0.02	0.02	0.07	0.0	0.0	7.089e+05	4875.53
-116.7	0d0	14/20	14/30	0.03	5.42e-03	0.02	0.02	0.06	0.0	0.0	7.089e+05	4359.92
-82.2	0d0	14/20	14/30	0.03	7.54e-03	0.01	0.02	0.05	0.0	0.0	7.089e+05	3896.07
-81.8	0d0	14/20	14/30	0.03	7.73e-03	0.01	0.02	0.05	0.0	0.0	7.089e+05	3891.48
-81.5	0d0	14/20	14/30	0.03	7.88e-03	0.01	0.02	0.05	0.0	0.0	7.089e+05	3886.88
-81.2	0d0	14/20	14/30	0.03	7.96e-03	0.01	0.02	0.05	0.0	0.0	7.089e+05	3882.29
-80.8	0d0	14/20	14/30	0.03	7.97e-03	0.01	0.02	0.04	0.0	0.0	7.089e+05	3877.69
-80.5	0d0	14/20	14/30	0.03	7.91e-03	0.01	0.02	0.04	0.0	0.0	7.089e+05	3873.09
-80.1	0d0	14/20	14/30	0.03	7.80e-03	0.01	0.02	0.04	0.0	0.0	7.089e+05	3868.30
-80.0	0d0	14/20	14/30	0.03	7.75e-03	0.01	0.02	0.04	0.0	0.0	7.089e+05	3866.73
-79.9	0d0	14/20	14/30	0.03	7.72e-03	0.01	0.02	0.04	0.0	0.0	7.089e+05	3865.22
-79.8	0d0	14/20	14/30	0.03	7.70e-03	0.01	0.02	0.04	0.0	0.0	7.089e+05	3863.50
-79.4	0d0	14/20	14/30	0.03	7.56e-03	0.01	0.02	0.04	0.0	0.0	7.089e+05	3858.70
-79.2	0d0	14/20	14/30	0.03	7.51e-03	0.01	0.02	0.04	0.0	0.0	7.089e+05	3855.52
-79.0	0d0	14/20	14/30	0.03	7.45e-03	0.01	0.02	0.04	0.0	0.0	7.089e+05	3853.90
-78.8	0d0	14/20	14/30	0.03	7.26e-03	0.01	0.02	0.04	0.0	0.0	7.089e+05	3850.98
-78.7	0d0	14/20	14/30	0.03	7.20e-03	0.01	0.02	0.04	0.0	0.0	7.089e+05	3849.11
-78.3	0d0	14/20	14/30	0.03	6.69e-03	0.01	0.02	0.04	0.0	0.0	7.089e+05	3844.31
-40.0	0d0	14/20	14/30	0.03	8.05e-03	0.01	0.01	0.04	0.0	0.0	7.089e+05	3328.70

Quota	Ver. N	Ver. N/M	Ver. V cls	Ver. V acc	Ver. V acc(7)	Ver. V scorr.
	0.03	8.97e-03	0.07	0.04	0.09	0.06

Quota	N v.N	N v.M/N	M v.M/N	N v.Vcls	V v.Vcls	N v.Vacc	M v. Vacc	V v.Vacc	N v.Vscor	M v.Vscor	V v.Vscor
cm	daN	daN	daN cm	daN	daN	daN	daN cm	daN	daN	daN cm	daN
-305.0	-5086.38	-3946.29	1.343e+04	-3946.29	2175.79	-5086.38	8583.41	1406.42	-3946.29	1.343e+04	2175.79
-270.0	-5412.69	-4130.50	4.425e+04	-4130.50	2108.09	-5412.69	3.801e+04	1338.72	-4130.50	4.425e+04	2108.09
-231.7	-2.091e+04	-1.831e+04	5.098e+05	-1.846e+04	5779.63	-1.832e+04	4.956e+05	3415.40	0.0	0.0	0.0
-193.3	-1.949e+04	-1.718e+04	3.307e+05	-1.749e+04	5588.88	-1.715e+04	3.147e+05	3532.75	0.0	0.0	0.0
-155.0	-1.853e+04	-1.684e+04	2.678e+05	-1.713e+04	5214.39	-1.680e+04	2.604e+05	3375.32	0.0	0.0	0.0
-116.7	-1.801e+04	-1.750e+04	3.145e+05	-1.728e+04	4612.11	-1.711e+04	2.794e+05	3188.81	0.0	0.0	0.0
-82.2	-1.840e+04	-1.777e+04	4.375e+05	-1.825e+04	3891.68	-1.762e+04	3.956e+05	2901.51	0.0	0.0	0.0
-81.8	-1.830e+04	-1.773e+04	4.485e+05	-1.816e+04	3775.01	-1.758e+04	4.051e+05	2898.55	0.0	0.0	0.0
-81.5	-1.818e+04	-1.769e+04	4.569e+05	-1.805e+04	3686.13	-1.756e+04	4.117e+05	2869.35	0.0	0.0	0.0
-81.2	-1.809e+04	-1.766e+04	4.616e+05	-1.795e+04	3586.17	-1.754e+04	4.163e+05	2827.59	0.0	0.0	0.0
-80.8	-1.803e+04	-1.763e+04	4.626e+05	-1.785e+04	3493.21	-1.751e+04	4.189e+05	2749.87	0.0	0.0	0.0
-80.5	-1.801e+04	-1.765e+04	4.590e+05	-1.774e+04	3372.67	-1.751e+04	4.182e+05	2679.59	0.0	0.0	0.0
-80.1	-1.801e+04	-1.765e+04	4.525e+05	-1.765e+04	3229.71	-1.747e+04	4.149e+05	2666.04	0.0	0.0	0.0
-80.0	-1.801e+04	-1.766e+04	4.495e+05	-1.762e+04	3224.87	-1.747e+04	4.131e+05	2640.26	0.0	0.0	0.0
-79.9	-1.797e+04	-1.763e+04	4.478e+05	-1.758e+04	3282.75	-1.744e+04	4.116e+05	2557.24	0.0	0.0	0.0
-79.8	-1.796e+04	-1.762e+04	4.468e+05	-1.757e+04	3307.66	-1.743e+04	4.106e+05	2507.79	0.0	0.0	0.0
-79.4	-1.788e+04	-1.753e+04	4.385e+05	-1.750e+04	3365.49	-1.735e+04	4.026e+05	2409.24	0.0	0.0	0.0
-79.2	-1.786e+04	-1.752e+04	4.354e+05	-1.750e+04	3358.73	-1.734e+04	3.995e+05	2400.16	0.0	0.0	0.0
-79.0	-1.785e+04	-1.750e+04	4.321e+05	-1.749e+04	3356.59	-1.732e+04	3.962e+05	2393.45	0.0	0.0	0.0
-78.8	-1.783e+04	-1.772e+04	4.212e+05	-1.751e+04	3271.59	-1.724e+04	3.824e+05	2446.55	0.0	0.0	0.0
-78.7	-1.785e+04	-1.770e+04	4.176e+05	-1.756e+04	3207.13	-1.719e+04	3.719e+05	2442.66	0.0	0.0	0.0
-78.3	-1.776e+04	-1.758e+04	3.880e+05	-1.752e+04	3101.40	-1.706e+04	3.411e+05	2321.25	0.0	0.0	0.0
-40.0	-1.955e+04	-1.907e+04	4.687e+05	-1.948e+04	3328.70	-1.900e+04	4.473e+05	2089.66	0.0	0.0	0.0

Quota	Ctg Vcls	Vrsd Vcls	Vrcd Vcls	Ctg Vac	Vrsd Vac	Vrcd Vac	Vdd	Vid	[A s.i.	Incli.	Dist.]	Vfd
cm		daN	daN		daN	daN	daN	daN	cm2	gradi	cm	daN
-305.0	1.00	2175.79	3.273e+04	1.00	3.956e+04	3.282e+04	2.108e+04	3399.72	1.0	29.7	0.0	9004.50
-270.0	1.00	2108.09	3.274e+04	1.00	3.956e+04	3.284e+04	2.108e+04	3399.72	1.0	29.7	0.0	9222.78
-231.7	1.00	5779.63	3.065e+05	1.00	1.478e+05	3.065e+05	0.0	0.0	0.0	0.0	0.0	0.0
-193.3	1.00	5588.88	3.064e+05	1.00	1.478e+05	3.063e+05	0.0	0.0	0.0	0.0	0.0	0.0
-155.0	1.00	5214.39	3.063e+05	1.00	1.478e+05	3.062e+05	0.0	0.0	0.0	0.0	0.0	0.0
-116.7	1.00	4612.11	3.063e+05	1.00	1.478e+05	3.063e+05	0.0	0.0	0.0	0.0	0.0	0.0
-82.2	1.00	3891.68	3.065e+05	1.00	1.478e+05	3.064e+05	0.0	0.0	0.0	0.0	0.0	0.0
-81.8	1.00	3775.01	3.065e+05	1.00	1.478e+05	3.064e+05	0.0	0.0	0.0	0.0	0.0	0.0
-81.5	1.00	3686.13	3.065e+05	1.00	1.478e+05	3.064e+05	0.0	0.0	0.0	0.0	0.0	0.0

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-81.2	1.00	3586.17	3.064e+05	1.00	1.478e+05	3.064e+05	0.0	0.0	0.0	0.0	0.0	0.0
-80.8	1.00	3493.21	3.064e+05	1.00	1.478e+05	3.064e+05	0.0	0.0	0.0	0.0	0.0	0.0
-80.5	1.00	3372.67	3.064e+05	1.00	1.478e+05	3.064e+05	0.0	0.0	0.0	0.0	0.0	0.0
-80.1	1.00	3229.71	3.064e+05	1.00	1.478e+05	3.064e+05	0.0	0.0	0.0	0.0	0.0	0.0
-80.0	1.00	3224.87	3.064e+05	1.00	1.478e+05	3.064e+05	0.0	0.0	0.0	0.0	0.0	0.0
-79.9	1.00	3282.75	3.064e+05	1.00	1.478e+05	3.063e+05	0.0	0.0	0.0	0.0	0.0	0.0
-79.8	1.00	3307.66	3.064e+05	1.00	1.478e+05	3.063e+05	0.0	0.0	0.0	0.0	0.0	0.0
-79.4	1.00	3365.49	3.064e+05	1.00	1.478e+05	3.063e+05	0.0	0.0	0.0	0.0	0.0	0.0
-79.2	1.00	3358.73	3.064e+05	1.00	1.478e+05	3.063e+05	0.0	0.0	0.0	0.0	0.0	0.0
-79.0	1.00	3356.59	3.064e+05	1.00	1.478e+05	3.063e+05	0.0	0.0	0.0	0.0	0.0	0.0
-78.8	1.00	3271.59	3.064e+05	1.00	1.478e+05	3.063e+05	0.0	0.0	0.0	0.0	0.0	0.0
-78.7	1.00	3207.13	3.064e+05	1.00	1.478e+05	3.063e+05	0.0	0.0	0.0	0.0	0.0	0.0
-78.3	1.00	3101.40	3.064e+05	1.00	1.478e+05	3.063e+05	0.0	0.0	0.0	0.0	0.0	0.0
-40.0	1.00	3328.70	3.067e+05	1.00	1.478e+05	3.067e+05	0.0	0.0	0.0	0.0	0.0	0.0

Quota cm	V[7.4.16]	N daN	M daN cm	V daN	alfaS	VRd,c daN	VRd,s daN	V[7.4.17]	roH	roV	roN
-305.0	0.09	-3946.29	1.343e+04	2175.79	0.22	1.439e+04	8609.06	0.0	5.13e-03	7.70e-03	0.0
-270.0	0.09	-4130.50	4.425e+04	2108.09	0.23	1.456e+04	9046.98	0.0	5.13e-03	7.70e-03	0.0
-231.7	0.07	-1.846e+04	9.607e+04	5779.63	0.20	5.072e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-193.3	0.07	-1.749e+04	3.726e+04	5588.88	0.20	4.976e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-155.0	0.07	-1.713e+04	2.810e+04	5214.39	0.20	4.940e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-116.7	0.06	-1.728e+04	1.286e+05	4612.11	0.20	4.955e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-82.2	0.05	-1.825e+04	1.918e+05	3891.68	0.20	5.051e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-81.8	0.05	-1.816e+04	2.124e+05	3775.01	0.20	5.041e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-81.5	0.05	-1.805e+04	2.320e+05	3686.13	0.20	5.031e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-81.2	0.05	-1.795e+04	2.476e+05	3586.17	0.20	5.021e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-80.8	0.04	-1.785e+04	2.592e+05	3493.21	0.20	5.011e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-80.5	0.04	-1.774e+04	2.674e+05	3372.67	0.20	5.000e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-80.1	0.04	-1.765e+04	2.726e+05	3229.71	0.20	4.992e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-80.0	0.04	-1.762e+04	2.731e+05	3224.87	0.20	4.988e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-79.9	0.04	-1.758e+04	2.707e+05	3282.75	0.20	4.984e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-79.8	0.04	-1.757e+04	2.696e+05	3307.66	0.20	4.983e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-79.4	0.04	-1.750e+04	2.629e+05	3365.49	0.20	4.977e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-79.2	0.04	-1.750e+04	2.617e+05	3358.73	0.20	4.977e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-79.0	0.04	-1.749e+04	2.593e+05	3356.59	0.20	4.976e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-78.8	0.04	-1.751e+04	2.606e+05	3271.59	0.20	4.977e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-78.7	0.04	-1.756e+04	2.691e+05	3207.13	0.20	4.983e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-78.3	0.04	-1.752e+04	2.561e+05	3101.40	0.20	4.979e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0
-40.0	0.04	-1.948e+04	3.072e+05	3328.70	0.20	5.172e+04	2.780e+04	0.0	5.13e-03	7.70e-03	0.0

Quota	V[7.4.16]	V[7.4.17]
0.09	0.0	0.0

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z daN/cm	N o daN/cm	N zo daN/cm	M z daN	M o daN	M zo daN
1	ok	0.31	4.81e-02	0.0	10.3	10.3	5.1	5.1	17.5	9.0	-9.8	-53.6	48.3	-17.1
2	ok	0.31	6.58e-02	1.59e-02	10.3	10.3	5.1	5.1	-47.5	-3.3	14.2	-164.8	-100.0	26.1
3	ok	0.31	7.14e-02	1.90e-02	10.3	10.3	5.1	5.1	-58.4	-12.8	12.7	-239.3	-88.7	2.6
4	ok	0.28	9.72e-02	2.41e-02	7.7	7.7	5.1	5.1	-61.4	-18.6	-1.2	-365.9	-77.8	-7.9
5	ok	0.28	9.65e-02	2.62e-02	7.7	7.7	5.1	5.1	-63.4	-17.2	-16.3	-362.7	-85.9	-0.8
6	ok	0.31	8.28e-02	2.98e-02	10.3	10.3	5.1	5.1	-78.1	-14.1	-37.6	-336.7	-83.0	2.7
7	ok	0.31	5.14e-02	0.0	10.3	10.3	5.1	5.1	14.7	18.3	9.6	-289.6	-29.0	-13.5
194	ok	0.31	9.06e-02	0.0	10.3	10.3	5.1	5.1	90.1	14.6	1.8	479.1	41.9	-2.8
195	ok	0.31	0.2	1.10e-02	10.3	10.3	5.1	5.1	-21.3	-10.7	6.8	850.6	160.7	-19.0
196	ok	0.31	0.2	2.05e-02	10.3	10.3	5.1	5.1	-64.1	-21.9	1.3	1197.8	236.3	-21.8
197	ok	0.31	0.2	2.49e-02	10.3	10.3	5.1	5.1	-80.9	-24.2	-2.1	1365.7	274.7	-17.6
198	ok	0.31	0.3	2.65e-02	10.3	10.3	5.1	5.1	-86.6	-23.1	-2.6	1421.5	288.7	-8.6
199	ok	0.31	0.3	2.66e-02	10.3	10.3	5.1	5.1	-87.0	-20.2	3.0	1409.4	285.4	11.9
200	ok	0.31	0.3	2.65e-02	10.3	10.3	5.1	5.1	-77.9	-16.0	-2.7	1420.6	439.9	34.9
201	ok	0.31	0.2	3.64e-02	10.3	10.3	5.1	5.1	-98.2	-34.3	17.9	1327.5	138.1	124.7
202	ok	0.31	0.2	3.61e-02	10.3	10.3	5.1	5.1	-115.0	-37.2	14.3	1201.8	220.2	-50.6
203	ok	0.31	0.2	3.41e-02	10.3	10.3	5.1	5.1	-109.7	-29.2	11.1	1071.7	255.6	-34.5
204	ok	0.28	0.2	3.37e-02	7.7	7.7	5.1	5.1	-102.7	-24.3	-8.1	766.5	194.5	62.1
205	ok	0.28	0.2	3.15e-02	7.7	7.7	5.1	5.1	-91.1	-27.7	-18.7	701.7	174.6	108.9
206	ok	0.31	0.2	2.76e-02	10.3	10.3	5.1	5.1	-80.2	-31.3	-21.9	693.5	210.6	139.4
207	ok	0.31	0.1	4.12e-02	10.3	10.3	5.1	5.1	-82.0	-44.8	-17.4	545.8	-124.2	41.3
208	ok	0.31	9.47e-02	1.64e-02	10.3	10.3	5.1	5.1	-8.3	-17.6	-18.3	527.0	153.0	-9.3
209	ok	0.31	3.67e-02	0.0	10.3	10.3	5.1	5.1	56.9	16.9	-3.6	200.2	37.1	1.4
252	ok	0.28	9.10e-02	7.38e-03	7.7	7.7	5.1	5.1	4.8	-13.8	-14.3	107.1	283.2	61.8
253	ok	0.28	5.61e-02	9.96e-03	7.7	7.7	5.1	5.1	-15.5	3.2	18.9	155.5	-8.7	147.1
254	ok	0.28	6.19e-02	1.92e-02	7.7	7.7	5.1	5.1	-54.1	-2.3	8.9	188.9	-19.0	65.5
255	ok	0.28	7.11e-02	2.55e-02	7.7	7.7	5.1	5.1	-74.7	-4.7	3.1	213.8	22.2	28.3
256	ok	0.28	7.72e-02	2.84e-02	7.7	7.7	5.1	5.1	-84.2	-6.5	1.0	230.3	45.8	11.3
257	ok	0.28	8.09e-02	2.93e-02	7.7	7.7	5.1	5.1	-89.6	-9.1	-1.5	241.6	62.4	9.0
258	ok	0.28	8.22e-02	2.93e-02	7.7	7.7	5.1	5.1	-88.5	-14.7	9.8	244.5	148.9	13.7

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

259	ok	0.28	6.60e-02	3.04e-02	7.7	7.7	5.1	5.1	-90.5	-7.7	5.9	135.4	51.5	-64.7
260	ok	0.28	0.2	3.47e-02	7.7	7.7	5.1	5.1	-103.4	-25.1	15.9	-224.3	-617.2	-1.7
261	ok	0.28	6.66e-02	3.30e-02	7.7	7.7	5.1	5.1	-100.0	-24.8	2.9	-117.4	-152.3	38.5
262	ok	0.28	6.05e-02	3.26e-02	7.7	7.7	5.1	5.1	-97.4	-22.9	1.8	121.9	76.5	14.5
263	ok	0.28	7.69e-02	3.02e-02	7.7	7.7	5.1	5.1	-91.7	-21.3	-8.7	216.2	181.7	-7.6
264	ok	0.28	5.23e-02	2.74e-02	7.7	7.7	5.1	5.1	-81.3	-22.2	-13.0	92.8	74.9	12.6
265	ok	0.28	3.93e-02	2.62e-02	7.7	7.7	5.1	5.1	-72.2	-22.0	-14.4	34.2	-47.4	-32.1
266	ok	0.28	0.2	2.39e-02	7.7	7.7	5.1	5.1	-54.9	-17.5	-30.7	-241.9	-504.0	-49.3
267	ok	0.28	6.29e-02	2.52e-02	7.7	7.7	5.1	5.1	-45.8	-7.0	-45.5	-153.2	-78.4	-23.0
268	ok	0.28	9.11e-02	9.09e-03	7.7	7.7	5.1	5.1	-1.2	-14.9	-11.7	42.8	297.6	17.8
311	ok	0.28	0.2	1.40e-02	7.7	7.7	5.1	5.1	-31.8	-24.2	-13.4	62.0	529.9	38.6
312	ok	0.28	6.67e-02	8.55e-03	7.7	7.7	5.1	5.1	-14.9	-22.7	2.3	-156.4	-62.0	136.5
313	ok	0.28	9.50e-02	1.56e-02	7.7	7.7	5.1	5.1	-46.1	-1.1	5.7	-184.0	-150.2	30.1
314	ok	0.28	9.90e-02	2.32e-02	7.7	7.7	5.1	5.1	-71.3	2.6	1.3	-262.3	-101.7	4.9
315	ok	0.28	1.00e-01	2.75e-02	7.7	7.7	5.1	5.1	-81.7	2.6	2.7	-287.0	-55.7	7.1
316	ok	0.28	9.44e-02	2.92e-02	7.7	7.7	5.1	5.1	-86.9	1.3	4.3	-278.4	-44.3	24.2
317	ok	0.28	8.39e-02	2.97e-02	7.7	7.7	5.1	5.1	-90.4	-0.3	7.5	-239.6	-53.9	-16.8
318	ok	0.28	6.77e-02	2.74e-02	7.7	7.7	5.1	5.1	-83.8	-0.1	5.1	-131.9	-45.5	-48.9
319	ok	0.28	0.1	2.68e-02	7.7	7.7	5.1	5.1	-82.1	-22.7	3.6	-127.7	-220.4	-4.7
320	ok	0.28	5.89e-02	2.81e-02	7.7	7.7	5.1	5.1	-85.9	-19.1	-0.5	-111.5	-144.3	32.5
321	ok	0.28	5.69e-02	2.95e-02	7.7	7.7	5.1	5.1	-90.3	-16.6	-4.9	-106.6	-47.4	42.0
322	ok	0.28	5.24e-02	2.84e-02	7.7	7.7	5.1	5.1	-86.3	-13.7	-8.1	-97.9	89.0	-8.9
323	ok	0.28	5.23e-02	2.45e-02	7.7	7.7	5.1	5.1	-74.3	-16.5	-6.6	-100.0	-26.8	-42.1
324	ok	0.28	5.81e-02	2.19e-02	7.7	7.7	5.1	5.1	-65.4	-19.7	-6.6	-98.2	-118.8	-50.4
325	ok	0.28	9.81e-02	1.74e-02	7.7	7.7	5.1	5.1	-44.8	-25.9	-14.2	-100.0	-304.8	-29.6
326	ok	0.28	3.27e-02	1.58e-02	7.7	7.7	5.1	5.1	-27.0	-12.6	-19.9	-26.9	-59.3	-19.1
327	ok	0.28	0.2	1.30e-02	7.7	7.7	5.1	5.1	-17.8	-27.8	-14.6	98.4	527.8	35.3
370	ok	0.28	0.2	1.37e-02	7.7	7.7	5.1	5.1	-40.3	-22.3	-4.9	51.8	558.7	3.6
371	ok	0.28	5.12e-02	9.47e-03	7.7	7.7	5.1	5.1	-15.5	-22.9	-3.8	-175.4	-59.4	-27.6
372	ok	0.28	8.57e-02	1.40e-02	7.7	7.7	5.1	5.1	-39.9	-7.65e-02	-3.2	-169.8	-159.0	-91.3
373	ok	0.28	0.1	2.21e-02	7.7	7.7	5.1	5.1	-65.5	5.1	-1.3	-255.2	-83.7	-65.1
374	ok	0.28	0.1	2.71e-02	7.7	7.7	5.1	5.1	-80.8	6.4	0.7	-292.1	-12.8	-15.5
375	ok	0.28	0.1	2.92e-02	7.7	7.7	5.1	5.1	-86.5	5.1	6.1	-297.7	-6.6	51.6
376	ok	0.28	8.99e-02	2.90e-02	7.7	7.7	5.1	5.1	-85.4	3.2	7.8	-240.4	-85.4	106.8
377	ok	0.28	6.95e-02	2.61e-02	7.7	7.7	5.1	5.1	-75.7	0.9	7.0	-101.7	-58.3	65.2
378	ok	0.28	0.1	2.55e-02	7.7	7.7	5.1	5.1	-74.6	-18.0	-13.9	-88.8	-145.6	25.8
379	ok	0.28	5.02e-02	2.75e-02	7.7	7.7	5.1	5.1	-79.5	-13.9	-12.2	-87.0	-117.8	-2.1
380	ok	0.28	5.39e-02	2.89e-02	7.7	7.7	5.1	5.1	-83.0	-10.4	-11.1	-96.3	-61.8	-13.3
381	ok	0.28	5.66e-02	2.85e-02	7.7	7.7	5.1	5.1	-84.1	-6.3	-6.5	-123.8	49.6	-6.8
382	ok	0.28	4.98e-02	2.42e-02	7.7	7.7	5.1	5.1	-70.7	-9.7	0.8	-108.6	-36.2	14.0
383	ok	0.28	4.68e-02	2.11e-02	7.7	7.7	5.1	5.1	-62.1	-13.0	3.6	-95.1	-107.7	21.4
384	ok	0.28	7.81e-02	1.44e-02	7.7	7.7	5.1	5.1	-41.1	-22.6	7.6	-72.3	-237.8	23.1
385	ok	0.28	2.56e-02	1.12e-02	7.7	7.7	5.1	5.1	-27.5	-11.5	-7.5	-19.1	-43.5	14.0
386	ok	0.28	0.2	1.18e-02	7.7	7.7	5.1	5.1	-16.3	-28.4	-6.3	120.4	583.5	-9.3
429	ok	0.28	0.1	9.66e-03	7.7	7.7	5.1	5.1	-27.4	-14.6	5.5	53.2	409.9	-28.6
430	ok	0.28	6.11e-02	8.87e-03	7.7	7.7	5.1	5.1	-8.2	6.2	-13.4	125.1	-115.7	-131.6
431	ok	0.28	8.24e-02	1.49e-02	7.7	7.7	5.1	5.1	-44.4	1.5	-8.3	105.6	-75.6	-148.7
432	ok	0.28	7.69e-02	2.24e-02	7.7	7.7	5.1	5.1	-68.7	3.7	-1.2	138.7	62.2	-89.3
433	ok	0.28	7.62e-02	2.75e-02	7.7	7.7	5.1	5.1	-84.3	4.3	3.3	159.2	150.4	-33.4
434	ok	0.28	7.08e-02	2.97e-02	7.7	7.7	5.1	5.1	-90.3	3.1	8.3	126.1	175.2	37.5
435	ok	0.28	7.07e-02	2.85e-02	7.7	7.7	5.1	5.1	-85.7	-1.4	11.3	52.9	58.5	144.9
436	ok	0.28	8.56e-02	2.59e-02	7.7	7.7	5.1	5.1	-75.5	-4.9	9.4	-64.1	-233.9	111.1
437	ok	0.28	0.1	2.79e-02	7.7	7.7	5.1	5.1	-75.8	-16.0	-25.5	-84.7	-361.8	20.4
438	ok	0.28	7.39e-02	2.96e-02	7.7	7.7	5.1	5.1	-81.4	-12.0	-22.4	-68.4	-206.4	-45.6
439	ok	0.28	5.77e-02	3.11e-02	7.7	7.7	5.1	5.1	-87.0	-6.5	-19.4	-60.2	-68.9	-62.7
440	ok	0.28	4.52e-02	3.18e-02	7.7	7.7	5.1	5.1	-94.2	-0.4	-7.5	-46.1	154.9	-12.9
441	ok	0.28	4.71e-02	2.79e-02	7.7	7.7	5.1	5.1	-83.6	-1.2	6.8	-54.9	48.2	58.2
442	ok	0.28	5.66e-02	2.53e-02	7.7	7.7	5.1	5.1	-72.1	-3.7	14.4	-63.9	-67.2	84.4
443	ok	0.28	0.1	1.89e-02	7.7	7.7	5.1	5.1	-45.2	-11.3	23.6	-90.0	-311.1	66.6
444	ok	0.28	3.26e-02	1.06e-02	7.7	7.7	5.1	5.1	-27.7	-1.9	6.7	-40.0	-76.6	38.5
445	ok	0.28	0.1	8.00e-03	7.7	7.7	5.1	5.1	1.5	-11.1	-5.2	50.0	211.5	-17.3
458	ok	0.28	7.21e-02	8.33e-03	7.7	7.7	5.1	5.1	-14.6	3.1	-8.1	268.2	-118.6	-90.3
459	ok	0.28	0.1	1.54e-02	7.7	7.7	5.1	5.1	-45.5	-1.5	-5.5	550.5	86.4	-83.9
460	ok	0.28	0.2	2.33e-02	7.7	7.7	5.1	5.1	-71.3	-2.1	-4.7	820.7	273.0	-21.8
461	ok	0.28	0.2	2.81e-02	7.7	7.7	5.1	5.1	-86.0	-3.1	4.3	991.2	333.8	-22.4
462	ok	0.28	0.2	3.13e-02	7.7	7.7	5.1	5.1	-93.5	-1.1	7.2	969.9	423.3	-106.1
463	ok	0.28	0.2	2.93e-02	7.7	7.7	5.1	5.1	-86.8	-6.8	15.7	735.0	308.6	9.1
464	ok	0.28	9.51e-02	2.40e-02	7.7	7.7	5.1	5.1	-70.0	-26.0	12.4	308.9	-194.8	-112.4
475	ok	0.28	6.24e-02	3.92e-03	7.7	7.7	5.1	5.1	46.8	8.3	-17.8	127.9	-186.6	-26.6
476	ok	0.28	0.2	2.97e-02	7.7	7.7	5.1	5.1	-72.3	-21.9	-34.7	103.5	-606.4	-42.0
487	ok	0.28	8.37e-02	3.39e-02	7.7	7.7	5.1	5.1	-85.1	-14.0	-31.9	136.5	-247.6	-64.6
489	ok	0.28	8.82e-02	3.55e-02	7.7	7.7	5.1	5.1	-99.3	-10.3	-30.0	265.3	80.6	-64.0
493	ok	0.28	0.1	3.93e-02	7.7	7.7	5.1	5.1	-117.8	-0.9	-11.1	390.6	340.3	9.2
497	ok	0.28	0.1	3.46e-02	7.7	7.7	5.1	5.1	-104.9	-1.1	10.8	332.8	180.0	-16.4
499	ok	0.28	8.15e-02	3.21e-02	7.7	7.7	5.1	5.1	-93.1	3.1	20.2	227.0	80.5	-23.2
503	ok	0.28	0.1	2.54e-02	7.7	7.7	5.1	5.1	-57.1	-0.8	39.0	-125.7	-432.1	-11.0
506	ok	0.28	4.02e-02	1.38e-02	7.7	7.7	5.1	5.1	-37.0	3.0	12.2	-94.7	-63.6	29.7
520	ok	0.28	5.97e-02	2.48e-03	7.7	7.7	5.1	5.1	41.3	9.9	0.1	59.2	2.4	20.3
700	ok	0.28	3.03e-02	3.00e-03	7.7	7.7	5.1	5.1	13.4	-5.2	-8.8	-45.5	-96.8	25.8

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

701	ok	0.28	8.95e-02	8.77e-03	7.7	7.7	5.1	5.1	-21.0	-22.2	-4.3	329.1	-12.2	136.9
702	ok	0.28	0.4	1.36e-02	7.7	7.7	5.1	5.1	-40.8	-17.3	-4.6	1517.1	309.6	380.3
703	ok	0.28	0.5	2.63e-02	7.7	7.7	5.1	5.1	-80.1	-19.7	-6.2	2435.1	557.6	94.6
704	ok	0.28	0.5	2.86e-02	7.7	7.7	5.1	5.1	-86.9	-18.7	8.4	2342.0	507.7	67.8
705	ok	0.28	0.6	3.32e-02	7.7	7.7	5.1	5.1	-100.3	-23.6	10.7	2874.0	685.9	30.8
706	ok	0.28	0.6	3.48e-02	7.7	7.7	5.1	5.1	-101.7	-24.1	13.3	2791.4	634.7	-366.8
707	ok	0.28	0.2	1.11e-02	7.7	7.7	5.1	5.1	-34.0	3.0	2.1	844.9	13.3	-291.9
708	ok	0.28	0.1	2.53e-02	7.7	7.7	5.1	5.1	-62.2	20.5	-16.2	461.9	-28.4	-226.7
709	ok	0.28	0.1	2.78e-02	7.7	7.7	5.1	5.1	-67.7	-7.5	-19.7	545.4	8.2	187.2
710	ok	0.28	0.4	4.93e-02	7.7	7.7	5.1	5.1	-145.7	-30.6	-25.1	1700.4	423.6	224.8
711	ok	0.28	0.4	4.64e-02	7.7	7.7	5.1	5.1	-142.5	-38.5	-2.5	1848.8	492.9	-102.9
712	ok	0.28	0.3	4.14e-02	7.7	7.7	5.1	5.1	-120.9	-34.1	-0.4	1132.4	272.9	-220.2
713	ok	0.28	0.2	4.04e-02	7.7	7.7	5.1	5.1	-122.6	-32.9	11.0	867.8	213.0	-194.7
714	ok	0.28	0.2	3.28e-02	7.7	7.7	5.1	5.1	-81.1	-23.0	3.8	982.5	21.7	-13.5
715	ok	0.28	0.2	1.13e-02	7.7	7.7	5.1	5.1	-28.4	-10.4	-6.0	906.0	198.3	-79.8
716	ok	0.28	4.69e-02	0.0	7.7	7.7	5.1	5.1	51.2	8.8	-10.2	208.4	-6.7	-13.4

Nodo	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
	0.31	0.58	0.05	10.26	10.26	5.13	5.13	-145.72	-44.79	-45.50	-365.89	-617.23	-366.81
								90.10	20.53	38.95	2874.04	685.94	380.28

Nodo	Stato	Max tau daN/cm2	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr daN/cm	V sec daN/cm
1	ok	2.05						
2	ok	1.37						
3	ok	1.48						
4	ok	1.10						
5	ok	0.94						
6	ok	0.74						
7	ok	0.71						
194	ok	1.28						
195	ok	1.36						
196	ok	2.29						
197	ok	2.55						
198	ok	2.56						
199	ok	2.28						
200	ok	2.32						
201	ok Av	8.52	0.31	0.19	8.9	5.5	107.2	65.9
202	ok	4.84						
203	ok	2.72						
204	ok	1.02						
205	ok	1.47						
206	ok	2.23						
207	ok	4.63						
208	ok	1.73						
209	ok	0.56						
252	ok	0.91						
253	ok	2.25						
254	ok	2.40						
255	ok	2.60						
256	ok	2.62						
257	ok	2.57						
258	ok	2.89						
259	ok	2.61						
260	ok	3.48						
261	ok	2.08						
262	ok	1.44						
263	ok	1.04						
264	ok	1.13						
265	ok	1.57						
266	ok	2.43						
267	ok	1.48						
268	ok	0.47						
311	ok	1.53						
312	ok	1.69						
313	ok	1.25						
314	ok	1.24						
315	ok	1.25						
316	ok	1.33						
317	ok	1.52						
318	ok	1.86						
319	ok	1.53						
320	ok	0.43						
321	ok	0.40						
322	ok	0.32						
323	ok	0.40						
324	ok	0.46						
325	ok	0.58						

SCARICATORE IN VIA PUCCI

326	ok	1.26										
327	ok	1.14										
370	ok	1.50										
371	ok	1.57										
372	ok	1.08										
373	ok	1.03										
374	ok	1.09										
375	ok	1.04										
376	ok	1.26										
377	ok	1.84										
378	ok	1.67										
379	ok	0.25										
380	ok	0.24										
381	ok	0.10										
382	ok	0.25										
383	ok	0.33										
384	ok	0.36										
385	ok	1.09										
386	ok	1.18										
429	ok	1.16										
430	ok	1.26										
431	ok	1.37										
432	ok	1.62										
433	ok	1.76										
434	ok	1.75										
435	ok	1.67										
436	ok	1.23										
437	ok	1.07										
438	ok	1.01										
439	ok	0.87										
440	ok	0.58										
441	ok	0.66										
442	ok	0.68										
443	ok	0.74										
444	ok	0.94										
445	ok	0.91										
458	ok	1.61										
459	ok	3.52										
460	ok	2.68										
461	ok	2.54										
462	ok	2.91										
463	ok	4.17										
464	ok	4.35										
475	ok	0.91										
476	ok	4.18										
487	ok	3.33										
489	ok	2.92										
493	ok	1.72										
497	ok	2.46										
499	ok	2.49										
503	ok	2.91										
506	ok	0.92										
520	ok	1.01										
700	ok	0.41										
701	ok	1.06										
702	ok	2.51										
703	ok	3.64										
704	ok	2.18										
705	ok	3.62										
706	ok Av	5.47	0.20	0.07	5.9	2.0	70.3	24.2				
707	ok	2.08										
708	ok	3.09										
709	ok	1.08										
710	ok	3.61										
711	ok	3.37										
712	ok	1.67										
713	ok	1.76										
714	ok Av	5.41	0.20	0.07	5.8	2.2	68.9	25.9				
715	ok	3.06										
716	ok	0.82										
Nodo		Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec				
		8.52	0.31	0.19	8.95	5.51	107.16	65.92				

Parete	H totale	Spessore	H critica	H critica V	L totale	L confinata	Verif. N	Verif. N-M	Fattore V	Diagramma V	Verif. V	Prog. composta
	cm	cm	cm	cm	cm	cm						
3	265.00	20.00	40.00	40.00	117.50	30.00	ok	ok	1.50	SI	ok	SI

SCARICATORE IN VIA PUCCI

Quota	Af conf.	Af std Af V (ori)		Ver. N	Ver. N/M	Ver. V cls	Ver. V acc	Ver. V acc(7)	Ver. V scorr.	N add	M invil	V invil		
cm										daN	daN	daN		
-305.0	4d14	14/20	14/30	0.03	0.01	0.12	0.0	0.19	0.13	0.0	7.718e+04	4344.41		
-270.0	4d14	14/20	14/30	0.03	0.01	0.12	0.0	0.18	0.13	0.0	7.718e+04	4344.41		
-231.7	0d0	14/20	14/30	0.03	0.02	0.05	0.0	0.19	0.0	0.0	7.718e+04	4344.41		
-193.3	0d0	14/20	14/30	0.03	0.02	0.05	0.0	0.19	0.0	0.0	7.718e+04	3798.87		
-155.0	0d0	14/20	14/30	0.03	0.02	0.04	0.0	0.18	0.0	0.0	7.670e+04	3478.75		
-116.7	0d0	14/20	14/30	0.02	0.01	0.04	0.0	0.17	0.0	0.0	7.621e+04	3158.62		
-80.0	0d0	14/20	14/30	0.01	0.01	0.03	0.0	0.16	0.0	0.0	7.574e+04	2852.41		
-40.0	0d0	14/20	14/30	5.16e-03	0.01	0.03	0.0	0.15	0.0	0.0	7.522e+04	2518.36		
Quota	Ver. N Ver. N/MVer. V clsVer. V accVer. V acc(7)Ver. V scorr.													
	0.03 0.02 0.12 0.0 0.19 0.13													
Quota	N v.N	N v.M/N	M v.M/N	N v.Vcls	V v.Vcls	N v.Vacc	M v. Vacc	V v.Vacc	N v.Vscor	M v.Vscor	V v.Vscor			
cm	daN	daN	daN cm	daN	daN	daN	daN cm	daN	daN	daN cm	daN			
-305.0	-4973.96	-2967.09	5.310e+04	-4973.96	3425.51	0.0	0.0	0.0	-4973.96	3.404e+04	3425.51			
-270.0	-4832.78	-3172.76	5.310e+04	-4832.78	3425.51	0.0	0.0	0.0	-4832.78	3.404e+04	3425.51			
-231.7	-4875.69	-3229.92	5.310e+04	-4875.69	3425.51	0.0	0.0	0.0	0.0	0.0	0.0			
-193.3	-4809.58	-3418.89	5.310e+04	-4809.58	3425.51	0.0	0.0	0.0	0.0	0.0	0.0			
-155.0	-4209.60	-3183.15	4.676e+04	-4209.60	3199.29	0.0	0.0	0.0	0.0	0.0	0.0			
-116.7	-3261.88	-2492.24	4.013e+04	-3261.88	2827.66	0.0	0.0	0.0	0.0	0.0	0.0			
-80.0	-2026.93	-1534.68	3.378e+04	-2018.44	2456.02	0.0	0.0	0.0	0.0	0.0	0.0			
-40.0	-798.61	-789.22	3.212e+04	-795.78	2100.55	0.0	0.0	0.0	0.0	0.0	0.0			
Quota	Ctg Vcls	Vrsd Vcls	Vrcd Vcls	Ctg Vac	Vrsd Vac	Vrcd Vac	Vdd	Vid	[A s.i.	Incli.	Dist.]	Vfd		
cm		daN	daN		daN	daN	daN	daN	cm2	gradi	cm	daN		
-305.0	1.00	3425.51	2.951e+04	0.0	0.0	0.0	1.807e+04	0.0	0.0	0.0	0.0	7781.09		
-270.0	1.00	3425.51	2.950e+04	0.0	0.0	0.0	1.807e+04	0.0	0.0	0.0	0.0	7753.55		
-231.7	1.00	3425.51	7.501e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
-193.3	1.00	3425.51	7.500e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
-155.0	1.00	3199.29	7.488e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
-116.7	1.00	2827.66	7.470e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
-80.0	1.00	2456.02	7.446e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
-40.0	1.00	2100.55	7.423e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
Quota	V[7.4.16]	N	M	V	alfaS	VRd,c	VRd,s	V[7.4.17]	roH	roV	roN			
cm		daN	daN cm	daN		daN	daN							
-305.0	0.19	-4973.96	3.404e+04	3425.51	0.11	1.440e+04	3983.67	0.0	5.13e-03	7.70e-03	0.0			
-270.0	0.18	-4832.78	3.404e+04	3425.51	0.13	1.427e+04	4578.23	0.0	5.13e-03	7.70e-03	0.0			
-231.7	0.19	-4875.69	3.404e+04	3425.51	0.13	1.363e+04	4578.23	0.0	5.13e-03	7.70e-03	0.0			
-193.3	0.19	-4809.58	3.404e+04	3425.51	0.13	1.356e+04	4578.23	0.0	5.13e-03	7.70e-03	0.0			
-155.0	0.18	-4209.60	3.353e+04	3199.29	0.13	1.299e+04	4578.23	0.0	5.13e-03	7.70e-03	0.0			
-116.7	0.17	-3261.88	3.299e+04	2827.66	0.13	1.208e+04	4578.23	0.0	5.13e-03	7.70e-03	0.0			
-80.0	0.16	-2018.44	3.249e+04	2456.02	0.13	1.089e+04	4578.23	0.0	5.13e-03	7.70e-03	0.0			
-40.0	0.15	-795.78	3.193e+04	2100.55	0.13	9720.58	4578.23	0.0	5.13e-03	7.70e-03	0.0			
Quota	V[7.4.16]	V[7.4.17]												
	0.19	0.0												
Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
									daN/cm	daN/cm	daN/cm	daN	daN	daN
1	ok	0.31	2.87e-02	0.0	10.3	10.3	5.1	5.1	27.6	62.1	23.4	-148.8	-72.6	-14.4
8	ok	0.31	5.81e-02	1.88e-02	10.3	10.3	5.1	5.1	-55.2	15.5	-16.7	-174.3	-80.2	29.5
16	ok	0.28	0.1	3.08e-02	7.7	7.7	5.1	5.1	-73.6	-13.1	-11.1	-408.4	-56.5	-6.3
22	ok	0.31	6.34e-02	1.79e-02	10.3	10.3	5.1	5.1	-58.4	-7.8	-2.5	-257.5	-80.6	-23.9
28	ok	0.31	2.43e-02	4.05e-03	10.3	10.3	5.1	5.1	-6.4	4.8	-10.6	-116.2	-53.4	-3.4
201	ok	0.31	0.1	6.03e-02	10.3	10.3	5.1	5.1	-78.8	-119.8	-53.5	10.6	-195.7	37.6
210	ok	0.31	6.10e-02	3.94e-02	10.3	10.3	5.1	5.1	-71.1	-33.1	-42.4	73.9	4.4	62.8
212	ok	0.28	6.32e-02	2.35e-02	7.7	7.7	5.1	5.1	-57.1	-25.4	-15.0	122.1	155.5	28.8
214	ok	0.31	4.73e-02	1.29e-02	10.3	10.3	5.1	5.1	-38.1	-16.8	-7.9	66.3	58.9	-89.8
216	ok	0.31	9.58e-02	1.16e-02	10.3	10.3	5.1	5.1	-25.6	-24.6	1.0	-71.8	-297.0	-13.5
260	ok	0.28	0.1	3.98e-02	7.7	7.7	5.1	5.1	-30.2	6.2	17.3	-24.9	-315.5	-9.4
269	ok	0.28	5.12e-02	3.77e-02	7.7	7.7	5.1	5.1	-81.2	-45.5	17.8	28.1	-48.9	25.7
271	ok	0.28	8.89e-02	1.93e-02	7.7	7.7	5.1	5.1	-43.6	-41.7	1.3	135.6	255.9	13.6
273	ok	0.28	3.49e-02	1.51e-02	7.7	7.7	5.1	5.1	-26.0	-28.4	14.1	52.7	49.7	-16.7
275	ok	0.28	0.1	1.50e-02	7.7	7.7	5.1	5.1	-31.9	-28.2	14.6	-67.0	-434.0	1.0
319	ok	0.28	0.1	2.47e-02	7.7	7.7	5.1	5.1	-73.6	11.3	-5.9	-48.7	-310.1	-5.6
328	ok	0.28	5.46e-02	2.58e-02	7.7	7.7	5.1	5.1	-79.0	3.4	3.5	-5.0	-69.5	-12.0
330	ok	0.28	8.19e-02	1.93e-02	7.7	7.7	5.1	5.1	-55.5	-16.6	3.2	87.7	262.1	-6.1

SCARICATORE IN VIA PUCCI

332	ok	0.28	2.18e-02	1.30e-02	7.7	7.7	5.1	5.1	-32.0	-20.2	9.1	12.0	26.4	15.7
334	ok	0.28	0.1	1.47e-02	7.7	7.7	5.1	5.1	-37.9	-24.1	11.5	-75.5	-411.0	2.9
378	ok	0.28	0.1	2.44e-02	7.7	7.7	5.1	5.1	-70.1	13.4	-16.8	-43.4	-228.3	3.9
387	ok	0.28	6.04e-02	2.50e-02	7.7	7.7	5.1	5.1	-71.3	8.2	-19.2	-9.1	-50.4	-11.2
389	ok	0.28	6.72e-02	1.86e-02	7.7	7.7	5.1	5.1	-50.6	-11.1	-13.0	67.3	219.5	-13.9
391	ok	0.28	2.23e-02	1.19e-02	7.7	7.7	5.1	5.1	-28.5	-18.8	-6.4	18.1	4.8	26.0
393	ok	0.28	0.1	1.24e-02	7.7	7.7	5.1	5.1	-36.7	-19.6	-1.9	-61.9	-325.8	2.4
437	ok	0.28	8.81e-02	3.12e-02	7.7	7.7	5.1	5.1	-76.6	-16.5	-37.6	-3.6	-84.1	-9.6
446	ok	0.28	4.28e-02	2.93e-02	7.7	7.7	5.1	5.1	-64.9	-20.7	-37.3	32.9	42.8	-14.7
448	ok	0.28	5.59e-02	1.66e-02	7.7	7.7	5.1	5.1	-31.0	-25.3	-19.5	61.7	147.4	-14.0
450	ok	0.28	2.26e-02	1.06e-02	7.7	7.7	5.1	5.1	-20.0	-9.2	-12.4	18.6	28.2	20.8
452	ok	0.28	8.34e-02	1.03e-02	7.7	7.7	5.1	5.1	-27.9	-14.3	-7.7	-40.7	-227.3	0.6
476	ok	0.28	7.15e-02	4.59e-02	7.7	7.7	5.1	5.1	-88.8	-98.9	-41.5	-50.9	10.1	-61.0
477	ok	0.28	5.80e-02	3.80e-02	7.7	7.7	5.1	5.1	-46.9	-90.1	-36.5	39.3	58.2	-35.4
478	ok	0.28	3.25e-02	1.12e-02	7.7	7.7	5.1	5.1	-16.8	-27.6	-3.6	-11.3	64.4	4.2
479	ok	0.28	2.35e-02	9.48e-03	7.7	7.7	5.1	5.1	-14.8	-8.5	4.2	-23.8	-15.9	41.4
480	ok	0.28	3.85e-02	6.84e-03	7.7	7.7	5.1	5.1	-13.8	-7.3	-9.5	-18.1	-109.2	2.5
708	ok	0.28	4.55e-02	2.18e-02	7.7	7.7	5.1	5.1	-61.6	6.6	-19.5	-0.3	-55.1	80.8
717	ok	0.28	4.29e-02	1.27e-02	7.7	7.7	5.1	5.1	16.1	15.5	8.8	-198.4	-61.6	-8.7
724	ok	0.28	5.95e-02	9.52e-03	7.7	7.7	5.1	5.1	-15.0	7.7	16.0	-233.2	-26.7	18.5
730	ok	0.28	4.61e-02	8.51e-03	7.7	7.7	5.1	5.1	-18.0	1.5	14.6	-177.8	-50.5	-20.1
736	ok	0.28	1.45e-02	7.77e-04	7.7	7.7	5.1	5.1	0.9	3.7	-0.9	-3.3	0.2	-2.1

Nodo	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
	0.31	0.14	0.06	10.26	10.26	5.13	5.13	-88.78	-119.84	-53.52	-408.39	-433.97	-89.80
								27.61	62.06	23.41	135.63	262.13	80.83

Nodo	Stato	Max tau daN/cm2	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr daN/cm	V sec daN/cm
1	ok	0.46						
8	ok	0.77						
16	ok	1.28						
22	ok	0.72						
28	ok	0.13						
201	ok	1.36						
210	ok	2.16						
212	ok	1.90						
214	ok	2.11						
216	ok	1.03						
260	ok	1.57						
269	ok	2.20						
271	ok	1.19						
273	ok	1.96						
275	ok	1.62						
319	ok	1.60						
328	ok	2.05						
330	ok	1.15						
332	ok	1.77						
334	ok	1.52						
378	ok	1.34						
387	ok	1.65						
389	ok	0.96						
391	ok	1.44						
393	ok	1.22						
437	ok	0.96						
446	ok	1.22						
448	ok	0.72						
450	ok	1.05						
452	ok	0.88						
476	ok	0.53						
477	ok	0.76						
478	ok	0.76						
479	ok	0.69						
480	ok	0.48						
708	ok	0.77						
717	ok	0.56						
724	ok	0.50						
730	ok	0.43						
736	ok	0.17						

Nodo	Max tau 2.20	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
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Parete	H totale	Spessore	H critica	H critica V	L totale	L confinata	Verif. N	Verif. N-M	Fattore V	Diagramma V	Verif. V	Prog. composta
	cm	cm	cm	cm	cm	cm						

SCARICATORE IN VIA PUCCI

Parete	H totale	Spessore	H critica	H critica V	L totale	L confinata	Verif. N	Verif. N-M	Fattore V	Diagramma V	Verif. V	Prog. composta
4	265.00	20.00	40.00	40.00	117.50	30.00	ok	ok	1.50	SI	ok	SI

Quota cm	Af conf.	Af std	Af V (ori)	Ver. N	Ver. N/M	Ver. V cls	Ver. V acc	Ver. V acc(7)	Ver. V scorr.	N add daN	M invil daN	V invil daN
-305.0	4d14	14/20	14/30	0.03	0.01	0.08	0.0	0.13	0.09	0.0	6.385e+04	2912.73
-270.0	4d14	14/20	14/30	0.03	0.01	0.08	0.0	0.13	0.09	0.0	6.385e+04	2912.73
-231.7	0d0	14/20	14/30	0.03	0.01	0.03	0.0	0.13	0.0	0.0	6.385e+04	2842.97
-193.3	0d0	14/20	14/30	0.02	0.01	0.03	0.0	0.13	0.0	0.0	6.028e+04	2659.83
-155.0	0d0	14/20	14/30	0.02	0.01	0.03	0.0	0.13	0.0	0.0	5.655e+04	2358.97
-116.7	0d0	14/20	14/30	0.01	0.01	0.03	0.0	0.12	0.0	0.0	5.282e+04	2058.10
-80.0	0d0	14/20	14/30	8.67e-03	0.01	0.02	0.0	0.11	0.0	0.0	4.926e+04	1770.32
-79.8	0d0	14/20	14/30	8.30e-03	0.01	0.02	0.0	0.09	0.0	0.0	4.923e+04	1768.36
-79.4	0d0	14/20	14/30	7.68e-03	0.01	0.02	0.0	0.09	0.0	0.0	4.919e+04	1765.23
-79.0	0d0	14/20	14/30	6.50e-03	0.01	0.02	0.0	0.09	0.0	0.0	4.915e+04	1762.10
-78.8	0d0	14/20	14/30	6.71e-03	0.01	0.02	0.0	0.09	0.0	0.0	4.914e+04	1761.12
-40.0	0d0	14/20	14/30	1.51e-03	0.01	0.02	0.0	0.10	0.0	0.0	4.536e+04	1456.37

Quota	Ver. N	Ver. N/M	Ver. V cls	Ver. V acc	Ver. V acc(7)	Ver. V scorr.
	0.03	0.01	0.08	0.0	0.13	0.09

Quota cm	N v.N daN	N v.M/N daN	M v.M/N daN cm	N v.Vcls daN	V v.Vcls daN	N v.Vacc daN	M v. Vacc daN cm	V v.Vacc daN	N v.Vscor daN	M v.Vscor daN cm	V v.Vscor daN
-305.0	-4576.58	-2886.54	4.279e+04	-4208.94	2415.91	0.0	0.0	0.0	-4208.94	4.116e+04	2415.91
-270.0	-4539.33	-2933.73	4.279e+04	-4189.23	2415.91	0.0	0.0	0.0	-4189.23	4.116e+04	2415.91
-231.7	-3953.04	-2636.45	4.279e+04	-3685.35	2415.91	0.0	0.0	0.0	0.0	0.0	0.0
-193.3	-3577.40	-2973.66	3.908e+04	-3424.30	2415.91	0.0	0.0	0.0	0.0	0.0	0.0
-155.0	-2953.63	-2767.77	3.635e+04	-2888.22	2256.37	0.0	0.0	0.0	0.0	0.0	0.0
-116.7	-2286.57	-2156.81	3.413e+04	-2185.97	1994.27	0.0	0.0	0.0	0.0	0.0	0.0
-80.0	-1341.87	-1294.70	3.200e+04	-1177.11	1732.17	0.0	0.0	0.0	0.0	0.0	0.0
-79.8	-1284.32	-1263.33	3.199e+04	-1150.32	1481.46	0.0	0.0	0.0	0.0	0.0	0.0
-79.4	-1188.38	-1176.90	3.196e+04	-1084.63	1479.75	0.0	0.0	0.0	0.0	0.0	0.0
-79.0	-1005.64	-994.01	3.194e+04	-945.16	1477.03	0.0	0.0	0.0	0.0	0.0	0.0
-78.8	-1038.02	-1022.93	3.193e+04	-990.00	1474.30	0.0	0.0	0.0	0.0	0.0	0.0
-40.0	-233.38	-178.34	2.968e+04	-92.89	1473.45	0.0	0.0	0.0	0.0	0.0	0.0

Quota cm	Ctg Vcls	Vrsd Vcls daN	Vrcd Vcls daN	Ctg Vac	Vrsd Vac daN	Vrcd Vac daN	Vdd daN	Vid daN	[A s.i. cm2	Incli. gradi	Dist.] cm	Vfd daN
-305.0	1.00	2415.91	2.946e+04	0.0	0.0	0.0	1.807e+04	0.0	0.0	0.0	0.0	7678.19
-270.0	1.00	2415.91	2.945e+04	0.0	0.0	0.0	1.807e+04	0.0	0.0	0.0	0.0	7673.56
-231.7	1.00	2415.91	7.478e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-193.3	1.00	2415.91	7.473e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-155.0	1.00	2256.37	7.463e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-116.7	1.00	1994.27	7.450e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-80.0	1.00	1732.17	7.430e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-79.8	1.00	1481.46	7.430e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-79.4	1.00	1479.75	7.429e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-79.0	1.00	1477.03	7.426e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-78.8	1.00	1474.30	7.427e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-40.0	1.00	1473.45	7.410e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota cm	V[7.4.16]	N daN	M daN cm	V daN	alfaS	VRd,c daN	VRd,s daN	V[7.4.17]	roH	roV	roN
-305.0	0.13	-3307.39	4.283e+04	2344.95	0.16	1.284e+04	5757.57	0.0	5.13e-03	7.70e-03	0.0
-270.0	0.13	-3332.33	4.283e+04	2344.95	0.16	1.286e+04	5757.57	0.0	5.13e-03	7.70e-03	0.0
-231.7	0.13	-2978.22	4.283e+04	2344.95	0.16	1.181e+04	5757.57	0.0	5.13e-03	7.70e-03	0.0
-193.3	0.13	-2973.66	3.908e+04	2344.95	0.16	1.181e+04	5757.57	0.0	5.13e-03	7.70e-03	0.0
-155.0	0.13	-2888.22	3.534e+04	2256.37	0.17	1.172e+04	6011.24	0.0	5.13e-03	7.70e-03	0.0
-116.7	0.12	-2185.97	3.236e+04	1994.27	0.17	1.105e+04	6011.24	0.0	5.13e-03	7.70e-03	0.0
-80.0	0.11	-1177.11	2.952e+04	1732.17	0.17	1.009e+04	6011.24	0.0	5.13e-03	7.70e-03	0.0
-79.8	0.09	-1150.32	2.950e+04	1481.46	0.17	1.006e+04	6011.24	0.0	5.13e-03	7.70e-03	0.0
-79.4	0.09	-1084.63	2.947e+04	1479.75	0.17	9997.14	6011.24	0.0	5.13e-03	7.70e-03	0.0
-79.0	0.09	-945.16	2.943e+04	1477.03	0.17	9863.61	6011.24	0.0	5.13e-03	7.70e-03	0.0
-78.8	0.09	-990.00	2.943e+04	1474.30	0.17	9906.54	6011.24	0.0	5.13e-03	7.70e-03	0.0
-40.0	0.10	-92.89	2.641e+04	1473.45	0.17	9047.61	6011.24	0.0	5.13e-03	7.70e-03	0.0

Quota	V[7.4.16]	V[7.4.17]
	0.13	0.0

Nodo	Stato	x/d	V N/M	ver. rid	Af pr- Af pr+Af sec-Af sec+	N z	N o	N zo	M z	M o	M zo
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SCARICATORE IN VIA PUCCI

									daN/cm	daN/cm	daN/cm	daN	daN	daN
7	ok	0.31	8.91e-02	0.0	10.3	10.3	5.1	5.1	27.4	48.5	28.8	380.2	46.3	166.6
15	ok	0.31	6.13e-02	2.69e-02	10.3	10.3	5.1	5.1	-76.4	12.9	-32.6	200.0	63.7	-67.2
21	ok	0.28	0.1	2.78e-02	7.7	7.7	5.1	5.1	-66.1	-18.8	-34.3	427.3	77.7	-14.6
27	ok	0.31	6.56e-02	1.66e-02	10.3	10.3	5.1	5.1	-52.9	-7.1	3.8	276.1	83.3	25.3
33	ok	0.31	2.70e-02	3.78e-03	10.3	10.3	5.1	5.1	0.5	4.9	-14.3	143.1	56.5	0.3
207	ok	0.31	0.2	5.43e-02	10.3	10.3	5.1	5.1	-95.6	-110.3	-8.3	448.6	206.7	-270.8
211	ok	0.31	5.94e-02	3.32e-02	10.3	10.3	5.1	5.1	-50.6	-81.6	-12.1	-125.2	67.2	-41.9
213	ok	0.28	5.67e-02	2.02e-02	7.7	7.7	5.1	5.1	-44.6	-25.3	-7.5	-98.7	-135.0	-40.6
215	ok	0.31	4.22e-02	1.14e-02	10.3	10.3	5.1	5.1	-33.5	-15.9	-7.2	-61.3	-61.3	80.3
221	ok	0.31	8.89e-02	1.09e-02	10.3	10.3	5.1	5.1	-21.7	-19.8	-12.8	61.2	283.1	4.4
266	ok	0.28	0.1	1.79e-02	7.7	7.7	5.1	5.1	-52.6	-8.1	-3.3	-95.0	315.1	132.8
270	ok	0.28	6.10e-02	2.16e-02	7.7	7.7	5.1	5.1	-64.2	-23.9	9.2	90.8	91.8	-76.4
272	ok	0.28	8.79e-02	1.33e-02	7.7	7.7	5.1	5.1	-39.0	-33.3	2.9	-124.6	-260.3	-18.8
274	ok	0.28	3.07e-02	1.18e-02	7.7	7.7	5.1	5.1	-23.9	-26.7	1.3	-51.8	-39.7	32.3
280	ok	0.28	0.1	1.33e-02	7.7	7.7	5.1	5.1	-32.3	-28.4	7.8	69.0	457.0	7.6
325	ok	0.28	7.86e-02	1.40e-02	7.7	7.7	5.1	5.1	-37.9	-2.5	-14.0	44.4	272.3	0.5
329	ok	0.28	2.46e-02	1.54e-02	7.7	7.7	5.1	5.1	-45.7	-5.1	-7.3	21.8	75.9	-8.4
331	ok	0.28	8.39e-02	1.40e-02	7.7	7.7	5.1	5.1	-39.2	-14.9	-4.1	-92.2	-256.0	9.0
333	ok	0.28	2.50e-02	1.21e-02	7.7	7.7	5.1	5.1	-29.1	-22.1	-4.8	-32.7	-35.7	-12.6
339	ok	0.28	0.1	1.23e-02	7.7	7.7	5.1	5.1	-29.8	-25.3	-9.0	74.5	421.5	-6.2
384	ok	0.28	5.94e-02	1.45e-02	7.7	7.7	5.1	5.1	-36.6	-0.7	-18.2	31.5	202.8	8.4
388	ok	0.28	2.97e-02	1.59e-02	7.7	7.7	5.1	5.1	-41.2	-4.3	-16.0	10.2	43.7	25.3
390	ok	0.28	7.16e-02	1.43e-02	7.7	7.7	5.1	5.1	-33.5	-12.4	-14.0	-65.7	-209.1	8.1
392	ok	0.28	2.55e-02	1.17e-02	7.7	7.7	5.1	5.1	-23.7	-17.9	-9.2	-21.0	-28.0	-26.0
398	ok	0.28	0.1	1.09e-02	7.7	7.7	5.1	5.1	-25.4	-21.5	-9.1	76.5	399.3	-6.9
443	ok	0.28	6.73e-02	1.91e-02	7.7	7.7	5.1	5.1	-45.1	-9.9	-24.6	53.3	212.6	8.4
447	ok	0.28	4.55e-02	1.95e-02	7.7	7.7	5.1	5.1	-42.7	-13.1	-24.8	34.7	70.8	40.5
449	ok	0.28	5.46e-02	1.40e-02	7.7	7.7	5.1	5.1	-21.9	-20.5	-20.0	-32.1	-149.0	8.4
451	ok	0.28	2.33e-02	9.64e-03	7.7	7.7	5.1	5.1	-14.2	-15.4	-8.6	-14.7	-26.5	-29.5
457	ok	0.28	8.84e-02	9.27e-03	7.7	7.7	5.1	5.1	-18.0	-15.9	-10.6	54.2	288.8	-6.5
485	ok	0.28	4.52e-02	6.27e-03	7.7	7.7	5.1	5.1	-9.2	-7.6	-10.2	25.9	139.1	-8.6
490	ok	0.28	2.31e-02	7.83e-03	7.7	7.7	5.1	5.1	-6.5	-7.1	-12.0	-17.8	-11.1	-47.4
495	ok	0.28	3.78e-02	1.10e-02	7.7	7.7	5.1	5.1	7.2	-30.0	-2.4	16.8	-78.4	36.9
501	ok	0.28	7.36e-02	3.66e-02	7.7	7.7	5.1	5.1	-28.8	-68.6	-42.4	69.5	93.1	43.5
503	ok	0.28	8.30e-02	3.38e-02	7.7	7.7	5.1	5.1	-62.5	-34.2	-33.0	109.1	228.5	11.3
714	ok	0.28	0.1	3.54e-02	7.7	7.7	5.1	5.1	-73.6	-52.4	-41.6	382.5	49.1	84.8
723	ok	0.28	3.30e-02	8.36e-03	7.7	7.7	5.1	5.1	24.2	-19.3	3.1	114.4	61.5	49.8
729	ok	0.28	2.50e-02	5.98e-03	7.7	7.7	5.1	5.1	-2.2	-4.5	6.8	112.3	9.1	-1.7
735	ok	0.28	3.25e-02	7.03e-03	7.7	7.7	5.1	5.1	-13.9	-2.1	11.1	125.4	30.8	3.2
741	ok	0.28	1.14e-02	1.22e-03	7.7	7.7	5.1	5.1	-0.3	3.7	-0.5	5.3	9.1	1.6

Nodo	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
	0.31	0.15	0.05	10.26	10.26	5.13	5.13	-95.63	-110.25	-42.44	-125.16	-260.35	-270.82
								27.44	48.53	28.85	448.62	456.96	166.64

Nodo	Stato	Max tau daN/cm2	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr daN/cm	V sec daN/cm
7	ok	0.78						
15	ok	1.23						
21	ok	1.35						
27	ok	0.78						
33	ok	0.09						
207	ok	2.79						
211	ok	2.27						
213	ok	2.00						
215	ok	2.15						
221	ok	0.98						
266	ok	2.33						
270	ok	2.39						
272	ok	1.12						
274	ok	1.97						
280	ok	1.62						
325	ok	1.40						
329	ok	1.83						
331	ok	1.03						
333	ok	1.81						
339	ok	1.56						
384	ok	1.06						
388	ok	1.43						
390	ok	0.90						
392	ok	1.48						
398	ok	1.28						
443	ok	0.96						
447	ok	1.32						
449	ok	0.75						
451	ok	1.10						
457	ok	0.95						

SCARICATORE IN VIA PUCCI

485	ok	0.57
490	ok	0.77
495	ok	0.65
501	ok	1.25
503	ok	1.16
714	ok	1.47
723	ok	0.47
729	ok	0.35
735	ok	0.35
741	ok	0.13

Nodo	Max tau 2.79	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
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Parete	H totale	Spessore	H critica	H critica V	L totale	L confinata	Verif. N	Verif. N-M	Fattore V	Diagramma V	Verif. V	Prog. composta
	cm	cm	cm	cm	cm	cm						
5	265.00	20.00	40.00	40.00	130.00	30.00	ok	ok	1.50	SI	ok	SI

Quota cm	Af conf.	Af std	Af V (ori)	Ver. N	Ver. N/M	Ver. V cls	Ver. V acc	Ver. V acc(7)	Ver. V scorr.	N add daN	M invil daN	V invil daN
-305.0	4d14	14/20	14/30	0.03	3.77e-03	0.03	0.0	0.05	0.03	0.0	1.850e+04	1009.65
-270.0	4d14	14/20	14/30	0.03	3.78e-03	0.03	0.0	0.05	0.03	0.0	1.850e+04	1009.65
-231.7	0d0	14/20	14/30	0.02	4.40e-03	0.01	0.0	0.05	0.0	0.0	1.843e+04	1009.65
-193.3	0d0	14/20	14/30	0.02	4.43e-03	0.01	0.0	0.05	0.0	0.0	1.836e+04	917.72
-155.0	0d0	14/20	14/30	0.02	4.47e-03	0.01	0.0	0.05	0.0	0.0	1.829e+04	814.80
-116.7	0d0	14/20	14/30	0.01	3.90e-03	9.85e-03	0.0	0.04	0.0	0.0	1.821e+04	711.88
-80.0	0d0	14/20	14/30	9.96e-03	3.80e-03	8.61e-03	0.0	0.04	0.0	0.0	1.814e+04	613.44
-40.0	0d0	14/20	14/30	7.75e-03	3.72e-03	7.42e-03	0.0	0.03	0.0	0.0	1.807e+04	506.04

Quota	Ver. N	Ver. N/M	Ver. V cls	Ver. V acc	Ver. V acc(7)	Ver. V scorr.
	0.03	4.47e-03	0.03	0.0	0.05	0.03

Quota cm	N v.N daN	N v.M/N daN	M v.M/N daN cm	N v.Vcls daN	V v.Vcls daN	N v.Vacc daN	M v. Vacc daN cm	V v.Vacc daN	N v.Vscor daN	M v.Vscor daN cm	V v.Vscor daN
-305.0	-4881.54	-3451.50	1.850e+04	-2844.20	1009.65	0.0	0.0	0.0	-2844.20	1.701e+04	1009.65
-270.0	-4588.98	-3225.34	1.850e+04	-2649.53	1009.65	0.0	0.0	0.0	-2649.53	1.701e+04	1009.65
-231.7	-4114.55	-3897.56	1.828e+04	-2159.44	1009.65	0.0	0.0	0.0	0.0	0.0	0.0
-193.3	-3579.30	-3248.26	1.828e+04	-2191.77	980.37	0.0	0.0	0.0	0.0	0.0	0.0
-155.0	-2965.83	-2613.26	1.828e+04	-2099.29	917.56	0.0	0.0	0.0	0.0	0.0	0.0
-116.7	-2321.05	-2041.38	1.586e+04	-1732.92	814.38	0.0	0.0	0.0	0.0	0.0	0.0
-80.0	-1704.70	-1452.35	1.536e+04	-1452.35	711.19	0.0	0.0	0.0	0.0	0.0	0.0
-40.0	-1326.04	-1252.46	1.500e+04	-1252.46	612.49	0.0	0.0	0.0	0.0	0.0	0.0

Quota cm	Ctg Vcls	Vrsd Vcls daN	Vrcd Vcls daN	Ctg Vac	Vrsd Vac daN	Vrcd Vac daN	Vdd daN	Vid daN	[A s.i. cm2	Incli. gradi	Dist.] cm	Vfd daN
-305.0	1.00	1009.65	3.265e+04	0.0	0.0	0.0	2.108e+04	0.0	0.0	0.0	0.0	8796.84
-270.0	1.00	1009.65	3.263e+04	0.0	0.0	0.0	2.108e+04	0.0	0.0	0.0	0.0	8755.93
-231.7	1.00	1009.65	8.272e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-193.3	1.00	980.37	8.273e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-155.0	1.00	917.56	8.271e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-116.7	1.00	814.38	8.264e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-80.0	1.00	711.19	8.259e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-40.0	1.00	612.49	8.255e+04	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Quota cm	V[7.4.16]	N daN	M daN cm	V daN	alfaS	VRd,c daN	VRd,s daN	V[7.4.17]	roH	roV	roN
-305.0	0.05	-2844.20	1.701e+04	1009.65	0.17	1.335e+04	6503.54	0.0	5.13e-03	7.70e-03	0.0
-270.0	0.05	-2649.53	1.701e+04	1009.65	0.19	1.316e+04	7375.53	0.0	5.13e-03	7.70e-03	0.0
-231.7	0.05	-2159.44	1.671e+04	1009.65	0.19	1.188e+04	7375.53	0.0	5.13e-03	7.70e-03	0.0
-193.3	0.05	-2191.77	1.637e+04	980.37	0.19	1.191e+04	7375.53	0.0	5.13e-03	7.70e-03	0.0
-155.0	0.05	-2099.29	1.603e+04	917.56	0.19	1.182e+04	7375.53	0.0	5.13e-03	7.70e-03	0.0
-116.7	0.04	-1732.92	1.569e+04	814.38	0.19	1.147e+04	7375.53	0.0	5.13e-03	7.70e-03	0.0
-80.0	0.04	-1452.35	1.536e+04	711.19	0.19	1.120e+04	7375.53	0.0	5.13e-03	7.70e-03	0.0
-40.0	0.03	-1252.46	1.500e+04	612.49	0.19	1.101e+04	7375.53	0.0	5.13e-03	7.70e-03	0.0

Quota	V[7.4.16] 0.05	V[7.4.17] 0.0
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Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
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SCARICATORE IN VIA PUCCI

									daN/cm	daN/cm	daN/cm	daN	daN	daN
28	ok	0.31	2.60e-02	2.47e-03	10.3	10.3	5.1	5.1	-3.4	1.9	-6.5	104.2	57.3	-3.7
29	ok	0.31	4.29e-02	1.44e-02	10.3	10.3	5.1	5.1	-40.5	-9.2	14.8	145.2	58.3	33.1
30	ok	0.28	9.34e-02	2.12e-02	7.7	7.7	5.1	5.1	-54.3	-26.6	-8.6	359.0	50.5	7.7
31	ok	0.28	9.16e-02	2.19e-02	7.7	7.7	5.1	5.1	-59.1	-24.5	-17.8	342.0	44.1	-14.9
32	ok	0.31	5.64e-02	1.69e-02	10.3	10.3	5.1	5.1	-47.1	-16.8	-16.3	232.1	40.6	-27.3
33	ok	0.31	2.04e-02	1.41e-03	10.3	10.3	5.1	5.1	0.6	4.0	6.5	104.0	57.7	-3.5
216	ok	0.31	9.45e-02	1.55e-02	10.3	10.3	5.1	5.1	-23.0	-19.8	-2.3	68.5	306.1	-6.5
217	ok	0.31	4.12e-02	1.51e-02	10.3	10.3	5.1	5.1	-31.5	-17.1	22.0	8.8	91.5	88.0
218	ok	0.28	6.65e-02	1.61e-02	7.7	7.7	5.1	5.1	-46.7	-10.8	-0.2	-115.9	-167.9	84.3
219	ok	0.28	6.13e-02	1.62e-02	7.7	7.7	5.1	5.1	-44.4	-8.8	1.3	-126.1	-179.5	-53.0
220	ok	0.31	5.10e-02	1.64e-02	10.3	10.3	5.1	5.1	-34.9	-11.9	-9.1	-60.1	-65.2	-103.1
221	ok	0.31	8.88e-02	1.43e-02	10.3	10.3	5.1	5.1	-20.7	-18.8	-1.0	60.0	281.5	-12.0
275	ok	0.28	0.1	1.55e-02	7.7	7.7	5.1	5.1	-32.6	-27.2	14.5	88.9	473.0	13.4
276	ok	0.28	5.98e-02	1.21e-02	7.7	7.7	5.1	5.1	-31.7	-25.2	3.9	21.3	168.8	21.0
277	ok	0.28	7.36e-02	1.17e-02	7.7	7.7	5.1	5.1	-24.2	-23.5	-2.9	-122.5	-223.3	15.9
278	ok	0.28	7.01e-02	1.23e-02	7.7	7.7	5.1	5.1	-29.1	-21.6	-5.6	-103.7	-209.9	-22.9
279	ok	0.28	3.63e-02	1.27e-02	7.7	7.7	5.1	5.1	-30.1	-23.8	-4.0	-49.7	-62.5	-30.7
280	ok	0.28	0.1	1.48e-02	7.7	7.7	5.1	5.1	-33.4	-26.5	-13.8	70.2	429.5	-4.5
334	ok	0.28	0.1	1.49e-02	7.7	7.7	5.1	5.1	-30.0	-23.6	10.0	97.2	470.2	9.7
335	ok	0.28	6.55e-02	1.21e-02	7.7	7.7	5.1	5.1	-34.7	-24.6	-5.1	2.7	151.5	-14.1
336	ok	0.28	7.26e-02	1.04e-02	7.7	7.7	5.1	5.1	-23.3	-25.3	-3.6	-101.5	-216.5	-16.2
337	ok	0.28	6.54e-02	1.00e-02	7.7	7.7	5.1	5.1	-24.0	-22.2	-2.6	-74.7	-196.2	5.3
338	ok	0.28	2.49e-02	1.03e-02	7.7	7.7	5.1	5.1	-25.8	-22.9	-3.4	-31.1	-37.9	21.2
339	ok	0.28	0.1	1.32e-02	7.7	7.7	5.1	5.1	-29.7	-25.6	2.8	69.8	466.2	5.5
393	ok	0.28	0.1	1.31e-02	7.7	7.7	5.1	5.1	-38.2	-16.5	6.5	36.7	323.8	6.8
394	ok	0.28	5.67e-02	1.10e-02	7.7	7.7	5.1	5.1	-30.1	-19.8	-0.6	-10.3	115.9	-28.5
395	ok	0.28	6.18e-02	8.91e-03	7.7	7.7	5.1	5.1	-21.2	-21.7	-2.3	-81.4	-180.5	-28.0
396	ok	0.28	5.39e-02	9.03e-03	7.7	7.7	5.1	5.1	-18.2	-21.9	-2.7	-67.3	-140.8	16.2
397	ok	0.28	2.30e-02	9.08e-03	7.7	7.7	5.1	5.1	-20.6	-21.7	-3.8	-28.9	2.5	31.3
398	ok	0.28	0.1	1.18e-02	7.7	7.7	5.1	5.1	-24.9	-21.2	-2.0	61.8	397.7	7.0
452	ok	0.28	8.27e-02	1.15e-02	7.7	7.7	5.1	5.1	-27.3	-14.1	2.9	21.0	224.5	-8.6
453	ok	0.28	4.09e-02	9.05e-03	7.7	7.7	5.1	5.1	-23.0	-14.3	3.8	-9.8	77.0	-35.2
454	ok	0.28	4.67e-02	7.33e-03	7.7	7.7	5.1	5.1	-16.4	-15.0	-0.9	-63.6	-130.8	-33.5
455	ok	0.28	3.89e-02	7.28e-03	7.7	7.7	5.1	5.1	-13.4	-15.2	-3.6	-53.4	-99.6	30.2
456	ok	0.28	2.12e-02	7.50e-03	7.7	7.7	5.1	5.1	-14.6	-15.1	-5.1	-22.6	1.0	46.3
457	ok	0.28	8.79e-02	9.97e-03	7.7	7.7	5.1	5.1	-17.5	-15.9	-5.7	45.2	287.0	7.8
480	ok	0.28	3.77e-02	7.98e-03	7.7	7.7	5.1	5.1	-16.0	-6.2	11.9	22.2	114.5	1.2
481	ok	0.28	2.37e-02	5.92e-03	7.7	7.7	5.1	5.1	-10.0	-3.4	-8.9	36.0	53.8	-48.5
482	ok	0.28	2.63e-02	7.44e-03	7.7	7.7	5.1	5.1	-20.8	-4.5	-5.9	27.9	-46.7	-40.9
483	ok	0.28	2.21e-02	6.78e-03	7.7	7.7	5.1	5.1	-19.8	-5.2	2.5	24.0	-50.9	32.3
484	ok	0.28	1.96e-02	5.68e-03	7.7	7.7	5.1	5.1	-16.2	-5.1	3.7	22.4	-10.6	42.3
485	ok	0.28	4.69e-02	7.02e-03	7.7	7.7	5.1	5.1	-11.3	-7.1	-11.6	29.8	150.3	8.0
736	ok	0.28	1.29e-02	1.17e-03	7.7	7.7	5.1	5.1	4.5	3.0	1.0	50.6	13.1	2.6
737	ok	0.28	2.23e-02	5.11e-03	7.7	7.7	5.1	5.1	-7.5	-2.5	4.2	82.2	20.7	10.1
738	ok	0.28	5.77e-02	9.25e-03	7.7	7.7	5.1	5.1	-21.3	-12.3	6.2	236.8	35.5	-1.7
739	ok	0.28	4.54e-02	8.32e-03	7.7	7.7	5.1	5.1	-18.8	-8.2	-10.0	181.1	29.0	-17.8
740	ok	0.28	2.99e-02	5.96e-03	7.7	7.7	5.1	5.1	-14.7	-6.6	-3.9	84.5	14.4	-7.3
741	ok	0.28	1.23e-02	1.59e-03	7.7	7.7	5.1	5.1	1.5	1.6	-2.6	25.4	12.8	-1.9

Nodo	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
	0.31	0.14	0.02	10.26	10.26	5.13	5.13	-59.08	-27.24	-17.85	-126.10	-223.27	-103.14
								4.55	3.99	21.98	358.96	472.98	88.05

Nodo	Stato	Max tau daN/cm2	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr daN/cm	V sec daN/cm
28	ok	0.46						
29	ok	0.79						
30	ok	1.14						
31	ok	1.14						
32	ok	0.80						
33	ok	0.27						
216	ok	1.50						
217	ok	2.00						
218	ok	2.23						
219	ok	2.26						
220	ok	1.90						
221	ok	1.13						
275	ok	1.89						
276	ok	2.17						
277	ok	1.63						
278	ok	1.75						
279	ok	1.77						
280	ok	1.67						
334	ok	1.74						
335	ok	1.93						
336	ok	1.53						
337	ok	1.63						

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338	ok	1.66
339	ok	1.59
393	ok	1.40
394	ok	1.55
395	ok	1.27
396	ok	1.35
397	ok	1.38
398	ok	1.31
452	ok	1.04
453	ok	1.11
454	ok	0.96
455	ok	1.04
456	ok	1.01
457	ok	0.98
480	ok	0.61
481	ok	0.67
482	ok	0.77
483	ok	0.80
484	ok	0.71
485	ok	0.58
736	ok	0.17
737	ok	0.30
738	ok	0.48
739	ok	0.41
740	ok	0.36
741	ok	0.17

Nodo	Max tau 2.26	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
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Parete	H totale	Spessore	H critica	H critica V	L totale	L confinata	Verif. N	Verif. N-M	Fattore V	Diagramma V	Verif. V	Prog. composta
	cm	cm	cm	cm	cm	cm						
7	230.00	20.00	40.00	40.00	465.00	93.00	ok	ok	1.50	SI	ok	SI

Quota cm	Af conf.	Af std	Af V (ori)	Ver. N	Ver. N/M	Ver. V cls	Ver. V acc	Ver. V acc(7)	Ver. V scorr.	N add daN	M invil daN	V invil daN
-270.0	14d14	14/20	14/30	0.04	8.21e-03	0.07	6.66e-03	0.11	0.07	0.0	5.617e+05	8525.69
-231.7	14d14	14/20	14/30	0.04	6.51e-03	0.07	5.48e-03	0.11	0.07	0.0	5.617e+05	8525.69
-193.3	0d0	14/20	14/30	0.04	5.35e-03	0.03	4.32e-03	0.11	0.0	0.0	5.008e+05	8233.48
-155.0	0d0	14/20	14/30	0.04	3.32e-03	0.02	4.21e-03	0.11	0.0	0.0	4.371e+05	7599.71
-116.7	0d0	14/20	14/30	0.03	3.00e-03	0.02	3.54e-03	0.10	0.0	0.0	3.735e+05	6965.95
-80.0	0d0	14/20	14/30	0.03	3.77e-03	0.02	2.38e-03	0.09	0.0	0.0	3.126e+05	6359.74
-79.9	0d0	14/20	14/30	0.03	3.64e-03	0.02	3.41e-03	0.09	0.0	0.0	3.124e+05	6357.50
-79.7	0d0	14/20	14/30	0.03	3.82e-03	0.02	3.17e-03	0.09	0.0	0.0	3.122e+05	6355.25
-79.6	0d0	14/20	14/30	0.03	3.97e-03	0.02	3.05e-03	0.09	0.0	0.0	3.119e+05	6353.00
-79.5	0d0	14/20	14/30	0.03	4.10e-03	0.02	3.05e-03	0.09	0.0	0.0	3.117e+05	6350.75
-79.3	0d0	14/20	14/30	0.03	4.19e-03	0.02	3.13e-03	0.09	0.0	0.0	3.115e+05	6348.51
-79.2	0d0	14/20	14/30	0.03	4.22e-03	0.02	3.30e-03	0.09	0.0	0.0	3.113e+05	6346.26
-79.0	0d0	14/20	14/30	0.03	4.19e-03	0.02	3.51e-03	0.09	0.0	0.0	3.110e+05	6343.91
-79.0	0d0	14/20	14/30	0.03	4.14e-03	0.02	3.76e-03	0.09	0.0	0.0	3.109e+05	6342.41
-78.9	0d0	14/20	14/30	0.03	4.08e-03	0.02	3.95e-03	0.09	0.0	0.0	3.108e+05	6341.57
-78.8	0d0	14/20	14/30	0.03	3.89e-03	0.02	4.48e-03	0.09	0.0	0.0	3.106e+05	6339.22
-78.7	0d0	14/20	14/30	0.03	3.74e-03	0.02	4.75e-03	0.09	0.0	0.0	3.104e+05	6337.67
-78.5	0d0	14/20	14/30	0.03	3.45e-03	0.02	5.19e-03	0.09	0.0	0.0	3.102e+05	6335.44
-78.5	0d0	14/20	14/30	0.03	3.30e-03	0.02	5.36e-03	0.09	0.0	0.0	3.101e+05	6334.53
-78.3	0d0	14/20	14/30	0.03	2.76e-03	0.02	5.63e-03	0.08	0.0	0.0	3.098e+05	6332.19
-40.0	0d0	14/20	14/30	0.03	2.31e-03	0.02	5.48e-03	0.09	0.0	0.0	2.462e+05	5698.43

Quota	Ver. N	Ver. N/M	Ver. V cls	Ver. V acc	Ver. V acc(7)	Ver. V scorr.
	0.04	8.21e-03	0.07	6.66e-03	0.11	0.07

Quota cm	N v.N daN	N v.M/N daN	M v.M/N daN	N v.Vcls daN	V v.Vcls daN	N v.Vacc daN	M v. Vacc daN	V v.Vacc daN	N v.Vscor daN	M v.Vscor daN	V v.Vscor daN
-270.0	-2.605e+04	-2.314e+04	5.617e+05	-2.150e+04	8352.35	-2.371e+04	5.592e+04	980.11	-2.150e+04	5.410e+05	8352.35
-231.7	-2.553e+04	-2.283e+04	4.450e+05	-2.112e+04	8525.69	-2.353e+04	1.984e+04	806.77	-2.112e+04	4.213e+05	8525.69
-193.3	-2.368e+04	-2.021e+04	3.124e+05	-2.018e+04	8233.48	-2.207e+04	4.208e+04	638.19	0.0	0.0	0.0
-155.0	-2.159e+04	-1.911e+04	1.933e+05	-1.910e+04	7660.79	-2.043e+04	1.049e+05	621.91	0.0	0.0	0.0
-116.7	-1.950e+04	-1.946e+04	1.746e+05	-1.784e+04	6942.05	-1.878e+04	1.615e+05	523.19	0.0	0.0	0.0
-80.0	-1.791e+04	-1.718e+04	2.185e+05	-1.724e+04	6266.61	-1.683e+04	1.557e+05	351.69	0.0	0.0	0.0
-79.9	-1.793e+04	-1.722e+04	2.109e+05	-1.711e+04	6249.44	-1.681e+04	1.602e+05	504.00	0.0	0.0	0.0
-79.7	-1.788e+04	-1.716e+04	2.211e+05	-1.707e+04	6151.69	-1.678e+04	1.645e+05	468.08	0.0	0.0	0.0
-79.6	-1.775e+04	-1.709e+04	2.297e+05	-1.699e+04	6078.43	-1.676e+04	1.677e+05	450.81	0.0	0.0	0.0

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-79.5	-1.767e+04	-1.748e+04	2.379e+05	-1.690e+04	6019.55	-1.672e+04	1.712e+05	450.24	0.0	0.0	0.0
-79.3	-1.758e+04	-1.739e+04	2.431e+05	-1.682e+04	5969.90	-1.667e+04	1.737e+05	463.24	0.0	0.0	0.0
-79.2	-1.749e+04	-1.730e+04	2.449e+05	-1.675e+04	5925.93	-1.661e+04	1.748e+05	487.17	0.0	0.0	0.0
-79.0	-1.739e+04	-1.720e+04	2.430e+05	-1.668e+04	5883.37	-1.721e+04	1.693e+05	518.77	0.0	0.0	0.0
-79.0	-1.733e+04	-1.714e+04	2.399e+05	-1.666e+04	5873.24	-1.649e+04	1.711e+05	555.46	0.0	0.0	0.0
-78.9	-1.727e+04	-1.708e+04	2.361e+05	-1.663e+04	5874.96	-1.645e+04	1.678e+05	584.44	0.0	0.0	0.0
-78.8	-1.717e+04	-1.698e+04	2.254e+05	-1.660e+04	5882.94	-1.636e+04	1.594e+05	662.52	0.0	0.0	0.0
-78.7	-1.710e+04	-1.691e+04	2.163e+05	-1.658e+04	5873.01	-1.631e+04	1.523e+05	701.37	0.0	0.0	0.0
-78.5	-1.700e+04	-1.680e+04	1.995e+05	-1.655e+04	5848.77	-1.623e+04	1.385e+05	766.72	0.0	0.0	0.0
-78.5	-1.696e+04	-1.676e+04	1.911e+05	-1.654e+04	5829.35	-1.619e+04	1.314e+05	792.28	0.0	0.0	0.0
-78.3	-1.680e+04	-1.627e+04	1.595e+05	-1.645e+04	5718.59	-1.609e+04	1.095e+05	831.52	0.0	0.0	0.0
-40.0	-1.709e+04	-1.681e+04	1.339e+05	-1.681e+04	5698.43	-1.641e+04	3.910e+04	809.76	0.0	0.0	0.0

Quota cm	Ctg VcIs	Vrds VcIs daN	Vrds VcIs daN	Ctg Vac	Vrds Vac daN	Vrds Vac daN	Vdd daN	Vid daN	[A s.i. cm2	Incli. gradi	Dist.] cm	Vfd daN
-270.0	1.00	8352.35	1.224e+05	1.00	1.472e+05	1.225e+05	8.132e+04	4176.17	1.2	26.3	0.0	3.661e+04
-231.7	1.00	8525.69	1.223e+05	1.00	1.472e+05	1.225e+05	8.132e+04	4262.84	1.2	26.3	0.0	3.633e+04
-193.3	1.00	8233.48	3.069e+05	1.00	1.478e+05	3.073e+05	0.0	0.0	0.0	0.0	0.0	0.0
-155.0	1.00	7660.79	3.067e+05	1.00	1.478e+05	3.069e+05	0.0	0.0	0.0	0.0	0.0	0.0
-116.7	1.00	6942.05	3.064e+05	1.00	1.478e+05	3.066e+05	0.0	0.0	0.0	0.0	0.0	0.0
-80.0	1.00	6266.61	3.063e+05	1.00	1.478e+05	3.062e+05	0.0	0.0	0.0	0.0	0.0	0.0
-79.9	1.00	6249.44	3.063e+05	1.00	1.478e+05	3.062e+05	0.0	0.0	0.0	0.0	0.0	0.0
-79.7	1.00	6151.69	3.063e+05	1.00	1.478e+05	3.062e+05	0.0	0.0	0.0	0.0	0.0	0.0
-79.6	1.00	6078.43	3.063e+05	1.00	1.478e+05	3.062e+05	0.0	0.0	0.0	0.0	0.0	0.0
-79.5	1.00	6019.55	3.062e+05	1.00	1.478e+05	3.062e+05	0.0	0.0	0.0	0.0	0.0	0.0
-79.3	1.00	5969.90	3.062e+05	1.00	1.478e+05	3.062e+05	0.0	0.0	0.0	0.0	0.0	0.0
-79.2	1.00	5925.93	3.062e+05	1.00	1.478e+05	3.062e+05	0.0	0.0	0.0	0.0	0.0	0.0
-79.0	1.00	5883.37	3.062e+05	1.00	1.478e+05	3.063e+05	0.0	0.0	0.0	0.0	0.0	0.0
-79.0	1.00	5873.24	3.062e+05	1.00	1.478e+05	3.062e+05	0.0	0.0	0.0	0.0	0.0	0.0
-78.9	1.00	5874.96	3.062e+05	1.00	1.478e+05	3.061e+05	0.0	0.0	0.0	0.0	0.0	0.0
-78.8	1.00	5882.94	3.062e+05	1.00	1.478e+05	3.061e+05	0.0	0.0	0.0	0.0	0.0	0.0
-78.7	1.00	5873.01	3.062e+05	1.00	1.478e+05	3.061e+05	0.0	0.0	0.0	0.0	0.0	0.0
-78.5	1.00	5848.77	3.062e+05	1.00	1.478e+05	3.061e+05	0.0	0.0	0.0	0.0	0.0	0.0
-78.5	1.00	5829.35	3.062e+05	1.00	1.478e+05	3.061e+05	0.0	0.0	0.0	0.0	0.0	0.0
-78.3	1.00	5718.59	3.062e+05	1.00	1.478e+05	3.061e+05	0.0	0.0	0.0	0.0	0.0	0.0
-40.0	1.00	5698.43	3.062e+05	1.00	1.478e+05	3.061e+05	0.0	0.0	0.0	0.0	0.0	0.0

Quota cm	V[7.4.16]	N daN	M daN cm	V daN	alfaS	VRd,c daN	VRd,s daN	V[7.4.17]	roH	roV	roN
-270.0	0.11	-2.150e+04	5.410e+05	8352.35	0.14	5.823e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-231.7	0.11	-2.112e+04	4.213e+05	8525.69	0.14	5.786e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-193.3	0.11	-2.018e+04	2.994e+05	8233.48	0.14	5.241e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-155.0	0.11	-1.910e+04	1.886e+05	7660.79	0.14	5.135e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-116.7	0.10	-1.784e+04	5.651e+04	6942.05	0.14	5.010e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-80.0	0.09	-1.724e+04	8.508e+04	6266.61	0.14	4.951e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-79.9	0.09	-1.711e+04	5.744e+04	6249.44	0.14	4.938e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-79.7	0.09	-1.707e+04	4.996e+04	6151.69	0.14	4.934e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-79.6	0.09	-1.699e+04	4.006e+04	6078.43	0.14	4.926e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-79.5	0.09	-1.690e+04	3.150e+04	6019.55	0.14	4.918e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-79.3	0.09	-1.682e+04	2.637e+04	5969.90	0.14	4.909e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-79.2	0.09	-1.675e+04	2.491e+04	5925.93	0.14	4.902e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-79.0	0.09	-1.668e+04	2.614e+04	5883.37	0.14	4.896e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-79.0	0.09	-1.666e+04	2.730e+04	5873.24	0.14	4.893e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-78.9	0.09	-1.663e+04	2.949e+04	5874.96	0.14	4.890e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-78.8	0.09	-1.660e+04	3.300e+04	5882.94	0.14	4.887e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-78.7	0.09	-1.658e+04	3.503e+04	5873.01	0.14	4.886e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-78.5	0.09	-1.655e+04	3.993e+04	5848.77	0.14	4.883e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-78.5	0.09	-1.654e+04	4.303e+04	5829.35	0.14	4.882e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-78.3	0.08	-1.645e+04	6.216e+04	5718.59	0.14	4.873e+04	1.951e+04	0.0	5.13e-03	7.70e-03	0.0
-40.0	0.09	-1.681e+04	1.339e+05	5698.43	0.11	4.908e+04	1.488e+04	0.0	5.13e-03	7.70e-03	0.0

Quota	V[7.4.16]	V[7.4.17]
0.11	0.0	0.0

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z daN/cm	N o daN/cm	N zo daN/cm	M z daN	M o daN	M zo daN
34	ok	0.33	5.27e-02	0.0	11.6	11.6	5.1	5.1	51.3	7.4	-3.9	-311.9	-39.5	5.1
35	ok	0.33	0.1	2.03e-02	11.6	11.6	5.1	5.1	-48.3	-23.5	-2.8	-704.2	-121.8	8.1
36	ok	0.33	0.2	2.72e-02	11.6	11.6	5.1	5.1	-88.2	-35.6	-11.6	-1077.6	-203.5	18.4
37	ok	0.28	0.3	3.58e-02	7.7	7.7	5.1	5.1	-104.9	-38.4	-18.1	-1273.0	-249.8	20.1
38	ok	0.28	0.3	3.82e-02	7.7	7.7	5.1	5.1	-111.2	-37.5	-21.2	-1353.2	-270.7	14.2
39	ok	0.28	0.3	3.86e-02	7.7	7.7	5.1	5.1	-111.3	-33.1	-1.4	-1377.4	-279.8	-12.6
40	ok	0.28	0.3	3.78e-02	7.7	7.7	5.1	5.1	-109.0	-31.7	-1.2	-1372.6	-279.2	-24.3
41	ok	0.28	0.3	3.69e-02	7.7	7.7	5.1	5.1	-108.0	-34.3	-19.5	-1367.1	-279.1	-27.2
42	ok	0.28	0.3	3.48e-02	7.7	7.7	5.1	5.1	-98.6	-31.3	-2.4	-1341.6	-260.7	-40.1

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

43	ok	0.28	0.3	3.28e-02	7.7	7.7	5.1	5.1	-100.8	-32.0	-1.8	-1323.9	-268.2	-40.6
44	ok	0.28	0.3	3.04e-02	7.7	7.7	5.1	5.1	-84.0	-27.8	-2.1	-1204.0	-245.3	-53.1
45	ok	0.33	0.2	2.44e-02	11.6	11.6	5.1	5.1	-75.5	-27.7	-17.3	-1079.9	-208.4	-39.8
46	ok	0.33	0.2	2.16e-02	11.6	11.6	5.1	5.1	-66.4	-23.9	-5.5	-985.8	-187.7	-41.6
47	ok	0.33	0.1	1.74e-02	11.6	11.6	5.1	5.1	-46.2	-16.2	-5.8	-763.1	-140.6	-31.8
48	ok	0.33	0.1	1.56e-02	11.6	11.6	5.1	5.1	-31.4	-10.3	-4.1	-593.0	-111.7	-21.8
49	ok	0.33	3.84e-02	0.0	11.6	11.6	5.1	5.1	54.0	15.4	5.0	-229.1	-26.7	-7.2
222	ok	0.33	9.12e-02	9.36e-03	11.6	11.6	5.1	5.1	-11.0	-15.4	-12.4	-83.9	-298.0	-56.7
223	ok	0.33	5.63e-02	1.59e-02	11.6	11.6	5.1	5.1	-36.3	-3.5	15.2	-101.0	38.4	-173.4
224	ok	0.33	4.98e-02	2.33e-02	11.6	11.6	5.1	5.1	-74.0	-9.8	5.5	-125.0	47.4	-87.1
225	ok	0.28	6.79e-02	3.28e-02	7.7	7.7	5.1	5.1	-95.5	-12.5	-5.1	-153.4	2.1	-40.9
226	ok	0.28	7.42e-02	3.65e-02	7.7	7.7	5.1	5.1	-105.8	-14.4	-10.0	-171.3	-31.0	-16.7
227	ok	0.28	7.74e-02	3.76e-02	7.7	7.7	5.1	5.1	-109.1	-15.7	-11.5	-177.5	-49.7	-15.3
228	ok	0.28	7.79e-02	3.71e-02	7.7	7.7	5.1	5.1	-107.6	-16.6	-11.2	-175.7	-58.9	-28.7
229	ok	0.28	7.71e-02	3.53e-02	7.7	7.7	5.1	5.1	-105.4	-18.3	-15.7	-165.7	-62.9	-51.4
230	ok	0.28	6.91e-02	3.42e-02	7.7	7.7	5.1	5.1	-101.8	-17.0	-16.2	-132.5	-27.0	-46.6
231	ok	0.28	6.53e-02	3.32e-02	7.7	7.7	5.1	5.1	-96.6	-16.0	-7.5	-135.9	-46.3	-32.5
232	ok	0.28	5.34e-02	2.82e-02	7.7	7.7	5.1	5.1	-82.3	-15.3	-16.9	-88.3	-4.5	-31.6
233	ok	0.33	5.56e-02	2.32e-02	11.6	11.6	5.1	5.1	-66.5	-12.7	-17.8	-47.6	65.0	33.5
234	ok	0.33	6.33e-02	2.14e-02	11.6	11.6	5.1	5.1	-58.1	-11.5	-16.0	-32.4	73.1	45.9
235	ok	0.33	6.16e-02	1.76e-02	11.6	11.6	5.1	5.1	-40.4	-10.2	-23.0	-11.2	74.6	90.8
236	ok	0.33	6.05e-02	1.58e-02	11.6	11.6	5.1	5.1	-12.6	-15.2	-21.7	14.8	-2.1	200.9
237	ok	0.33	0.1	9.69e-03	11.6	11.6	5.1	5.1	-3.1	-15.7	-2.8	-72.2	-372.4	32.0
281	ok	0.28	0.2	1.40e-02	7.7	7.7	5.1	5.1	-38.1	-25.3	-8.5	-57.1	-543.4	-35.2
282	ok	0.28	6.99e-02	1.11e-02	7.7	7.7	5.1	5.1	-23.5	-24.1	1.8	166.5	53.4	-142.9
283	ok	0.28	0.1	2.04e-02	7.7	7.7	5.1	5.1	-61.9	-2.7	1.2	208.2	174.0	-48.4
284	ok	0.28	0.1	2.92e-02	7.7	7.7	5.1	5.1	-89.2	0.6	-6.2	292.4	132.0	-17.4
285	ok	0.28	0.1	3.40e-02	7.7	7.7	5.1	5.1	-103.3	-0.5	-10.2	327.9	79.5	-3.4
286	ok	0.28	0.1	3.58e-02	7.7	7.7	5.1	5.1	-108.6	-2.7	-11.9	342.6	45.6	-5.4
287	ok	0.28	0.1	3.57e-02	7.7	7.7	5.1	5.1	-108.1	-4.6	-12.3	352.6	34.1	-16.9
288	ok	0.28	0.1	3.41e-02	7.7	7.7	5.1	5.1	-100.1	-4.7	-10.2	371.7	71.7	-25.0
289	ok	0.28	0.1	3.21e-02	7.7	7.7	5.1	5.1	-97.5	-5.5	-9.1	377.1	102.5	-32.2
290	ok	0.28	0.1	3.14e-02	7.7	7.7	5.1	5.1	-89.9	-5.1	-11.4	380.5	121.0	-30.8
291	ok	0.28	0.1	2.64e-02	7.7	7.7	5.1	5.1	-74.4	-6.5	-12.3	361.2	154.9	-14.0
292	ok	0.28	0.1	2.19e-02	7.7	7.7	5.1	5.1	-59.6	-8.7	-14.9	327.1	193.0	9.0
293	ok	0.28	0.1	2.00e-02	7.7	7.7	5.1	5.1	-54.5	-10.4	-18.1	300.9	192.0	24.3
294	ok	0.28	8.29e-02	1.59e-02	7.7	7.7	5.1	5.1	-36.5	-14.7	-16.4	221.3	156.8	32.2
295	ok	0.28	6.16e-02	1.45e-02	7.7	7.7	5.1	5.1	-21.8	-19.6	-15.0	144.5	101.3	51.1
296	ok	0.28	0.2	1.47e-02	7.7	7.7	5.1	5.1	-19.1	-31.7	-3.1	-115.3	-731.4	9.7
340	ok	0.28	0.2	1.48e-02	7.7	7.7	5.1	5.1	-39.8	-21.3	11.0	-59.0	-565.9	-5.2
341	ok	0.28	4.68e-02	9.56e-03	7.7	7.7	5.1	5.1	-22.2	-23.5	-5.4	163.7	36.1	18.5
342	ok	0.28	8.95e-02	1.81e-02	7.7	7.7	5.1	5.1	-52.3	4.8	-7.2	171.3	175.5	74.7
343	ok	0.28	0.1	2.74e-02	7.7	7.7	5.1	5.1	-81.1	8.6	-7.1	255.8	125.4	53.0
344	ok	0.28	0.1	3.24e-02	7.7	7.7	5.1	5.1	-96.4	7.5	-7.8	291.2	63.1	31.6
345	ok	0.28	0.1	3.44e-02	7.7	7.7	5.1	5.1	-102.4	4.9	-9.0	304.8	22.4	12.7
346	ok	0.28	0.1	3.45e-02	7.7	7.7	5.1	5.1	-102.4	2.6	-7.8	315.2	6.9	-6.6
347	ok	0.28	0.1	3.30e-02	7.7	7.7	5.1	5.1	-97.2	1.3	-9.2	336.0	48.5	-19.9
348	ok	0.28	0.1	3.11e-02	7.7	7.7	5.1	5.1	-94.4	-1.57e-02	-9.5	340.4	82.9	-34.4
349	ok	0.28	0.1	3.00e-02	7.7	7.7	5.1	5.1	-87.1	0.2	-10.6	349.1	103.7	-41.8
350	ok	0.28	0.1	2.49e-02	7.7	7.7	5.1	5.1	-71.3	-1.9	-9.2	333.9	149.2	-54.5
351	ok	0.28	9.71e-02	1.99e-02	7.7	7.7	5.1	5.1	-56.4	-5.1	-9.1	300.0	188.2	-63.1
352	ok	0.28	8.42e-02	1.73e-02	7.7	7.7	5.1	5.1	-48.0	-7.3	-8.8	270.4	189.3	-77.1
353	ok	0.28	6.62e-02	1.24e-02	7.7	7.7	5.1	5.1	-31.5	-12.8	-7.4	194.6	151.1	-81.8
354	ok	0.28	5.53e-02	1.09e-02	7.7	7.7	5.1	5.1	-24.7	-17.7	-9.1	119.4	74.7	-78.3
355	ok	0.28	0.2	1.41e-02	7.7	7.7	5.1	5.1	-23.3	-30.6	-14.3	-135.6	-807.7	-11.5
399	ok	0.28	0.1	9.30e-03	7.7	7.7	5.1	5.1	57.4	-3.2	7.5	-208.9	-77.8	23.1
400	ok	0.28	5.65e-02	8.66e-03	7.7	7.7	5.1	5.1	-9.0	12.6	-18.7	-130.6	102.9	170.6
401	ok	0.28	7.88e-02	1.92e-02	7.7	7.7	5.1	5.1	-56.8	12.3	-11.6	-122.3	72.7	128.0
402	ok	0.28	7.96e-02	2.70e-02	7.7	7.7	5.1	5.1	-82.6	10.7	-6.1	-142.9	3.0	75.8
403	ok	0.28	8.09e-02	3.12e-02	7.7	7.7	5.1	5.1	-95.3	7.5	-2.6	-175.5	-60.6	36.8
404	ok	0.28	8.67e-02	3.29e-02	7.7	7.7	5.1	5.1	-100.7	4.5	-3.9	-195.2	-96.9	16.5
405	ok	0.28	8.70e-02	3.31e-02	7.7	7.7	5.1	5.1	-101.0	2.3	-5.9	-194.2	-109.7	7.4
406	ok	0.28	8.16e-02	3.19e-02	7.7	7.7	5.1	5.1	-94.5	1.4	-10.1	-164.1	-93.7	-0.6
407	ok	0.28	8.03e-02	3.01e-02	7.7	7.7	5.1	5.1	-89.6	0.9	-10.0	-129.3	-50.5	-13.8
408	ok	0.28	8.03e-02	2.91e-02	7.7	7.7	5.1	5.1	-86.1	1.0	-8.4	-112.5	-48.6	-26.0
409	ok	0.28	7.87e-02	2.44e-02	7.7	7.7	5.1	5.1	-73.7	2.37e-02	-7.0	-58.7	30.7	-54.3
410	ok	0.28	7.82e-02	1.97e-02	7.7	7.7	5.1	5.1	-60.0	-1.0	-4.4	-26.6	75.3	-90.6
411	ok	0.28	7.60e-02	1.69e-02	7.7	7.7	5.1	5.1	-51.6	-1.8	-4.4	-14.7	87.0	-102.5
412	ok	0.28	6.02e-02	1.13e-02	7.7	7.7	5.1	5.1	-32.0	-2.4	-0.4	9.2	85.4	-131.2
413	ok	0.28	5.36e-02	7.62e-03	7.7	7.7	5.1	5.1	-18.3	-4.2	2.6	5.6	54.3	-168.0
414	ok	0.28	0.2	1.01e-02	7.7	7.7	5.1	5.1	-14.0	-20.5	-11.9	-112.5	-597.6	-26.3
465	ok	0.28	6.94e-02	1.36e-03	7.7	7.7	5.1	5.1	95.2	15.7	-16.6	-232.5	199.4	52.4
486	ok	0.28	9.16e-02	9.65e-03	7.7	7.7	5.1	5.1	-15.3	17.6	-13.3	-394.3	22.4	101.4
488	ok	0.28	0.1	2.07e-02	7.7	7.7	5.1	5.1	-61.0	9.6	-3.6	-630.4	-98.8	54.2
491	ok	0.28	0.2	2.71e-02	7.7	7.7	5.1	5.1	-80.4	4.7	1.5	-825.0	-186.2	-29.7
492	ok	0.28	0.2	3.01e-02	7.7	7.7	5.1	5.1	-89.8	0.8	1.7	-975.5	-239.5	-32.7
494	ok	0.28	0.2	3.13e-02	7.7	7.7	5.1	5.1	-93.4	-1.7	-0.8	-1053.9	-265.8	-10.9
496	ok	0.28	0.2	3.14e-02	7.7	7.7	5.1	5.1	-93.0	-2.8	-6.8	-1069.3	-272.0	25.6
498	ok	0.28	0.2	3.05e-02	7.7	7.7	5.1	5.1	-90.3	-4.3	-7.5	-1023.7	-259.0	59.9

SCARICATORE IN VIA PUCCI

500	ok	0.28	0.2	2.92e-02	7.7	7.7	5.1	5.1	-88.5	-4.1	-8.3	-952.2	-226.0	70.9
502	ok	0.28	0.2	2.85e-02	7.7	7.7	5.1	5.1	-84.3	-4.1	-9.7	-913.6	-221.1	74.2
504	ok	0.28	0.2	2.47e-02	7.7	7.7	5.1	5.1	-70.8	-1.5	-9.2	-741.9	-162.0	76.5
505	ok	0.28	0.1	2.06e-02	7.7	7.7	5.1	5.1	-60.9	1.0	-5.3	-590.6	-109.9	52.7
507	ok	0.28	0.1	1.80e-02	7.7	7.7	5.1	5.1	-53.2	2.7	-6.1	-506.9	-84.2	37.8
508	ok	0.28	9.11e-02	1.22e-02	7.7	7.7	5.1	5.1	-37.4	4.9	-2.5	-366.8	-38.3	-45.9
509	ok	0.28	6.79e-02	8.60e-03	7.7	7.7	5.1	5.1	-25.0	7.3	6.8	-255.6	-43.7	-70.1
510	ok	0.28	7.19e-02	3.88e-03	7.7	7.7	5.1	5.1	35.6	10.8	-9.6	-71.9	132.4	-18.1
521	ok	0.28	4.70e-02	5.44e-04	7.7	7.7	5.1	5.1	77.0	-1.0	-4.8	-201.5	111.6	-26.7
522	ok	0.28	0.2	1.50e-02	7.7	7.7	5.1	5.1	-25.0	-24.6	3.5	-835.3	-114.5	-154.6
523	ok	0.28	0.3	2.16e-02	7.7	7.7	5.1	5.1	-63.5	-20.8	6.0	-1515.6	-305.9	-158.6
524	ok	0.28	0.4	2.73e-02	7.7	7.7	5.1	5.1	-81.4	-16.9	9.1	-1945.5	-407.1	-122.6
525	ok	0.28	0.5	2.90e-02	7.7	7.7	5.1	5.1	-88.0	-14.4	8.8	-2183.6	-457.4	-78.1
526	ok	0.28	0.5	2.98e-02	7.7	7.7	5.1	5.1	-90.5	-13.4	6.1	-2289.8	-478.0	-30.8
527	ok	0.28	0.5	3.01e-02	7.7	7.7	5.1	5.1	-90.1	-13.7	-12.8	-2306.9	-481.2	27.4
528	ok	0.28	0.5	2.93e-02	7.7	7.7	5.1	5.1	-86.2	-14.2	-14.8	-2232.8	-463.9	74.8
529	ok	0.28	0.4	2.89e-02	7.7	7.7	5.1	5.1	-80.3	-15.2	-15.2	-2130.7	-438.1	99.7
530	ok	0.28	0.4	2.89e-02	7.7	7.7	5.1	5.1	-79.5	-14.8	-4.9	-2056.1	-424.6	105.8
531	ok	0.28	0.4	2.56e-02	7.7	7.7	5.1	5.1	-73.2	-14.3	-17.7	-1758.0	-365.2	147.1
532	ok	0.28	0.3	2.18e-02	7.7	7.7	5.1	5.1	-61.6	-12.2	-16.4	-1480.2	-302.5	162.2
533	ok	0.28	0.3	2.02e-02	7.7	7.7	5.1	5.1	-57.4	-10.6	-14.6	-1307.7	-269.9	162.5
534	ok	0.28	0.2	1.46e-02	7.7	7.7	5.1	5.1	-38.5	-5.2	-15.2	-962.4	-196.7	164.0
535	ok	0.28	0.2	1.08e-02	7.7	7.7	5.1	5.1	-26.1	-1.5	-14.3	-715.2	-143.0	154.0
536	ok	0.28	4.73e-02	2.11e-04	7.7	7.7	5.1	5.1	50.8	9.0	-13.1	-205.8	61.4	34.7

Nodo	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
	0.33	0.48	0.04	11.59	11.59	5.13	5.13	-111.34	-38.37	-23.00	-2306.89	-807.67	-173.38
								95.21	17.63	15.15	380.47	199.43	200.86

Nodo	Stato	Max tau daN/cm2	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr daN/cm	V sec daN/cm
34	ok	0.64						
35	ok	1.21						
36	ok	2.27						
37	ok	2.56						
38	ok	2.65						
39	ok	2.66						
40	ok	2.64						
41	ok	2.72						
42	ok	2.80						
43	ok	2.68						
44	ok	2.33						
45	ok	2.35						
46	ok	2.16						
47	ok	1.66						
48	ok	1.12						
49	ok	0.80						
222	ok	0.96						
223	ok	2.26						
224	ok	2.31						
225	ok	2.63						
226	ok	2.76						
227	ok	2.79						
228	ok	2.83						
229	ok	2.90						
230	ok	2.69						
231	ok	2.98						
232	ok	2.59						
233	ok	2.26						
234	ok	2.23						
235	ok	1.81						
236	ok	1.79						
237	ok	0.84						
281	ok	1.59						
282	ok	1.70						
283	ok	1.23						
284	ok	1.25						
285	ok	1.31						
286	ok	1.34						
287	ok	1.42						
288	ok	1.56						
289	ok	1.39						
290	ok	1.67						
291	ok	1.41						
292	ok	1.26						
293	ok	1.08						
294	ok	1.15						
295	ok	1.64						

SCARICATORE IN VIA PUCCI

296	ok	1.72
340	ok	1.50
341	ok	1.57
342	ok	1.11
343	ok	1.02
344	ok	1.10
345	ok	1.11
346	ok	1.14
347	ok	1.19
348	ok	1.06
349	ok	1.29
350	ok	1.08
351	ok	1.00
352	ok	0.98
353	ok	1.25
354	ok	1.66
355	ok	1.83
399	ok	1.09
400	ok	1.26
401	ok	1.29
402	ok	1.57
403	ok	1.69
404	ok	1.72
405	ok	1.74
406	ok	1.79
407	ok	1.67
408	ok	1.85
409	ok	1.53
410	ok	1.35
411	ok	1.27
412	ok	1.04
413	ok	1.23
414	ok	1.36
465	ok	1.63
486	ok	2.04
488	ok	2.38
491	ok	2.42
492	ok	2.37
494	ok	2.30
496	ok	2.29
498	ok	2.32
500	ok	2.31
502	ok	2.50
504	ok	2.42
505	ok	2.26
507	ok	2.21
508	ok	2.04
509	ok	1.93
510	ok	1.42
521	ok	0.84
522	ok	1.14
523	ok	2.05
524	ok	2.32
525	ok	2.35
526	ok	2.30
527	ok	2.30
528	ok	2.39
529	ok	2.45
530	ok	2.32
531	ok	2.28
532	ok	2.18
533	ok	1.95
534	ok	1.64
535	ok	1.33
536	ok	1.27

Nodo	Max tau 2.98	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
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Parete	H totale	Spessore	H critica	H critica V	L totale	L confinata	Verif. N	Verif. N-M	Fattore V	Diagramma V	Verif. V	Prog. composta
	cm	cm	cm	cm	cm	cm						
8	230.00	20.00	40.00	40.00	325.00	30.00	ok	ok	1.50	SI	ok	SI

SCARICATORE IN VIA PUCCI

Quota cm	Af conf.	Af std	Af V (ori)	Ver. N	Ver. N/M	Ver. V cls	Ver. V acc	Ver. V acc(7)	Ver. V scorr.	N add daN	M invil daN	V invil daN		
-270.0	4d14	14/20	14/30	0.07	0.04	0.08	3.68e-03	0.06	0.08	0.0	2.473e+05	3250.01		
-231.7	4d14	14/20	14/30	0.07	0.03	0.09	7.11e-03	0.07	0.08	0.0	2.473e+05	3250.01		
-193.3	0d0	14/20	14/30	0.07	0.04	0.04	7.58e-03	0.07	0.0	0.0	2.473e+05	3250.01		
-155.0	0d0	14/20	14/30	0.06	0.02	0.04	5.09e-03	0.07	0.0	0.0	2.473e+05	3150.61		
-116.7	0d0	14/20	14/30	0.06	0.04	0.04	0.01	0.07	0.0	0.0	2.473e+05	3051.20		
-80.0	0d0	14/20	14/30	0.06	0.05	0.03	9.70e-03	0.07	0.0	0.0	2.473e+05	2956.11		
-40.0	0d0	14/20	14/30	0.02	2.44e-03	0.01	0.02	0.03	0.0	0.0	2.473e+05	2852.38		
Quota				Ver. N	Ver. N/M	Ver. V cls	Ver. V acc	Ver. V acc(7)	Ver. V scorr.					
				0.07	0.05	0.09	0.02	0.07	0.08					
Quota cm	N v.N daN	N v.M/N daN	M v.M/N daN cm	N v.Vcls daN	V v.Vcls daN	N v.Vacc daN	M v. Vacc daN cm	V v.Vacc daN	N v.Vscor daN	M v.Vscor daN cm	V v.Vscor daN			
-270.0	-1.265e+04	-1.084e+04	2.385e+05	-1.084e+04	2855.88	-1.258e+04	2.036e+04	151.33	-1.084e+04	2.385e+05	2855.88			
-231.7	-1.259e+04	-1.110e+04	1.873e+05	-1.110e+04	2997.36	-1.249e+04	2.047e+04	292.81	-1.110e+04	1.873e+05	2997.36			
-193.3	-1.181e+04	-9509.85	1.619e+05	-1.043e+04	3250.01	-1.176e+04	5.214e+04	316.69	0.0	0.0	0.0			
-155.0	-1.140e+04	-8974.85	9.761e+04	-1.082e+04	3215.50	-8216.96	6.758e+04	212.61	0.0	0.0	0.0			
-116.7	-1.104e+04	-9496.36	1.872e+05	-9496.36	3089.04	-8546.11	3.920e+04	454.56	0.0	0.0	0.0			
-80.0	-1.099e+04	-9926.44	2.473e+05	-8955.06	2845.27	-7813.91	4.266e+04	405.02	0.0	0.0	0.0			
-40.0	-8419.05	-7592.77	6.735e+04	-8419.05	2852.38	-7290.13	3.991e+04	1709.45	0.0	0.0	0.0			
Quota cm	Ctg Vcls	Vrsd Vcls daN	Vrcd Vcls daN	Ctg Vac	Vrsd Vac daN	Vrcd Vac daN	Vdd daN	Vid daN	[A s.i. cm2	Incli. gradi	Dist.] cm	Vfd daN		
-270.0	1.00	2855.88	3.457e+04	1.00	4.116e+04	3.470e+04	2.108e+04	3194.10	1.0	35.3	0.0	1.138e+04		
-231.7	1.00	2997.36	3.459e+04	1.00	4.116e+04	3.470e+04	2.108e+04	3194.10	1.0	35.3	0.0	1.115e+04		
-193.3	1.00	3250.01	8.761e+04	1.00	4.176e+04	8.787e+04	0.0	0.0	0.0	0.0	0.0	0.0		
-155.0	1.00	3215.50	8.768e+04	1.00	4.176e+04	8.718e+04	0.0	0.0	0.0	0.0	0.0	0.0		
-116.7	1.00	3089.04	8.743e+04	1.00	4.176e+04	8.725e+04	0.0	0.0	0.0	0.0	0.0	0.0		
-80.0	1.00	2845.27	8.733e+04	1.00	4.176e+04	8.711e+04	0.0	0.0	0.0	0.0	0.0	0.0		
-40.0	1.00	2852.38	2.124e+05	1.00	1.028e+05	2.121e+05	0.0	0.0	0.0	0.0	0.0	0.0		
Quota cm	V[7.4.16]	N daN	M daN cm	V daN	alfaS	VRd,c daN	VRd,s daN	V[7.4.17]	roH	roV	roN			
-270.0	0.06	-9482.28	2.207e+05	2807.71	0.60	2.002e+04	2.434e+04	0.0	5.13e-03	7.70e-03	0.0			
-231.7	0.07	-9798.56	1.699e+05	2949.20	0.60	2.032e+04	2.434e+04	0.0	5.13e-03	7.70e-03	0.0			
-193.3	0.07	-9360.30	1.214e+05	3199.48	0.60	1.916e+04	2.434e+04	0.0	5.13e-03	7.70e-03	0.0			
-155.0	0.07	-9962.71	3.569e+04	3196.52	0.60	1.974e+04	2.434e+04	0.0	5.13e-03	7.70e-03	0.0			
-116.7	0.07	-9496.36	1.872e+05	3089.04	0.60	1.929e+04	2.434e+04	0.0	5.13e-03	7.70e-03	0.0			
-80.0	0.07	-8955.06	2.299e+05	2845.27	0.60	1.877e+04	2.434e+04	0.0	5.13e-03	7.70e-03	0.0			
-40.0	0.03	-8419.05	4.441e+04	2852.38	0.56	3.128e+04	5.524e+04	0.0	5.13e-03	7.70e-03	0.0			
Quota	V[7.4.16] 0.07							V[7.4.17] 0.0						
Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z daN/cm	N o daN/cm	N zo daN/cm	M z daN	M o daN	M zo daN
34	ok	0.31	4.92e-02	0.0	10.3	10.3	5.1	5.1	56.4	15.0	25.6	-267.3	-49.3	-10.1
50	ok	0.31	0.1	3.42e-02	10.3	10.3	5.1	5.1	-32.8	-9.0	27.4	-574.7	-151.8	-7.9
66	ok	0.31	0.2	0.1	10.3	10.3	5.1	5.1	-372.9	-48.8	-74.8	-697.3	-13.6	17.8
146	ok	0.31	0.2	0.2	10.3	10.3	5.1	5.1	-523.5	-72.7	110.5	-833.1	-13.6	-6.1
162	ok	0.31	0.1	4.10e-02	10.3	10.3	5.1	5.1	-31.1	-24.5	-4.5	-738.3	-160.1	23.0
178	ok	0.31	6.95e-02	2.86e-03	10.3	10.3	5.1	5.1	19.8	7.0	-16.8	-386.6	-85.6	28.1
194	ok	0.31	6.38e-02	0.0	10.3	10.3	5.1	5.1	95.4	17.7	-17.1	-334.1	-29.3	13.4
222	ok	0.31	8.70e-02	1.28e-02	10.3	10.3	5.1	5.1	25.6	-15.2	-6.9	-68.3	-194.5	10.6
238	ok	0.31	6.31e-02	4.75e-02	10.3	10.3	5.1	5.1	-118.1	-5.6	-14.4	-12.1	-33.2	91.5
240	ok	0.31	7.95e-02	8.11e-02	10.3	10.3	5.1	5.1	-258.3	17.8	15.9	42.5	-42.7	76.8
246	ok	0.31	8.79e-02	9.52e-02	10.3	10.3	5.1	5.1	-286.6	32.7	-30.1	8.2	-28.4	-70.3
248	ok	0.31	8.52e-02	7.12e-02	10.3	10.3	5.1	5.1	-156.7	-1.0	31.5	-26.7	-20.9	-101.5
250	ok	0.31	4.51e-02	1.64e-02	10.3	10.3	5.1	5.1	-4.5	-14.4	18.2	-53.7	-100.3	-54.0
252	ok	0.31	7.86e-02	1.14e-02	10.3	10.3	5.1	5.1	52.5	-12.2	-8.2	-79.9	-186.0	15.0
281	ok	0.28	0.2	1.77e-02	7.7	7.7	5.1	5.1	-39.8	-28.3	0.6	-87.1	-542.5	-24.5
297	ok	0.28	6.36e-02	4.12e-02	7.7	7.7	5.1	5.1	-126.5	-11.3	-3.16e-02	90.8	-22.7	-23.1
299	ok	0.28	0.1	8.00e-02	7.7	7.7	5.1	5.1	-243.1	2.2	0.4	160.6	-20.6	-33.8
305	ok	0.28	0.1	8.25e-02	7.7	7.7	5.1	5.1	-253.3	2.3	-1.0	173.4	-9.7	-32.2
307	ok	0.28	7.77e-02	5.00e-02	7.7	7.7	5.1	5.1	-146.0	-5.8	13.1	113.0	21.6	-19.0
309	ok	0.28	9.13e-02	1.85e-02	7.7	7.7	5.1	5.1	-28.9	-21.9	19.4	-13.6	-288.3	4.8
311	ok	0.28	0.2	1.96e-02	7.7	7.7	5.1	5.1	-34.2	-27.7	4.0	-74.2	-533.0	20.1
340	ok	0.28	0.2	1.60e-02	7.7	7.7	5.1	5.1	-40.3	-28.1	12.5	-101.3	-565.7	-18.0
356	ok	0.28	7.56e-02	4.43e-02	7.7	7.7	5.1	5.1	-130.4	-8.3	23.2	51.1	-20.5	-131.3
358	ok	0.28	0.1	8.65e-02	7.7	7.7	5.1	5.1	-262.4	6.7	1.6	134.3	-14.2	-87.6
364	ok	0.28	0.1	7.72e-02	7.7	7.7	5.1	5.1	-234.3	4.8	0.7	149.0	-16.0	65.7
366	ok	0.28	7.61e-02	4.65e-02	7.7	7.7	5.1	5.1	-137.0	-3.6	-1.0	91.1	25.0	95.1

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

368	ok	0.28	0.1	1.28e-02	7.7	7.7	5.1	5.1	-37.9	-21.8	3.9	-47.8	-343.4	26.2
370	ok	0.28	0.2	1.76e-02	7.7	7.7	5.1	5.1	-46.5	-24.6	14.1	-100.3	-576.7	-9.7
399	ok	0.28	0.1	1.16e-02	7.7	7.7	5.1	5.1	64.3	-10.0	3.0	-62.7	-83.1	-16.1
415	ok	0.28	9.36e-02	7.25e-02	7.7	7.7	5.1	5.1	-176.3	-45.4	86.9	-133.4	7.6	-161.0
417	ok	0.28	0.1	0.1	7.7	7.7	5.1	5.1	-296.6	67.8	-33.8	62.0	-18.8	-180.0
423	ok	0.28	9.85e-02	8.51e-02	7.7	7.7	5.1	5.1	-225.6	48.8	33.4	114.5	-52.7	148.8
425	ok	0.28	9.25e-02	6.55e-02	7.7	7.7	5.1	5.1	-184.7	-26.1	-51.7	-103.9	27.9	191.4
427	ok	0.28	8.05e-02	1.14e-02	7.7	7.7	5.1	5.1	-28.0	-16.8	-10.7	-54.6	-259.0	25.9
429	ok	0.28	0.1	1.13e-02	7.7	7.7	5.1	5.1	-29.7	-17.2	2.6	-88.5	-422.9	-11.7
465	ok	0.28	6.85e-02	1.02e-03	7.7	7.7	5.1	5.1	103.0	15.6	-24.5	-74.1	202.0	16.8
466	ok	0.28	9.70e-02	3.29e-02	7.7	7.7	5.1	5.1	-75.3	-48.3	-33.8	-303.7	36.7	15.9
467	ok	0.28	0.3	0.2	7.7	7.7	5.1	5.1	-548.1	-147.4	153.1	-929.8	-15.1	55.5
468	ok	0.28	0.2	5.02e-03	7.7	7.7	5.1	5.1	110.0	203.1	-28.5	161.2	-233.1	169.0
469	ok	0.28	0.2	0.0	7.7	7.7	5.1	5.1	4.6	317.8	6.6	-15.4	-106.8	85.4
470	ok	0.28	0.2	0.0	7.7	7.7	6.1	5.1	8.6	330.6	2.3	-50.6	-296.9	-107.6
471	ok	0.28	0.2	2.66e-03	7.7	7.7	5.1	5.1	-1.0	180.1	-36.1	157.0	-257.8	-399.6
472	ok	0.28	0.3	0.2	7.7	7.7	5.1	5.1	-193.4	-123.7	-172.4	-515.2	141.1	-616.1
473	ok	0.28	9.40e-02	3.50e-02	7.7	7.7	5.1	5.1	-85.5	-58.3	30.6	-290.8	162.5	-16.4
474	ok	0.28	5.03e-02	1.15e-02	7.7	7.7	5.1	5.1	9.4	-1.3	33.3	-80.0	143.3	-50.6
475	ok	0.28	5.97e-02	4.41e-03	7.7	7.7	5.1	5.1	51.2	5.5	26.0	-60.7	196.4	-9.8
521	ok	0.28	5.74e-02	2.07e-03	7.7	7.7	5.1	5.1	72.2	10.8	-36.1	-241.2	81.5	41.9
537	ok	0.28	0.2	2.66e-02	7.7	7.7	5.1	5.1	-63.5	51.5	-48.4	-724.3	-147.5	225.6
555	ok	0.28	0.2	3.83e-02	7.7	7.7	5.1	5.1	-81.7	108.7	76.9	-885.9	-243.0	254.8
573	ok	0.28	0.2	8.38e-02	7.7	7.7	5.1	5.1	-58.5	-125.3	151.6	-535.0	-126.5	220.0
591	ok	0.28	9.81e-02	4.71e-02	7.7	7.7	5.1	5.1	-40.6	-121.3	38.1	-269.9	-71.3	67.1
609	ok	0.28	0.1	5.19e-02	7.7	7.7	5.1	5.1	-26.7	-138.9	-36.1	-512.7	-155.2	2.2
627	ok	0.28	0.3	9.51e-02	7.7	7.7	5.1	5.1	-119.0	-112.8	-166.8	-1128.6	-284.1	-623.2
645	ok	0.28	0.1	2.20e-02	7.7	7.7	5.1	5.1	-14.9	88.1	-88.9	-279.7	-83.0	-345.4
663	ok	0.28	8.58e-02	1.48e-02	7.7	7.7	5.1	5.1	-42.4	74.5	19.0	-259.1	-6.27e-02	-212.6
681	ok	0.28	3.60e-02	1.11e-02	7.7	7.7	5.1	5.1	-13.9	14.9	26.6	-66.2	60.4	-54.4
700	ok	0.28	2.54e-02	4.06e-03	7.7	7.7	5.1	5.1	10.7	1.7	17.5	-118.9	81.0	4.7

Nodo	x/d	V N/M	ver. rid	Af pr-	Af pr+	Af sec-	Af sec+	N z	N o	N zo	M z	M o	M zo
	0.31	0.34	0.20	10.26	10.26	6.12	5.13	-548.11	-147.43	-172.37	-1128.59	-576.73	-623.21
								110.03	330.62	153.05	173.37	202.03	254.80

Nodo	Stato	Max tau daN/cm2	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr daN/cm	V sec daN/cm
34	ok	0.84						
50	ok	1.18						
66	ok	2.12						
146	ok	2.18						
162	ok	1.67						
178	ok	0.68						
194	ok	1.30						
222	ok	0.51						
238	ok	1.73						
240	ok	2.15						
246	ok	2.40						
248	ok	1.55						
250	ok	1.47						
252	ok	0.89						
281	ok	1.30						
297	ok	1.59						
299	ok	0.79						
305	ok	0.89						
307	ok	1.16						
309	ok	1.84						
311	ok	1.51						
340	ok	1.27						
356	ok	1.37						
358	ok	1.44						
364	ok	1.34						
366	ok	1.08						
368	ok	1.58						
370	ok	1.48						
399	ok	0.84						
415	ok	0.97						
417	ok	1.92						
423	ok	1.91						
425	ok	1.10						
427	ok	1.19						
429	ok	1.02						
465	ok	1.58						
466	ok	1.81						
467	ok Av	5.91	0.05	0.23	1.4	6.6	17.0	78.5
468	ok	2.49						
469	ok	1.30						

SCARICATORE IN VIA PUCCI

470	ok	1.08										
471	ok	5.19										
472	ok Av	7.60	0.07	0.29	2.0	8.4	24.2	100.5				
473	ok	1.96										
474	ok	0.86										
475	ok	0.54										
521	ok	1.64										
537	ok	1.82										
555	ok	4.89										
573	ok	2.59										
591	ok	1.03										
609	ok	1.23										
627	ok Av	5.64	0.14	0.17	4.0	5.0	48.1	59.8				
645	ok Av	5.33	0.05	0.20	1.5	5.9	17.8	70.3				
663	ok	1.43										
681	ok	0.50										
700	ok	0.99										

Nodo	Max tau	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec
	7.60	0.14	0.29	4.01	8.39	48.05	100.50

Parete	H totale	Spessore	H critica	H critica V	L totale	L confinata	Verif. N	Verif. N-M	Fattore V	Diagramma V	Verif. V	Prog. composta
	cm	cm	cm	cm	cm	cm						
9	230.00	20.00	40.00	40.00	325.00	65.00	ok	ok	1.50	SI	ok	SI

Quota	Af conf.	Af std	Af V (ori)	Ver. N	Ver. N/M	Ver. V cls	Ver. V acc	Ver. V acc(7)	Ver. V scorr.	N add	M invil	V invil
cm										daN	daN	daN
-270.0	10d14	14/20	14/30	0.03	5.48e-03	0.05	3.75e-03	0.10	0.05	0.0	1.812e+05	4185.92
-231.7	10d14	14/20	14/30	0.03	5.07e-03	0.05	4.86e-03	0.10	0.05	0.0	1.812e+05	4185.92
-193.3	0d0	14/20	14/30	0.03	3.40e-03	0.02	5.34e-03	0.11	0.0	0.0	1.596e+05	4185.92
-155.0	0d0	14/20	14/30	0.03	2.61e-03	0.02	6.88e-03	0.09	0.0	0.0	1.371e+05	3868.56
-116.7	0d0	14/20	14/30	0.02	2.05e-03	0.02	9.66e-03	0.09	0.0	0.0	1.145e+05	3551.20
-78.3	0d0	14/20	14/30	0.02	1.60e-03	0.02	6.29e-03	0.08	0.0	0.0	9.199e+04	3233.84
-40.0	0d0	14/20	14/30	0.02	1.10e-03	0.01	4.10e-03	0.07	0.0	0.0	6.945e+04	2916.48

Quota	Ver. N	Ver. N/M	Ver. V cls	Ver. V acc	Ver. V acc(7)	Ver. V scorr.
	0.03	5.48e-03	0.05	9.66e-03	0.11	0.05

Quota	N v.N	N v.M/N	M v.M/N	N v.Vcls	V v.Vcls	N v.Vacc	M v. Vacc	V v.Vacc	N v.Vscor	M v.Vscor	V v.Vscor
cm	daN	daN	daN cm	daN	daN	daN	daN cm	daN	daN	daN cm	daN
-270.0	-1.141e+04	-1.090e+04	1.812e+05	-1.090e+04	4169.19	-1.073e+04	5.140e+04	382.95	-1.090e+04	1.812e+05	4169.19
-231.7	-1.162e+04	-1.106e+04	1.679e+05	-1.106e+04	4054.94	-1.104e+04	2.760e+04	497.20	-8107.30	6.447e+04	4017.05
-193.3	-1.124e+04	-1.096e+04	9.509e+04	-1.098e+04	4088.35	-1.062e+04	1.049e+04	549.47	0.0	0.0	0.0
-155.0	-1.074e+04	-1.057e+04	7.305e+04	-1.057e+04	4185.92	-8641.42	4557.13	707.05	0.0	0.0	0.0
-116.7	-1.023e+04	-1.010e+04	5.730e+04	-1.010e+04	4004.11	-8677.87	3710.72	993.24	0.0	0.0	0.0
-78.3	-9685.67	-9628.85	4.450e+04	-9628.85	3484.62	-8628.97	1.045e+04	646.23	0.0	0.0	0.0
-40.0	-9038.47	-8990.20	3.044e+04	-9038.47	2916.48	-8537.56	7349.63	421.02	0.0	0.0	0.0

Quota	Ctg Vcls	Vrsd Vcls	Vrzd Vcls	Ctg Vac	Vrsd Vac	Vrzd Vac	Vdd	Vid	[A s.i.	Incli.	Dist.]	Vfd
cm		daN	daN		daN	daN	daN	daN	cm2	gradi	cm	daN
-270.0	1.00	4169.19	8.465e+04	1.00	1.022e+05	8.463e+04	5.722e+04	3194.10	1.0	35.3	0.0	2.487e+04
-231.7	1.00	4054.94	8.466e+04	1.00	1.022e+05	8.466e+04	5.722e+04	3194.10	1.0	35.3	0.0	2.402e+04
-193.3	1.00	4088.35	2.129e+05	1.00	1.028e+05	2.128e+05	0.0	0.0	0.0	0.0	0.0	0.0
-155.0	1.00	4185.92	2.128e+05	1.00	1.028e+05	2.124e+05	0.0	0.0	0.0	0.0	0.0	0.0
-116.7	1.00	4004.11	2.127e+05	1.00	1.028e+05	2.124e+05	0.0	0.0	0.0	0.0	0.0	0.0
-78.3	1.00	3484.62	2.126e+05	1.00	1.028e+05	2.124e+05	0.0	0.0	0.0	0.0	0.0	0.0
-40.0	1.00	2916.48	2.125e+05	1.00	1.028e+05	2.124e+05	0.0	0.0	0.0	0.0	0.0	0.0

Quota	V[7.4.16]	N	M	V	alfaS	VRd,c	VRd,s	V[7.4.17]	roH	roV	roN
cm		daN	daN cm	daN		daN	daN				
-270.0	0.10	-7519.09	3.950e+04	3902.79	0.05	3.375e+04	4834.03	0.0	5.13e-03	7.70e-03	0.0
-231.7	0.10	-8107.30	6.447e+04	4017.05	0.05	3.433e+04	4834.03	0.0	5.13e-03	7.70e-03	0.0
-193.3	0.11	-8110.60	4.677e+04	3809.49	0.05	3.097e+04	4834.03	0.0	5.13e-03	7.70e-03	0.0
-155.0	0.09	-1.057e+04	7.305e+04	4185.92	0.13	3.340e+04	1.309e+04	0.0	5.13e-03	7.70e-03	0.0
-116.7	0.09	-1.010e+04	5.730e+04	4004.11	0.13	3.294e+04	1.309e+04	0.0	5.13e-03	7.70e-03	0.0
-78.3	0.08	-9628.85	4.450e+04	3484.62	0.13	3.247e+04	1.309e+04	0.0	5.13e-03	7.70e-03	0.0
-40.0	0.07	-9038.47	2.695e+04	2916.48	0.13	3.189e+04	1.247e+04	0.0	5.13e-03	7.70e-03	0.0

Quota	V[7.4.16]	V[7.4.17]
	0.11	0.0

SCARICATORE IN VIA PUCCI

Nodo	Stato	x/d	V N/M	ver. rid	Af pr-	Af pr+Af	sec-Af	sec+	N z daN/cm	N o daN/cm	N zo daN/cm	M z daN	M o daN	M zo daN
49	ok	0.33	5.03e-02	0.0	11.8	11.8	5.1	5.1	55.6	12.4	12.6	304.2	21.6	8.6
65	ok	0.33	0.1	1.15e-02	11.8	11.8	5.1	5.1	-23.4	-3.3	4.8	620.7	125.7	22.4
81	ok	0.28	0.2	1.98e-02	7.7	7.7	5.1	5.1	-57.4	-15.2	6.9	1011.3	202.6	34.4
97	ok	0.28	0.3	2.57e-02	7.7	7.7	5.1	5.1	-77.1	-22.3	9.6	1313.7	266.3	27.1
113	ok	0.28	0.3	2.72e-02	7.7	7.7	5.1	5.1	-79.9	-22.7	-4.0	1430.7	293.4	-7.7
129	ok	0.28	0.3	2.49e-02	7.7	7.7	5.1	5.1	-72.9	-21.0	-3.5	1387.7	282.6	-26.5
145	ok	0.28	0.3	1.96e-02	7.7	7.7	5.1	5.1	-56.0	-15.8	-3.3	1197.8	240.7	-38.0
161	ok	0.28	0.2	1.44e-02	7.7	7.7	5.1	5.1	-41.9	-10.4	-3.5	1001.9	196.8	-31.1
177	ok	0.33	0.1	6.98e-03	11.8	11.8	5.1	5.1	-19.6	-0.1	-3.2	711.1	155.0	-19.9
193	ok	0.33	6.63e-02	0.0	11.8	11.8	5.1	5.1	16.1	8.0	2.2	414.9	113.8	-1.6
209	ok	0.33	5.96e-02	9.79e-05	11.8	11.8	5.1	5.1	61.5	11.5	-14.3	358.6	26.4	-9.2
237	ok	0.33	0.1	7.90e-03	11.8	11.8	5.1	5.1	17.1	-12.4	11.4	86.0	214.6	-32.8
239	ok	0.33	5.32e-02	9.96e-03	11.8	11.8	5.1	5.1	-17.9	-7.4	-14.8	42.1	-8.3	-147.5
241	ok	0.28	6.52e-02	1.77e-02	7.7	7.7	5.1	5.1	-48.9	-4.7	-6.5	70.4	-46.4	-102.9
242	ok	0.28	5.53e-02	2.40e-02	7.7	7.7	5.1	5.1	-70.3	-4.8	-0.9	126.7	4.3	-55.4
243	ok	0.28	5.99e-02	2.64e-02	7.7	7.7	5.1	5.1	-76.9	-5.1	2.2	151.8	26.4	-19.2
244	ok	0.28	5.55e-02	2.46e-02	7.7	7.7	5.1	5.1	-71.1	-5.1	5.0	141.7	20.6	20.8
245	ok	0.28	4.86e-02	1.92e-02	7.7	7.7	5.1	5.1	-53.9	-5.7	5.3	88.9	-41.6	56.3
247	ok	0.28	5.99e-02	1.49e-02	7.7	7.7	5.1	5.1	-39.3	-5.5	6.3	59.2	-43.6	91.8
249	ok	0.33	5.32e-02	8.12e-03	11.8	11.8	5.1	5.1	-17.5	-7.0	7.6	38.1	-22.3	127.8
251	ok	0.33	6.72e-02	6.08e-03	11.8	11.8	5.1	5.1	-2.0	-15.6	-6.1	26.3	137.1	155.4
268	ok	0.33	8.78e-02	1.05e-02	11.8	11.8	5.1	5.1	15.2	-13.6	-24.9	78.6	194.9	-0.6
296	ok	0.28	0.2	1.38e-02	7.7	7.7	5.1	5.1	-19.8	-31.9	13.3	117.7	735.2	-11.2
298	ok	0.28	4.82e-02	9.53e-03	7.7	7.7	5.1	5.1	-12.3	-26.4	4.0	-106.8	51.4	-135.1
300	ok	0.28	9.50e-02	1.47e-02	7.7	7.7	5.1	5.1	-44.0	-6.9	0.5	-269.3	-164.7	-72.2
301	ok	0.28	0.1	2.19e-02	7.7	7.7	5.1	5.1	-67.0	0.6	3.3	-367.2	-143.5	-38.7
302	ok	0.28	0.1	2.48e-02	7.7	7.7	5.1	5.1	-75.9	2.6	4.5	-401.8	-114.5	-11.7
303	ok	0.28	0.1	2.32e-02	7.7	7.7	5.1	5.1	-71.0	1.5	1.1	-396.7	-120.0	14.5
304	ok	0.28	0.1	1.77e-02	7.7	7.7	5.1	5.1	-53.8	-3.3	1.0	-349.6	-172.9	40.5
306	ok	0.28	9.77e-02	1.28e-02	7.7	7.7	5.1	5.1	-38.6	-8.0	0.6	-287.3	-164.7	60.5
308	ok	0.28	6.87e-02	7.38e-03	7.7	7.7	5.1	5.1	-11.2	-19.8	-4.0	-197.5	-67.3	137.9
310	ok	0.28	9.18e-02	9.01e-03	7.7	7.7	5.1	5.1	-13.0	-22.0	-4.0	-22.2	267.0	97.2
327	ok	0.28	0.2	1.32e-02	7.7	7.7	5.1	5.1	-15.6	-23.0	-19.4	48.3	540.9	-1.6
355	ok	0.28	0.2	1.39e-02	7.7	7.7	5.1	5.1	-23.4	-29.8	-0.1	132.8	811.2	-2.4
357	ok	0.28	4.72e-02	1.19e-02	7.7	7.7	5.1	5.1	-10.0	-26.5	7.1	-100.9	89.4	27.2
359	ok	0.28	8.04e-02	1.48e-02	7.7	7.7	5.1	5.1	-39.1	-6.2	11.5	-272.6	-169.1	56.5
360	ok	0.28	0.1	2.14e-02	7.7	7.7	5.1	5.1	-62.3	2.1	8.4	-383.2	-151.4	33.2
361	ok	0.28	0.1	2.44e-02	7.7	7.7	5.1	5.1	-72.4	4.7	4.7	-425.1	-119.1	7.2
362	ok	0.28	0.1	2.30e-02	7.7	7.7	5.1	5.1	-67.9	3.2	-1.9	-418.0	-127.1	-21.0
363	ok	0.28	0.1	1.76e-02	7.7	7.7	5.1	5.1	-50.5	-2.4	-5.7	-357.8	-177.8	-40.9
365	ok	0.28	8.18e-02	1.33e-02	7.7	7.7	5.1	5.1	-36.0	-7.6	-8.5	-282.3	-165.9	-57.9
367	ok	0.28	5.78e-02	1.02e-02	7.7	7.7	5.1	5.1	-19.9	-14.0	-10.2	-166.5	-86.5	-70.5
369	ok	0.28	9.69e-02	8.89e-03	7.7	7.7	5.1	5.1	-11.2	-20.5	-9.0	-14.3	303.9	-25.8
386	ok	0.28	0.2	1.17e-02	7.7	7.7	5.1	5.1	-18.5	-18.8	2.4	63.5	593.8	9.0
414	ok	0.28	0.2	1.00e-02	7.7	7.7	5.1	5.1	-13.9	-19.5	1.8	106.1	597.9	11.3
416	ok	0.28	5.81e-02	1.29e-02	7.7	7.7	5.1	5.1	-8.7	-18.4	12.5	-50.5	82.4	143.5
418	ok	0.28	7.87e-02	1.71e-02	7.7	7.7	5.1	5.1	-42.3	-1.1	18.4	-58.0	-79.0	124.5
419	ok	0.28	8.65e-02	2.26e-02	7.7	7.7	5.1	5.1	-65.2	0.5	11.2	-59.9	-35.2	69.4
420	ok	0.28	8.01e-02	2.51e-02	7.7	7.7	5.1	5.1	-74.7	0.6	4.5	-53.2	2.4	15.0
421	ok	0.28	8.05e-02	2.39e-02	7.7	7.7	5.1	5.1	-70.8	-0.2	-4.1	-55.5	-7.1	-38.0
422	ok	0.28	8.56e-02	1.91e-02	7.7	7.7	5.1	5.1	-53.7	-2.4	-10.5	-61.2	-66.8	-89.0
424	ok	0.28	8.11e-02	1.53e-02	7.7	7.7	5.1	5.1	-38.3	-4.6	-14.9	-49.9	-76.6	-124.2
426	ok	0.28	6.10e-02	1.14e-02	7.7	7.7	5.1	5.1	-17.9	-7.9	-17.6	-26.0	-45.9	-149.4
428	ok	0.28	8.62e-02	7.34e-03	7.7	7.7	5.1	5.1	-11.1	-16.3	-7.4	20.9	254.4	-111.8
445	ok	0.28	0.1	8.55e-03	7.7	7.7	5.1	5.1	-10.7	-14.0	2.1	65.1	452.4	-4.7
510	ok	0.28	6.82e-02	3.61e-03	7.7	7.7	5.1	5.1	36.8	11.9	6.6	57.0	-145.5	18.5
511	ok	0.28	5.35e-02	1.15e-02	7.7	7.7	5.1	5.1	-19.5	3.9	24.2	198.6	16.0	85.2
512	ok	0.28	0.1	1.81e-02	7.7	7.7	5.1	5.1	-49.5	-4.5	12.5	409.7	74.7	53.2
513	ok	0.28	0.1	2.38e-02	7.7	7.7	5.1	5.1	-71.2	-11.2	6.2	610.0	150.3	20.3
514	ok	0.28	0.2	2.62e-02	7.7	7.7	5.1	5.1	-80.1	-14.3	0.7	709.3	192.8	2.0
515	ok	0.28	0.2	2.51e-02	7.7	7.7	5.1	5.1	-76.6	-14.2	-1.0	687.9	183.7	-11.8
516	ok	0.28	0.1	2.05e-02	7.7	7.7	5.1	5.1	-60.9	-11.0	-7.1	548.8	126.4	-36.7
517	ok	0.28	0.1	1.64e-02	7.7	7.7	5.1	5.1	-44.6	-7.4	-15.3	416.1	67.8	-63.6
518	ok	0.28	6.66e-02	1.07e-02	7.7	7.7	5.1	5.1	-20.5	-2.6	-18.7	263.5	33.1	-85.9
519	ok	0.28	5.73e-02	4.52e-03	7.7	7.7	5.1	5.1	14.3	1.9	-11.2	131.6	5.0	-65.5
520	ok	0.28	5.77e-02	4.02e-03	7.7	7.7	5.1	5.1	33.4	3.7	2.8	96.4	-83.1	1.0
536	ok	0.28	4.24e-02	0.0	7.7	7.7	5.1	5.1	54.7	7.8	-8.7	184.8	-72.7	-27.2
554	ok	0.28	0.1	9.75e-03	7.7	7.7	5.1	5.1	-15.8	-12.8	-6.6	601.0	100.6	-143.7
572	ok	0.28	0.3	1.88e-02	7.7	7.7	5.1	5.1	-49.8	-27.2	-6.9	1154.4	233.1	-147.3
590	ok	0.28	0.4	2.51e-02	7.7	7.7	5.1	5.1	-72.1	-38.5	-8.0	1645.4	341.7	-103.2
608	ok	0.28	0.4	2.74e-02	7.7	7.7	5.1	5.1	-80.8	-43.6	-9.1	1877.3	393.5	-34.2
626	ok	0.28	0.4	2.66e-02	7.7	7.7	5.1	5.1	-77.6	-43.0	9.7	1828.4	382.8	57.5
644	ok	0.28	0.3	2.20e-02	7.7	7.7	5.1	5.1	-60.6	-35.4	7.7	1492.5	308.4	121.1
662	ok	0.28	0.3	1.60e-02	7.7	7.7	5.1	5.1	-44.4	-26.8	5.5	1139.1	230.5	138.3
680	ok	0.28	0.2	8.38e-03	7.7	7.7	5.1	5.1	-17.8	-12.5	6.4	689.1	137.7	137.5

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

699	ok	0.28	6.83e-02	6.98e-04	7.7	7.7	5.1	5.1	25.4	3.5	7.6	275.6	26.4	93.0
716	ok	0.28	5.08e-02	0.0	7.7	7.7	5.1	5.1	54.3	11.1	6.4	225.9	-32.7	7.3
Nodo		x/d	V N/M	ver. rid	Af pr-	Af pr+Af	sec-Af	sec+	N z	N o	N zo	M z	M o	M zo
		0.33	0.39	0.03	11.84	11.84	5.13	5.13	-80.83	-43.62	-24.89	-425.09	-177.76	-149.42
									61.48	12.38	24.18	1877.27	811.20	155.44
Nodo	Stato	Max tau		Ver V pr		Ver V sec		Af V pr		Af V sec		V pr		V sec
		daN/cm2										daN/cm		daN/cm
49	ok	1.11												
65	ok	1.15												
81	ok	2.08												
97	ok	2.52												
113	ok	2.68												
129	ok	2.59												
145	ok	2.37												
161	ok	2.19												
177	ok	1.60												
193	ok	0.98												
209	ok	1.22												
237	ok	0.96												
239	ok	2.01												
241	ok	2.34												
242	ok	2.69												
243	ok	2.74												
244	ok	2.74												
245	ok	2.51												
247	ok	2.19												
249	ok	1.82												
251	ok	1.51												
268	ok	1.67												
296	ok	1.89												
298	ok	1.83												
300	ok	1.30												
301	ok	1.30												
302	ok	1.30												
303	ok	1.38												
304	ok	1.37												
306	ok	1.14												
308	ok	1.37												
310	ok	1.99												
327	ok	2.01												
355	ok	1.93												
357	ok	1.82												
359	ok	1.29												
360	ok	1.01												
361	ok	0.98												
362	ok	1.02												
363	ok	1.05												
365	ok	1.09												
367	ok	1.46												
369	ok	1.90												
386	ok	1.93												
414	ok	1.41												
416	ok	1.33												
418	ok	1.16												
419	ok	1.43												
420	ok	1.53												
421	ok	1.52												
422	ok	1.38												
424	ok	1.07												
426	ok	1.17												
428	ok	1.35												
445	ok	1.71												
510	ok	1.41												
511	ok	1.85												
512	ok	2.17												
513	ok	2.27												
514	ok	2.17												
515	ok	2.21												
516	ok	2.20												
517	ok	2.05												
518	ok	1.76												
519	ok	1.20												
520	ok	1.18												
536	ok	1.26												
554	ok	1.16												
572	ok	1.77												

SCARICATORE IN VIA PUCCI

590	ok	2.17						
608	ok	2.30						
626	ok	2.28						
644	ok	2.07						
662	ok	1.70						
680	ok	1.11						
699	ok	0.61						
716	ok	1.36						
Nodo		Max tau 2.74	Ver V pr	Ver V sec	Af V pr	Af V sec	V pr	V sec

STATI LIMITE D' ESERCIZIO

LEGENDA TABELLA STATI LIMITE D' ESERCIZIO

In tabella vengono riportati i valori di interesse per il controllo degli stati limite d'esercizio.

In particolare vengono riportati, in relazione al tipo di elemento strutturale, i risultati relativi alle tre categorie di combinazione considerate:

Combinazioni rare

Combinazioni frequenti

Combinazioni quasi permanenti.

I valori di interesse sono i seguenti:

rRfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni rare [normalizzato a 1]
rRfyk	rapporto tra la massima tensione nell'acciaio e la tensione fyk in combinazioni rare [normalizzato a 1]
rPfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni quasi permanenti [normalizzato a 1]
wR	apertura caratteristica delle fessure in combinazioni rare [mm]
wF	apertura caratteristica delle fessure in combinazioni frequenti [mm]
wP	apertura caratteristica delle fessure in combinazioni quasi permanenti [mm]
dR	massima deformazione in combinazioni rare
dF	massima deformazione in combinazioni frequenti
dP	massima deformazione in combinazioni quasi permanenti

Per ognuno dei nove valori soprariportati viene indicata (Rif.cmb) la combinazione in cui si è verificato.

In relazione al tipo di elemento strutturale i valori sono selezionati nel modo seguente:

pilastrati	rRfck	rRfyk	rPfck	per sezioni significative
travi	rRfck	rRfyk	rPfck	per sezioni significative
	wR	wF	wP	per sezioni significative
	dR	dF	dP	massimi in campata
setti e gusci	rRfck	rRfyk	rPfck	massimi nei nodi dell'elemento
	wR	wF	wP	massimi nei nodi dell'elemento

Si precisa che i valori di massima deformazione per travi sono riferiti al piano verticale (piano locale 1-2 con momenti flettenti 3-3).

Setto	rRfck	rRfyk	rPfck	Rif. cmb	wR mm	wF mm	wP mm	Rif. cmb
26	0.13	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0
27	0.11	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0
28	0.09	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
29	0.06	0.04	0.0	74,74,0	0.0	0.0	0.0	0,0,0
30	0.04	0.03	0.0	73,73,0	0.0	0.0	0.0	0,0,0
31	0.04	0.08	0.0	74,76,0	0.0	0.0	0.0	0,0,0

SCARICATORE IN VIA PUCCI

32	0.04	0.18	0.0	73,75,0	0.0	0.0	0.0	0,0,0
33	0.07	0.19	0.0	76,74,0	0.0	0.0	0.0	0,0,0
34	0.04	0.07	0.0	76,74,0	0.0	0.0	0.0	0,0,0
35	0.05	0.05	0.0	73,74,0	0.0	0.0	0.0	0,0,0
36	0.04	0.02	0.0	76,73,0	0.0	0.0	0.0	0,0,0
37	0.05	0.03	0.0	73,73,0	0.0	0.0	0.0	0,0,0
38	0.04	0.05	0.0	76,73,0	0.0	0.0	0.0	0,0,0
39	0.04	0.05	0.0	73,76,0	0.0	0.0	0.0	0,0,0
40	0.04	0.05	0.0	76,76,0	0.0	0.0	0.0	0,0,0
41	0.05	0.03	0.0	73,75,0	0.0	0.0	0.0	0,0,0
42	0.05	0.04	0.0	73,73,0	0.0	0.0	0.0	0,0,0
43	0.05	0.04	0.0	73,74,0	0.0	0.0	0.0	0,0,0
44	0.04	0.05	0.0	74,74,0	0.0	0.0	0.0	0,0,0
195	0.08	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
196	0.13	0.11	0.0	74,73,0	0.0	0.0	0.0	0,0,0
197	0.18	0.20	0.0	73,73,0	0.0	0.0	0.0	0,0,0
198	0.20	0.22	0.0	73,73,0	0.0	0.0	0.0	0,0,0
199	0.21	0.24	0.0	73,73,0	0.0	0.0	0.0	0,0,0
200	0.21	0.24	0.0	73,73,0	0.0	0.0	0.0	0,0,0
201	0.21	0.24	0.0	73,73,0	0.0	0.0	0.0	0,0,0
202	0.21	0.24	0.0	73,73,0	0.0	0.0	0.0	0,0,0
203	0.21	0.23	0.0	73,73,0	0.0	0.0	0.0	0,0,0
204	0.20	0.23	0.0	73,73,0	0.0	0.0	0.0	0,0,0
205	0.18	0.21	0.0	73,73,0	0.0	0.0	0.0	0,0,0
206	0.13	0.13	0.0	74,73,0	0.0	0.0	0.0	0,0,0
207	0.12	0.11	0.0	74,73,0	0.0	0.0	0.0	0,0,0
208	0.09	0.09	0.0	74,73,0	0.0	0.0	0.0	0,0,0
209	0.06	0.09	0.0	74,74,0	0.0	0.0	0.0	0,0,0
210	0.05	0.13	0.0	74,74,0	0.0	0.0	0.0	0,0,0
211	0.07	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
212	0.11	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
213	0.14	0.15	0.0	74,73,0	0.0	0.0	0.0	0,0,0
214	0.18	0.21	0.0	74,75,0	0.0	0.0	0.0	0,0,0
215	0.20	0.24	0.0	74,75,0	0.0	0.0	0.0	0,0,0
216	0.20	0.24	0.0	74,75,0	0.0	0.0	0.0	0,0,0
217	0.19	0.23	0.0	74,75,0	0.0	0.0	0.0	0,0,0
218	0.17	0.20	0.0	74,75,0	0.0	0.0	0.0	0,0,0
219	0.14	0.10	0.0	76,75,0	0.0	0.0	0.0	0,0,0
220	0.14	0.17	0.0	74,75,0	0.0	0.0	0.0	0,0,0
221	0.07	0.10	0.0	76,76,0	0.0	0.0	0.0	0,0,0
222	0.09	0.08	0.0	74,76,0	0.0	0.0	0.0	0,0,0
223	0.05	0.17	0.0	76,76,0	0.0	0.0	0.0	0,0,0
224	0.05	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
225	0.10	0.17	0.0	76,76,0	0.0	0.0	0.0	0,0,0
226	0.15	0.15	0.0	76,75,0	0.0	0.0	0.0	0,0,0
227	0.17	0.17	0.0	76,75,0	0.0	0.0	0.0	0,0,0
228	0.18	0.18	0.0	76,75,0	0.0	0.0	0.0	0,0,0
229	0.18	0.18	0.0	76,75,0	0.0	0.0	0.0	0,0,0
230	0.18	0.16	0.0	76,75,0	0.0	0.0	0.0	0,0,0
231	0.18	0.15	0.0	74,76,0	0.0	0.0	0.0	0,0,0
232	0.14	0.13	0.0	74,74,0	0.0	0.0	0.0	0,0,0
233	0.14	0.07	0.0	74,74,0	0.0	0.0	0.0	0,0,0
234	0.12	0.06	0.0	74,74,0	0.0	0.0	0.0	0,0,0
235	0.09	0.03	0.0	74,74,0	0.0	0.0	0.0	0,0,0
236	0.08	0.03	0.0	74,73,0	0.0	0.0	0.0	0,0,0
237	0.08	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0
238	0.07	0.09	0.0	74,74,0	0.0	0.0	0.0	0,0,0
239	0.06	0.09	0.0	74,74,0	0.0	0.0	0.0	0,0,0
240	0.06	0.12	0.0	73,73,0	0.0	0.0	0.0	0,0,0
241	0.07	0.12	0.0	76,73,0	0.0	0.0	0.0	0,0,0
242	0.04	0.05	0.0	73,73,0	0.0	0.0	0.0	0,0,0
243	0.04	0.04	0.0	75,73,0	0.0	0.0	0.0	0,0,0
244	0.03	0.04	0.0	75,73,0	0.0	0.0	0.0	0,0,0
245	0.04	0.03	0.0	75,75,0	0.0	0.0	0.0	0,0,0
246	0.07	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
247	0.07	0.08	0.0	73,73,0	0.0	0.0	0.0	0,0,0
248	0.07	0.09	0.0	74,74,0	0.0	0.0	0.0	0,0,0
249	0.03	0.02	0.0	73,73,0	0.0	0.0	0.0	0,0,0
250	0.03	0.01	0.0	73,74,0	0.0	0.0	0.0	0,0,0
251	0.03	0.02	0.0	74,74,0	0.0	0.0	0.0	0,0,0
252	0.07	0.08	0.0	73,73,0	0.0	0.0	0.0	0,0,0
253	0.14	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
254	0.09	0.11	0.0	75,75,0	0.0	0.0	0.0	0,0,0
255	0.06	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
256	0.06	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
257	0.07	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
258	0.07	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
259	0.07	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
260	0.07	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

261	0.07	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
262	0.07	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
263	0.07	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
264	0.07	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
265	0.06	0.05	0.0	75,73,0	0.0	0.0	0.0	0,0,0
266	0.06	0.05	0.0	75,73,0	0.0	0.0	0.0	0,0,0
267	0.04	0.04	0.0	73,73,0	0.0	0.0	0.0	0,0,0
268	0.12	0.16	0.0	75,75,0	0.0	0.0	0.0	0,0,0
269	0.09	0.11	0.0	75,73,0	0.0	0.0	0.0	0,0,0
270	0.12	0.15	0.0	75,75,0	0.0	0.0	0.0	0,0,0
271	0.05	0.06	0.0	74,73,0	0.0	0.0	0.0	0,0,0
272	0.06	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
273	0.07	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
274	0.07	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
275	0.07	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
276	0.07	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
277	0.07	0.08	0.0	75,75,0	0.0	0.0	0.0	0,0,0
278	0.05	0.06	0.0	76,75,0	0.0	0.0	0.0	0,0,0
279	0.06	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
280	0.04	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
281	0.04	0.05	0.0	73,75,0	0.0	0.0	0.0	0,0,0
282	0.09	0.12	0.0	73,75,0	0.0	0.0	0.0	0,0,0
283	0.09	0.12	0.0	75,75,0	0.0	0.0	0.0	0,0,0
284	0.08	0.11	0.0	73,76,0	0.0	0.0	0.0	0,0,0
285	0.05	0.07	0.0	75,76,0	0.0	0.0	0.0	0,0,0
286	0.06	0.05	0.0	75,73,0	0.0	0.0	0.0	0,0,0
287	0.06	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
288	0.06	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
289	0.06	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
290	0.05	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
291	0.07	0.11	0.0	75,73,0	0.0	0.0	0.0	0,0,0
292	0.06	0.06	0.0	74,74,0	0.0	0.0	0.0	0,0,0
293	0.02	0.01	0.0	74,74,0	0.0	0.0	0.0	0,0,0
294	0.03	0.02	0.0	74,74,0	0.0	0.0	0.0	0,0,0
295	0.03	0.01	0.0	74,74,0	0.0	0.0	0.0	0,0,0
296	0.02	0.01	0.0	74,74,0	0.0	0.0	0.0	0,0,0
297	0.06	0.06	0.0	74,74,0	0.0	0.0	0.0	0,0,0
298	0.01	0.04	0.0	76,76,0	0.0	0.0	0.0	0,0,0
299	0.08	0.10	0.0	75,75,0	0.0	0.0	0.0	0,0,0
300	0.08	0.19	0.0	73,73,0	0.0	0.0	0.0	0,0,0
301	0.06	0.08	0.0	76,74,0	0.0	0.0	0.0	0,0,0
302	0.04	0.10	0.0	75,73,0	0.0	0.0	0.0	0,0,0
303	0.04	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
304	0.04	0.07	0.0	76,73,0	0.0	0.0	0.0	0,0,0
305	0.04	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
306	0.07	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
307	0.08	0.09	0.0	73,73,0	0.0	0.0	0.0	0,0,0
308	0.07	0.09	0.0	74,74,0	0.0	0.0	0.0	0,0,0
309	0.03	0.02	0.0	73,73,0	0.0	0.0	0.0	0,0,0
310	0.03	0.01	0.0	73,73,0	0.0	0.0	0.0	0,0,0
311	0.03	0.02	0.0	74,74,0	0.0	0.0	0.0	0,0,0
312	0.08	0.09	0.0	73,73,0	0.0	0.0	0.0	0,0,0
313	0.09	0.13	0.0	75,75,0	0.0	0.0	0.0	0,0,0
314	0.06	0.06	0.0	75,76,0	0.0	0.0	0.0	0,0,0
315	0.07	0.06	0.0	73,73,0	0.0	0.0	0.0	0,0,0
316	0.08	0.07	0.0	75,73,0	0.0	0.0	0.0	0,0,0
317	0.09	0.08	0.0	75,75,0	0.0	0.0	0.0	0,0,0
318	0.09	0.08	0.0	75,75,0	0.0	0.0	0.0	0,0,0
319	0.09	0.09	0.0	75,75,0	0.0	0.0	0.0	0,0,0
320	0.09	0.09	0.0	75,75,0	0.0	0.0	0.0	0,0,0
321	0.09	0.09	0.0	75,75,0	0.0	0.0	0.0	0,0,0
322	0.08	0.08	0.0	75,75,0	0.0	0.0	0.0	0,0,0
323	0.07	0.08	0.0	75,75,0	0.0	0.0	0.0	0,0,0
324	0.06	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
325	0.05	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
326	0.04	0.03	0.0	73,76,0	0.0	0.0	0.0	0,0,0
327	0.13	0.18	0.0	75,75,0	0.0	0.0	0.0	0,0,0
328	0.09	0.12	0.0	75,75,0	0.0	0.0	0.0	0,0,0
329	0.13	0.18	0.0	75,75,0	0.0	0.0	0.0	0,0,0
330	0.05	0.04	0.0	76,76,0	0.0	0.0	0.0	0,0,0
331	0.06	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
332	0.07	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
333	0.08	0.09	0.0	75,75,0	0.0	0.0	0.0	0,0,0
334	0.08	0.08	0.0	75,75,0	0.0	0.0	0.0	0,0,0
335	0.08	0.08	0.0	75,75,0	0.0	0.0	0.0	0,0,0
336	0.07	0.08	0.0	75,75,0	0.0	0.0	0.0	0,0,0
337	0.05	0.03	0.0	76,76,0	0.0	0.0	0.0	0,0,0
338	0.06	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
339	0.05	0.06	0.0	73,75,0	0.0	0.0	0.0	0,0,0

SCARICATORE IN VIA PUCCI

340	0.05	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
341	0.09	0.12	0.0	75,75,0	0.0	0.0	0.0	0,0,0
342	0.10	0.14	0.0	75,75,0	0.0	0.0	0.0	0,0,0
343	0.09	0.12	0.0	75,73,0	0.0	0.0	0.0	0,0,0
344	0.05	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
345	0.07	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
346	0.07	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
347	0.07	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
348	0.06	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
349	0.05	0.06	0.0	75,73,0	0.0	0.0	0.0	0,0,0
350	0.08	0.12	0.0	75,75,0	0.0	0.0	0.0	0,0,0
351	0.02	0.01	0.0	74,74,0	0.0	0.0	0.0	0,0,0
352	0.02	0.01	0.0	74,74,0	0.0	0.0	0.0	0,0,0
353	0.02	0.01	0.0	74,74,0	0.0	0.0	0.0	0,0,0
354	0.02	0.01	0.0	74,74,0	0.0	0.0	0.0	0,0,0
355	0.02	0.01	0.0	74,74,0	0.0	0.0	0.0	0,0,0
356	0.04	0.03	0.0	74,74,0	0.0	0.0	0.0	0,0,0
357	0.01	8.41e-03	0.0	76,76,0	0.0	0.0	0.0	0,0,0
358	0.09	0.12	0.0	75,75,0	0.0	0.0	0.0	0,0,0
359	0.08	0.19	0.0	73,75,0	0.0	0.0	0.0	0,0,0
360	0.05	0.08	0.0	74,76,0	0.0	0.0	0.0	0,0,0
361	0.04	0.11	0.0	76,75,0	0.0	0.0	0.0	0,0,0
362	0.04	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
363	0.04	0.07	0.0	76,73,0	0.0	0.0	0.0	0,0,0
364	0.04	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
365	0.07	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
366	0.07	0.09	0.0	73,75,0	0.0	0.0	0.0	0,0,0
367	0.07	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
368	0.03	0.02	0.0	73,74,0	0.0	0.0	0.0	0,0,0
369	0.03	0.01	0.0	73,74,0	0.0	0.0	0.0	0,0,0
370	0.03	0.01	0.0	74,74,0	0.0	0.0	0.0	0,0,0
371	0.07	0.09	0.0	73,73,0	0.0	0.0	0.0	0,0,0
372	0.09	0.12	0.0	75,75,0	0.0	0.0	0.0	0,0,0
373	0.05	0.06	0.0	73,76,0	0.0	0.0	0.0	0,0,0
374	0.07	0.06	0.0	73,73,0	0.0	0.0	0.0	0,0,0
375	0.08	0.08	0.0	75,73,0	0.0	0.0	0.0	0,0,0
376	0.09	0.08	0.0	75,75,0	0.0	0.0	0.0	0,0,0
377	0.09	0.09	0.0	75,75,0	0.0	0.0	0.0	0,0,0
378	0.09	0.09	0.0	75,75,0	0.0	0.0	0.0	0,0,0
379	0.09	0.09	0.0	75,75,0	0.0	0.0	0.0	0,0,0
380	0.09	0.09	0.0	75,75,0	0.0	0.0	0.0	0,0,0
381	0.08	0.09	0.0	75,75,0	0.0	0.0	0.0	0,0,0
382	0.07	0.08	0.0	75,75,0	0.0	0.0	0.0	0,0,0
383	0.06	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
384	0.05	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
385	0.04	0.04	0.0	76,75,0	0.0	0.0	0.0	0,0,0
386	0.13	0.17	0.0	75,75,0	0.0	0.0	0.0	0,0,0
387	0.09	0.11	0.0	75,75,0	0.0	0.0	0.0	0,0,0
388	0.13	0.18	0.0	75,75,0	0.0	0.0	0.0	0,0,0
389	0.06	0.06	0.0	76,75,0	0.0	0.0	0.0	0,0,0
390	0.05	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
391	0.07	0.08	0.0	75,75,0	0.0	0.0	0.0	0,0,0
392	0.08	0.09	0.0	75,75,0	0.0	0.0	0.0	0,0,0
393	0.08	0.09	0.0	75,75,0	0.0	0.0	0.0	0,0,0
394	0.08	0.09	0.0	75,75,0	0.0	0.0	0.0	0,0,0
395	0.07	0.08	0.0	75,75,0	0.0	0.0	0.0	0,0,0
396	0.05	0.04	0.0	74,73,0	0.0	0.0	0.0	0,0,0
397	0.05	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
398	0.05	0.05	0.0	73,73,0	0.0	0.0	0.0	0,0,0
399	0.05	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
400	0.09	0.11	0.0	73,73,0	0.0	0.0	0.0	0,0,0
401	0.10	0.13	0.0	75,75,0	0.0	0.0	0.0	0,0,0
402	0.09	0.12	0.0	75,73,0	0.0	0.0	0.0	0,0,0
403	0.05	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
404	0.07	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
405	0.07	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
406	0.07	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
407	0.06	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
408	0.04	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
409	0.08	0.13	0.0	75,75,0	0.0	0.0	0.0	0,0,0
410	0.05	0.06	0.0	76,74,0	0.0	0.0	0.0	0,0,0
411	0.03	0.03	0.0	76,74,0	0.0	0.0	0.0	0,0,0
412	0.02	0.03	0.0	74,74,0	0.0	0.0	0.0	0,0,0
413	0.02	0.03	0.0	74,76,0	0.0	0.0	0.0	0,0,0
414	0.02	0.01	0.0	74,76,0	0.0	0.0	0.0	0,0,0
415	0.04	0.05	0.0	76,76,0	0.0	0.0	0.0	0,0,0
416	0.02	0.02	0.0	76,76,0	0.0	0.0	0.0	0,0,0
417	0.09	0.12	0.0	75,75,0	0.0	0.0	0.0	0,0,0
418	0.08	0.20	0.0	75,75,0	0.0	0.0	0.0	0,0,0

SCARICATORE IN VIA PUCCI

419	0.03	0.07	0.0	74,76,0	0.0	0.0	0.0	0,0,0
420	0.04	0.11	0.0	73,75,0	0.0	0.0	0.0	0,0,0
421	0.04	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
422	0.03	0.06	0.0	76,75,0	0.0	0.0	0.0	0,0,0
423	0.04	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
424	0.06	0.07	0.0	74,74,0	0.0	0.0	0.0	0,0,0
425	0.06	0.08	0.0	75,75,0	0.0	0.0	0.0	0,0,0
426	0.06	0.07	0.0	74,74,0	0.0	0.0	0.0	0,0,0
427	0.02	0.01	0.0	73,74,0	0.0	0.0	0.0	0,0,0
428	0.02	0.01	0.0	73,74,0	0.0	0.0	0.0	0,0,0
429	0.02	0.01	0.0	74,74,0	0.0	0.0	0.0	0,0,0
430	0.06	0.07	0.0	75,75,0	0.0	0.0	0.0	0,0,0
431	0.07	0.06	0.0	74,74,0	0.0	0.0	0.0	0,0,0
432	0.10	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
433	0.11	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
434	0.07	0.10	0.0	73,74,0	0.0	0.0	0.0	0,0,0
435	0.12	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
436	0.11	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
437	0.08	0.08	0.0	74,76,0	0.0	0.0	0.0	0,0,0
438	0.06	0.19	0.0	75,76,0	0.0	0.0	0.0	0,0,0
439	0.06	0.17	0.0	75,76,0	0.0	0.0	0.0	0,0,0
440	0.16	0.14	0.0	76,76,0	0.0	0.0	0.0	0,0,0
441	0.13	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0
442	0.04	0.05	0.0	73,74,0	0.0	0.0	0.0	0,0,0
443	0.07	0.09	0.0	73,74,0	0.0	0.0	0.0	0,0,0
444	0.09	0.14	0.0	76,76,0	0.0	0.0	0.0	0,0,0
445	0.09	0.13	0.0	76,76,0	0.0	0.0	0.0	0,0,0
446	0.06	0.14	0.0	75,75,0	0.0	0.0	0.0	0,0,0
447	0.03	0.08	0.0	75,75,0	0.0	0.0	0.0	0,0,0
448	0.02	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
449	0.04	0.05	0.0	74,74,0	0.0	0.0	0.0	0,0,0
450	0.04	0.05	0.0	74,74,0	0.0	0.0	0.0	0,0,0
451	0.02	0.01	0.0	75,74,0	0.0	0.0	0.0	0,0,0
452	0.02	0.01	0.0	73,76,0	0.0	0.0	0.0	0,0,0
453	0.02	0.01	0.0	74,76,0	0.0	0.0	0.0	0,0,0
454	0.05	0.05	0.0	75,75,0	0.0	0.0	0.0	0,0,0
455	0.07	0.09	0.0	76,76,0	0.0	0.0	0.0	0,0,0
456	0.04	0.05	0.0	76,76,0	0.0	0.0	0.0	0,0,0
457	0.05	0.06	0.0	75,75,0	0.0	0.0	0.0	0,0,0
458	0.10	0.06	0.0	76,76,0	0.0	0.0	0.0	0,0,0
459	0.11	0.07	0.0	76,76,0	0.0	0.0	0.0	0,0,0
460	0.05	0.09	0.0	76,76,0	0.0	0.0	0.0	0,0,0
461	0.03	0.04	0.0	75,75,0	0.0	0.0	0.0	0,0,0
462	0.12	0.08	0.0	76,76,0	0.0	0.0	0.0	0,0,0
463	0.12	0.09	0.0	76,76,0	0.0	0.0	0.0	0,0,0
464	0.05	0.07	0.0	76,76,0	0.0	0.0	0.0	0,0,0
465	0.13	0.09	0.0	76,76,0	0.0	0.0	0.0	0,0,0
466	0.03	0.04	0.0	74,76,0	0.0	0.0	0.0	0,0,0
467	0.03	0.04	0.0	75,75,0	0.0	0.0	0.0	0,0,0
468	0.12	0.08	0.0	76,76,0	0.0	0.0	0.0	0,0,0
469	0.11	0.08	0.0	76,76,0	0.0	0.0	0.0	0,0,0
470	0.06	0.11	0.0	76,76,0	0.0	0.0	0.0	0,0,0
471	0.11	0.08	0.0	76,76,0	0.0	0.0	0.0	0,0,0
472	0.03	0.06	0.0	74,76,0	0.0	0.0	0.0	0,0,0
473	0.09	0.06	0.0	76,75,0	0.0	0.0	0.0	0,0,0
474	0.03	0.06	0.0	76,76,0	0.0	0.0	0.0	0,0,0
475	0.07	0.06	0.0	76,75,0	0.0	0.0	0.0	0,0,0
476	0.06	0.05	0.0	76,75,0	0.0	0.0	0.0	0,0,0
477	0.04	0.04	0.0	76,73,0	0.0	0.0	0.0	0,0,0
478	0.07	0.09	0.0	75,75,0	0.0	0.0	0.0	0,0,0
479	0.10	0.13	0.0	75,75,0	0.0	0.0	0.0	0,0,0
480	0.10	0.13	0.0	75,75,0	0.0	0.0	0.0	0,0,0
481	0.05	0.06	0.0	74,76,0	0.0	0.0	0.0	0,0,0
482	0.07	0.05	0.0	74,76,0	0.0	0.0	0.0	0,0,0
483	0.08	0.04	0.0	74,73,0	0.0	0.0	0.0	0,0,0
484	0.08	0.04	0.0	74,75,0	0.0	0.0	0.0	0,0,0
485	0.08	0.04	0.0	76,73,0	0.0	0.0	0.0	0,0,0
486	0.06	0.05	0.0	76,76,0	0.0	0.0	0.0	0,0,0
487	0.05	0.06	0.0	76,76,0	0.0	0.0	0.0	0,0,0
488	0.05	0.07	0.0	75,76,0	0.0	0.0	0.0	0,0,0
489	0.07	0.10	0.0	75,75,0	0.0	0.0	0.0	0,0,0
490	0.17	0.19	0.0	74,74,0	0.0	0.0	0.0	0,0,0
491	0.33	0.37	0.0	74,74,0	0.0	0.0	0.0	0,0,0
492	0.31	0.34	0.0	74,74,0	0.0	0.0	0.0	0,0,0
493	0.05	0.11	0.0	76,74,0	0.0	0.0	0.0	0,0,0
494	0.35	0.39	0.0	74,74,0	0.06	0.0	0.0	74,0,0
495	0.38	0.43	0.0	74,74,0	0.07	0.0	0.0	74,0,0
496	0.32	0.34	0.0	74,74,0	0.0	0.0	0.0	0,0,0
497	0.10	0.20	0.0	76,76,0	0.0	0.0	0.0	0,0,0

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

SCARICATORE IN VIA PUCCI

498	0.10	0.22	0.0	76,76,0	0.0	0.0	0.0	0,0,0
499	0.11	0.31	0.0	76,76,0	0.0	0.0	0.0	0,0,0
500	0.11	0.50	0.0	76,74,0	0.0	0.0	0.0	0,0,0
501	0.06	0.64	0.0	76,74,0	0.0	0.0	0.0	0,0,0
502	0.05	0.64	0.0	74,76,0	0.0	0.0	0.0	0,0,0
503	0.17	0.62	0.0	74,76,0	0.0	0.0	0.0	0,0,0
504	0.15	0.42	0.0	74,76,0	0.0	0.0	0.0	0,0,0
505	0.09	0.30	0.0	74,74,0	0.0	0.0	0.0	0,0,0
506	0.05	0.16	0.0	74,74,0	0.0	0.0	0.0	0,0,0
507	0.03	0.08	0.0	73,74,0	0.0	0.0	0.0	0,0,0
508	0.12	0.14	0.0	74,74,0	0.0	0.0	0.0	0,0,0
509	0.09	0.13	0.0	76,76,0	0.0	0.0	0.0	0,0,0
510	0.03	0.07	0.0	76,74,0	0.0	0.0	0.0	0,0,0
511	0.03	0.07	0.0	76,74,0	0.0	0.0	0.0	0,0,0
512	0.03	0.04	0.0	76,75,0	0.0	0.0	0.0	0,0,0
513	0.02	0.02	0.0	74,75,0	0.0	0.0	0.0	0,0,0
514	0.02	0.03	0.0	74,74,0	0.0	0.0	0.0	0,0,0
515	0.03	0.03	0.0	76,74,0	0.0	0.0	0.0	0,0,0
516	0.03	0.03	0.0	76,75,0	0.0	0.0	0.0	0,0,0
517	0.02	0.03	0.0	75,75,0	0.0	0.0	0.0	0,0,0
518	0.02	0.03	0.0	73,75,0	0.0	0.0	0.0	0,0,0
519	0.20	0.21	0.0	76,76,0	0.0	0.0	0.0	0,0,0
520	0.19	0.13	0.0	74,76,0	0.0	0.0	0.0	0,0,0
521	0.02	0.03	0.0	75,75,0	0.0	0.0	0.0	0,0,0
522	0.26	0.28	0.0	76,76,0	0.0	0.0	0.0	0,0,0
523	0.29	0.31	0.0	76,76,0	0.0	0.0	0.0	0,0,0
524	0.22	0.17	0.0	74,74,0	0.0	0.0	0.0	0,0,0
525	0.02	0.03	0.0	76,75,0	0.0	0.0	0.0	0,0,0
526	0.31	0.33	0.0	76,76,0	0.0	0.0	0.0	0,0,0
527	0.31	0.34	0.0	76,76,0	0.0	0.0	0.0	0,0,0
528	0.21	0.16	0.0	74,74,0	0.0	0.0	0.0	0,0,0
529	0.31	0.33	0.0	76,76,0	0.0	0.0	0.0	0,0,0
530	0.13	0.07	0.0	76,76,0	0.0	0.0	0.0	0,0,0
531	0.03	0.05	0.0	76,74,0	0.0	0.0	0.0	0,0,0
532	0.30	0.32	0.0	76,76,0	0.0	0.0	0.0	0,0,0
533	0.29	0.31	0.0	76,76,0	0.0	0.0	0.0	0,0,0
534	0.10	0.14	0.0	76,76,0	0.0	0.0	0.0	0,0,0
535	0.28	0.30	0.0	76,76,0	0.0	0.0	0.0	0,0,0
536	0.04	0.06	0.0	76,74,0	0.0	0.0	0.0	0,0,0
537	0.24	0.26	0.0	76,76,0	0.0	0.0	0.0	0,0,0
538	0.12	0.14	0.0	76,76,0	0.0	0.0	0.0	0,0,0
539	0.20	0.22	0.0	76,76,0	0.0	0.0	0.0	0,0,0
540	0.18	0.20	0.0	76,76,0	0.0	0.0	0.0	0,0,0
541	0.13	0.15	0.0	76,76,0	0.0	0.0	0.0	0,0,0
542	0.10	0.12	0.0	76,76,0	0.0	0.0	0.0	0,0,0
543	0.10	0.12	0.0	76,76,0	0.0	0.0	0.0	0,0,0
544	0.08	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0
545	0.15	0.15	0.0	74,74,0	0.0	0.0	0.0	0,0,0
546	0.22	0.23	0.0	74,74,0	0.0	0.0	0.0	0,0,0
547	0.25	0.26	0.0	74,74,0	0.0	0.0	0.0	0,0,0
548	0.25	0.26	0.0	74,74,0	0.0	0.0	0.0	0,0,0
549	0.25	0.26	0.0	76,76,0	0.0	0.0	0.0	0,0,0
550	0.20	0.21	0.0	74,74,0	0.0	0.0	0.0	0,0,0
551	0.16	0.17	0.0	74,74,0	0.0	0.0	0.0	0,0,0
552	0.09	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
553	0.04	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0

Setto	rRfck	rRfyk	rPfck	wR	wF	wP
	0.38	0.64	0.0	0.07	0.0	0.0

Guscio	rRfck	rRfyk	rPfck	Rif. cmb	wR mm	wF mm	wP mm	Rif. cmb
1	9.67e-03	0.05	0.0	76,76,0	0.0	0.0	0.0	0,0,0
2	0.02	0.05	0.0	76,76,0	0.0	0.0	0.0	0,0,0
3	0.02	0.04	0.0	76,74,0	0.0	0.0	0.0	0,0,0
4	0.02	0.04	0.0	76,76,0	0.0	0.0	0.0	0,0,0
5	0.01	0.04	0.0	76,76,0	0.0	0.0	0.0	0,0,0
6	9.31e-03	0.03	0.0	76,74,0	0.0	0.0	0.0	0,0,0
7	0.02	0.04	0.0	76,76,0	0.0	0.0	0.0	0,0,0
8	0.02	0.05	0.0	76,76,0	0.0	0.0	0.0	0,0,0
9	0.01	0.04	0.0	76,76,0	0.0	0.0	0.0	0,0,0
10	0.01	0.04	0.0	76,76,0	0.0	0.0	0.0	0,0,0
11	0.01	0.06	0.0	76,74,0	0.0	0.0	0.0	0,0,0
12	0.02	0.05	0.0	76,76,0	0.0	0.0	0.0	0,0,0
13	0.02	0.05	0.0	76,76,0	0.0	0.0	0.0	0,0,0
14	0.02	0.06	0.0	76,76,0	0.0	0.0	0.0	0,0,0
15	0.01	0.06	0.0	76,74,0	0.0	0.0	0.0	0,0,0
16	0.01	0.04	0.0	76,76,0	0.0	0.0	0.0	0,0,0

SCARICATORE IN VIA PUCCI

17	0.02	0.06	0.0	76,76,0	0.0	0.0	0.0	0,0,0
18	0.02	0.05	0.0	76,76,0	0.0	0.0	0.0	0,0,0
19	0.02	0.05	0.0	76,76,0	0.0	0.0	0.0	0,0,0
20	0.02	0.04	0.0	76,76,0	0.0	0.0	0.0	0,0,0
21	0.01	0.05	0.0	76,76,0	0.0	0.0	0.0	0,0,0
22	0.02	0.03	0.0	76,76,0	0.0	0.0	0.0	0,0,0
23	0.01	0.02	0.0	76,76,0	0.0	0.0	0.0	0,0,0
24	0.02	0.05	0.0	76,76,0	0.0	0.0	0.0	0,0,0
25	0.02	0.04	0.0	76,76,0	0.0	0.0	0.0	0,0,0
45	0.05	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
46	0.04	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
47	0.04	0.06	0.0	74,74,0	0.0	0.0	0.0	0,0,0
48	0.03	0.04	0.0	76,74,0	0.0	0.0	0.0	0,0,0
49	0.03	0.04	0.0	73,73,0	0.0	0.0	0.0	0,0,0
50	0.03	0.06	0.0	76,76,0	0.0	0.0	0.0	0,0,0
51	0.04	0.07	0.0	76,76,0	0.0	0.0	0.0	0,0,0
52	0.04	0.09	0.0	74,76,0	0.0	0.0	0.0	0,0,0
53	0.04	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
54	0.05	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
55	0.05	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
56	0.05	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
57	0.05	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
58	0.04	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
59	0.05	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
60	0.04	0.10	0.0	76,76,0	0.0	0.0	0.0	0,0,0
61	0.06	0.12	0.0	76,76,0	0.0	0.0	0.0	0,0,0
62	0.07	0.14	0.0	76,76,0	0.0	0.0	0.0	0,0,0
63	0.07	0.15	0.0	76,76,0	0.0	0.0	0.0	0,0,0
64	0.07	0.15	0.0	76,76,0	0.0	0.0	0.0	0,0,0
65	0.07	0.15	0.0	76,76,0	0.0	0.0	0.0	0,0,0
66	0.07	0.15	0.0	76,76,0	0.0	0.0	0.0	0,0,0
67	0.07	0.15	0.0	74,74,0	0.0	0.0	0.0	0,0,0
68	0.07	0.15	0.0	74,74,0	0.0	0.0	0.0	0,0,0
69	0.07	0.15	0.0	74,74,0	0.0	0.0	0.0	0,0,0
70	0.06	0.14	0.0	74,74,0	0.0	0.0	0.0	0,0,0
71	0.06	0.13	0.0	74,74,0	0.0	0.0	0.0	0,0,0
72	0.06	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0
73	0.05	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
74	0.05	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
75	0.10	0.26	0.0	76,76,0	0.0	0.0	0.0	0,0,0
76	0.09	0.23	0.0	76,76,0	0.0	0.0	0.0	0,0,0
77	0.10	0.22	0.0	76,76,0	0.0	0.0	0.0	0,0,0
78	0.10	0.23	0.0	76,74,0	0.0	0.0	0.0	0,0,0
79	0.10	0.23	0.0	76,74,0	0.0	0.0	0.0	0,0,0
80	0.10	0.23	0.0	74,74,0	0.0	0.0	0.0	0,0,0
81	0.09	0.22	0.0	74,74,0	0.0	0.0	0.0	0,0,0
82	0.09	0.21	0.0	74,74,0	0.0	0.0	0.0	0,0,0
83	0.08	0.19	0.0	74,74,0	0.0	0.0	0.0	0,0,0
84	0.08	0.18	0.0	74,74,0	0.0	0.0	0.0	0,0,0
85	0.07	0.16	0.0	74,74,0	0.0	0.0	0.0	0,0,0
86	0.06	0.13	0.0	74,74,0	0.0	0.0	0.0	0,0,0
87	0.06	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0
88	0.05	0.09	0.0	74,74,0	0.0	0.0	0.0	0,0,0
89	0.04	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
90	0.11	0.29	0.0	74,74,0	0.0	0.0	0.0	0,0,0
91	0.11	0.28	0.0	74,74,0	0.0	0.0	0.0	0,0,0
92	0.11	0.26	0.0	74,74,0	0.0	0.0	0.0	0,0,0
93	0.11	0.25	0.0	74,74,0	0.0	0.0	0.0	0,0,0
94	0.11	0.25	0.0	74,74,0	0.0	0.0	0.0	0,0,0
95	0.10	0.25	0.0	74,74,0	0.0	0.0	0.0	0,0,0
96	0.10	0.24	0.0	74,74,0	0.0	0.0	0.0	0,0,0
97	0.09	0.22	0.0	74,74,0	0.0	0.0	0.0	0,0,0
98	0.09	0.20	0.0	74,74,0	0.0	0.0	0.0	0,0,0
99	0.08	0.19	0.0	74,74,0	0.0	0.0	0.0	0,0,0
100	0.07	0.15	0.0	74,74,0	0.0	0.0	0.0	0,0,0
101	0.06	0.13	0.0	74,74,0	0.0	0.0	0.0	0,0,0
102	0.05	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
103	0.04	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
104	0.04	0.06	0.0	74,74,0	0.0	0.0	0.0	0,0,0
105	0.11	0.29	0.0	74,74,0	0.0	0.0	0.0	0,0,0
106	0.11	0.28	0.0	74,74,0	0.0	0.0	0.0	0,0,0
107	0.11	0.26	0.0	74,74,0	0.0	0.0	0.0	0,0,0
108	0.11	0.26	0.0	74,74,0	0.0	0.0	0.0	0,0,0
109	0.11	0.25	0.0	74,74,0	0.0	0.0	0.0	0,0,0
110	0.10	0.25	0.0	74,74,0	0.0	0.0	0.0	0,0,0
111	0.10	0.24	0.0	74,74,0	0.0	0.0	0.0	0,0,0
112	0.09	0.22	0.0	74,74,0	0.0	0.0	0.0	0,0,0
113	0.09	0.20	0.0	74,74,0	0.0	0.0	0.0	0,0,0
114	0.08	0.19	0.0	74,74,0	0.0	0.0	0.0	0,0,0

SCARICATORE IN VIA PUCCI

115	0.07	0.15	0.0	74,74,0	0.0	0.0	0.0	0,0,0
116	0.06	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0
117	0.05	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
118	0.04	0.07	0.0	74,74,0	0.0	0.0	0.0	0,0,0
119	0.03	0.05	0.0	74,74,0	0.0	0.0	0.0	0,0,0
120	0.10	0.25	0.0	74,74,0	0.0	0.0	0.0	0,0,0
121	0.10	0.24	0.0	74,74,0	0.0	0.0	0.0	0,0,0
122	0.10	0.23	0.0	74,74,0	0.0	0.0	0.0	0,0,0
123	0.10	0.23	0.0	74,74,0	0.0	0.0	0.0	0,0,0
124	0.10	0.23	0.0	74,74,0	0.0	0.0	0.0	0,0,0
125	0.10	0.23	0.0	74,74,0	0.0	0.0	0.0	0,0,0
126	0.09	0.22	0.0	74,74,0	0.0	0.0	0.0	0,0,0
127	0.09	0.20	0.0	74,74,0	0.0	0.0	0.0	0,0,0
128	0.08	0.18	0.0	74,74,0	0.0	0.0	0.0	0,0,0
129	0.08	0.17	0.0	74,74,0	0.0	0.0	0.0	0,0,0
130	0.06	0.14	0.0	74,74,0	0.0	0.0	0.0	0,0,0
131	0.06	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0
132	0.05	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
133	0.04	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
134	0.04	0.06	0.0	74,74,0	0.0	0.0	0.0	0,0,0
135	0.06	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0
136	0.06	0.13	0.0	74,74,0	0.0	0.0	0.0	0,0,0
137	0.07	0.15	0.0	74,74,0	0.0	0.0	0.0	0,0,0
138	0.07	0.16	0.0	74,74,0	0.0	0.0	0.0	0,0,0
139	0.07	0.16	0.0	74,74,0	0.0	0.0	0.0	0,0,0
140	0.07	0.16	0.0	74,74,0	0.0	0.0	0.0	0,0,0
141	0.07	0.16	0.0	74,74,0	0.0	0.0	0.0	0,0,0
142	0.07	0.15	0.0	74,74,0	0.0	0.0	0.0	0,0,0
143	0.07	0.15	0.0	74,74,0	0.0	0.0	0.0	0,0,0
144	0.07	0.14	0.0	74,74,0	0.0	0.0	0.0	0,0,0
145	0.06	0.13	0.0	74,74,0	0.0	0.0	0.0	0,0,0
146	0.05	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0
147	0.05	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
148	0.04	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
149	0.04	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
150	0.05	0.13	0.0	76,76,0	0.0	0.0	0.0	0,0,0
151	0.04	0.09	0.0	74,74,0	0.0	0.0	0.0	0,0,0
152	0.05	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
153	0.05	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
154	0.05	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
155	0.05	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
156	0.05	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
157	0.06	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
158	0.06	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
159	0.05	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0
160	0.05	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0
161	0.05	0.11	0.0	74,74,0	0.0	0.0	0.0	0,0,0
162	0.05	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
163	0.04	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
164	0.04	0.07	0.0	74,74,0	0.0	0.0	0.0	0,0,0
165	0.04	0.13	0.0	74,76,0	0.0	0.0	0.0	0,0,0
166	0.03	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
167	0.03	0.07	0.0	74,74,0	0.0	0.0	0.0	0,0,0
168	0.03	0.06	0.0	74,74,0	0.0	0.0	0.0	0,0,0
169	0.03	0.04	0.0	74,74,0	0.0	0.0	0.0	0,0,0
170	0.03	0.06	0.0	74,74,0	0.0	0.0	0.0	0,0,0
171	0.04	0.07	0.0	74,74,0	0.0	0.0	0.0	0,0,0
172	0.04	0.07	0.0	74,74,0	0.0	0.0	0.0	0,0,0
173	0.04	0.07	0.0	74,76,0	0.0	0.0	0.0	0,0,0
174	0.04	0.09	0.0	74,74,0	0.0	0.0	0.0	0,0,0
175	0.04	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
176	0.04	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
177	0.04	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
178	0.04	0.07	0.0	74,74,0	0.0	0.0	0.0	0,0,0
179	0.03	0.06	0.0	74,76,0	0.0	0.0	0.0	0,0,0
180	0.03	0.08	0.0	76,76,0	0.0	0.0	0.0	0,0,0
181	0.02	0.05	0.0	76,75,0	0.0	0.0	0.0	0,0,0
182	0.03	0.04	0.0	76,76,0	0.0	0.0	0.0	0,0,0
183	0.03	0.05	0.0	76,74,0	0.0	0.0	0.0	0,0,0
184	0.03	0.05	0.0	74,74,0	0.0	0.0	0.0	0,0,0
185	0.03	0.06	0.0	74,74,0	0.0	0.0	0.0	0,0,0
186	0.03	0.09	0.0	74,75,0	0.0	0.0	0.0	0,0,0
187	0.06	0.19	0.0	74,74,0	0.0	0.0	0.0	0,0,0
188	0.05	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
189	0.04	0.09	0.0	74,74,0	0.0	0.0	0.0	0,0,0
190	0.03	0.07	0.0	74,74,0	0.0	0.0	0.0	0,0,0
191	0.02	0.05	0.0	76,74,0	0.0	0.0	0.0	0,0,0
192	0.03	0.08	0.0	74,74,0	0.0	0.0	0.0	0,0,0
193	0.03	0.09	0.0	74,73,0	0.0	0.0	0.0	0,0,0

SCARICATORE IN VIA PUCCI

194	0.02	0.06	0.0	74,74,0	0.0	0.0	0.0	0,0,0
554	0.12	0.21	0.0	76,76,0	0.0	0.0	0.0	0,0,0
555	0.09	0.21	0.0	76,76,0	0.0	0.0	0.0	0,0,0
556	0.09	0.18	0.0	76,76,0	0.0	0.0	0.0	0,0,0
557	0.11	0.19	0.0	76,76,0	0.0	0.0	0.0	0,0,0
558	0.12	0.21	0.0	76,76,0	0.0	0.0	0.0	0,0,0
559	0.13	0.22	0.0	76,76,0	0.0	0.0	0.0	0,0,0
560	0.13	0.22	0.0	76,76,0	0.0	0.0	0.0	0,0,0
561	0.13	0.22	0.0	76,76,0	0.0	0.0	0.0	0,0,0
562	0.13	0.22	0.0	76,76,0	0.0	0.0	0.0	0,0,0
563	0.12	0.21	0.0	76,76,0	0.0	0.0	0.0	0,0,0
564	0.10	0.18	0.0	76,76,0	0.0	0.0	0.0	0,0,0
565	0.09	0.16	0.0	76,76,0	0.0	0.0	0.0	0,0,0
566	0.08	0.15	0.0	74,76,0	0.0	0.0	0.0	0,0,0
567	0.08	0.15	0.0	74,76,0	0.0	0.0	0.0	0,0,0
568	0.09	0.17	0.0	76,76,0	0.0	0.0	0.0	0,0,0
569	0.09	0.19	0.0	76,76,0	0.0	0.0	0.0	0,0,0
570	0.13	0.22	0.0	76,76,0	0.0	0.0	0.0	0,0,0
571	0.10	0.18	0.0	76,76,0	0.0	0.0	0.0	0,0,0
572	0.07	0.23	0.0	76,76,0	0.0	0.0	0.0	0,0,0
573	0.09	0.23	0.0	74,76,0	0.0	0.0	0.0	0,0,0
574	0.10	0.18	0.0	74,76,0	0.0	0.0	0.0	0,0,0
575	0.10	0.19	0.0	74,76,0	0.0	0.0	0.0	0,0,0
576	0.10	0.18	0.0	74,76,0	0.0	0.0	0.0	0,0,0
577	0.09	0.16	0.0	74,76,0	0.0	0.0	0.0	0,0,0
578	0.08	0.13	0.0	74,74,0	0.0	0.0	0.0	0,0,0
579	0.08	0.14	0.0	74,74,0	0.0	0.0	0.0	0,0,0
580	0.09	0.15	0.0	74,74,0	0.0	0.0	0.0	0,0,0
581	0.10	0.16	0.0	74,74,0	0.0	0.0	0.0	0,0,0
582	0.10	0.17	0.0	74,74,0	0.0	0.0	0.0	0,0,0
583	0.10	0.17	0.0	74,74,0	0.0	0.0	0.0	0,0,0
584	0.10	0.17	0.0	74,74,0	0.0	0.0	0.0	0,0,0
585	0.10	0.17	0.0	74,74,0	0.0	0.0	0.0	0,0,0
586	0.10	0.16	0.0	76,74,0	0.0	0.0	0.0	0,0,0
587	0.09	0.14	0.0	76,74,0	0.0	0.0	0.0	0,0,0
588	0.09	0.15	0.0	76,76,0	0.0	0.0	0.0	0,0,0
589	0.05	0.20	0.0	76,76,0	0.0	0.0	0.0	0,0,0
590	0.08	0.16	0.0	74,76,0	0.0	0.0	0.0	0,0,0
591	0.12	0.20	0.0	74,74,0	0.0	0.0	0.0	0,0,0
592	0.13	0.23	0.0	74,74,0	0.0	0.0	0.0	0,0,0
593	0.14	0.25	0.0	74,74,0	0.0	0.0	0.0	0,0,0
594	0.15	0.26	0.0	74,74,0	0.0	0.0	0.0	0,0,0
595	0.14	0.26	0.0	74,74,0	0.0	0.0	0.0	0,0,0
596	0.14	0.26	0.0	74,74,0	0.0	0.0	0.0	0,0,0
597	0.14	0.26	0.0	74,74,0	0.0	0.0	0.0	0,0,0
598	0.14	0.25	0.0	74,74,0	0.0	0.0	0.0	0,0,0
599	0.14	0.25	0.0	74,74,0	0.0	0.0	0.0	0,0,0
600	0.13	0.24	0.0	74,74,0	0.0	0.0	0.0	0,0,0
601	0.13	0.22	0.0	76,74,0	0.0	0.0	0.0	0,0,0
602	0.11	0.19	0.0	76,74,0	0.0	0.0	0.0	0,0,0
603	0.10	0.17	0.0	76,74,0	0.0	0.0	0.0	0,0,0
604	0.09	0.14	0.0	76,74,0	0.0	0.0	0.0	0,0,0
605	0.09	0.15	0.0	74,74,0	0.0	0.0	0.0	0,0,0
606	0.07	0.09	0.0	74,76,0	0.0	0.0	0.0	0,0,0
607	0.10	0.14	0.0	74,74,0	0.0	0.0	0.0	0,0,0
608	0.13	0.23	0.0	74,74,0	0.0	0.0	0.0	0,0,0
609	0.15	0.27	0.0	74,74,0	0.0	0.0	0.0	0,0,0
610	0.17	0.31	0.0	74,74,0	0.0	0.0	0.0	0,0,0
611	0.18	0.33	0.0	74,74,0	0.0	0.0	0.0	0,0,0
612	0.18	0.33	0.0	74,74,0	0.0	0.0	0.0	0,0,0
613	0.17	0.31	0.0	74,74,0	0.0	0.0	0.0	0,0,0
614	0.16	0.30	0.0	74,74,0	0.0	0.0	0.0	0,0,0
615	0.15	0.28	0.0	74,74,0	0.0	0.0	0.0	0,0,0
616	0.15	0.27	0.0	76,74,0	0.0	0.0	0.0	0,0,0
617	0.14	0.25	0.0	76,74,0	0.0	0.0	0.0	0,0,0
618	0.13	0.23	0.0	76,74,0	0.0	0.0	0.0	0,0,0
619	0.11	0.19	0.0	76,74,0	0.0	0.0	0.0	0,0,0
620	0.10	0.17	0.0	76,74,0	0.0	0.0	0.0	0,0,0
621	0.08	0.13	0.0	76,74,0	0.0	0.0	0.0	0,0,0
622	0.10	0.17	0.0	74,74,0	0.0	0.0	0.0	0,0,0
623	0.07	0.04	0.0	74,74,0	0.0	0.0	0.0	0,0,0
624	0.10	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0
625	0.13	0.23	0.0	76,74,0	0.0	0.0	0.0	0,0,0
626	0.17	0.30	0.0	76,74,0	0.0	0.0	0.0	0,0,0
627	0.19	0.34	0.0	76,76,0	0.0	0.0	0.0	0,0,0
628	0.19	0.35	0.0	74,76,0	0.0	0.0	0.0	0,0,0
629	0.19	0.35	0.0	74,76,0	0.0	0.0	0.0	0,0,0
630	0.18	0.33	0.0	74,76,0	0.0	0.0	0.0	0,0,0
631	0.16	0.30	0.0	74,74,0	0.0	0.0	0.0	0,0,0

SCARICATORE IN VIA PUCCI

632	0.16	0.29	0.0	74,74,0	0.0	0.0	0.0	0,0,0
633	0.15	0.27	0.0	76,74,0	0.0	0.0	0.0	0,0,0
634	0.14	0.25	0.0	76,74,0	0.0	0.0	0.0	0,0,0
635	0.13	0.22	0.0	76,74,0	0.0	0.0	0.0	0,0,0
636	0.11	0.18	0.0	76,74,0	0.0	0.0	0.0	0,0,0
637	0.09	0.15	0.0	76,74,0	0.0	0.0	0.0	0,0,0
638	0.07	0.10	0.0	74,74,0	0.0	0.0	0.0	0,0,0
639	0.10	0.17	0.0	74,74,0	0.0	0.0	0.0	0,0,0
640	0.09	0.17	0.0	76,74,0	0.0	0.0	0.0	0,0,0
641	0.09	0.19	0.0	74,74,0	0.0	0.0	0.0	0,0,0
642	0.24	0.44	0.0	76,74,0	0.0	0.0	0.0	0,0,0
643	0.22	0.39	0.0	76,74,0	0.0	0.0	0.0	0,0,0
644	0.19	0.34	0.0	76,76,0	0.0	0.0	0.0	0,0,0
645	0.19	0.36	0.0	74,76,0	0.0	0.0	0.0	0,0,0
646	0.26	0.47	0.0	74,76,0	0.0	0.0	0.0	0,0,0
647	0.34	0.65	0.0	74,76,0	0.15	0.0	0.0	76,0,0
648	0.19	0.35	0.0	74,76,0	0.0	0.0	0.0	0,0,0
649	0.15	0.29	0.0	74,74,0	0.0	0.0	0.0	0,0,0
650	0.17	0.31	0.0	76,74,0	0.0	0.0	0.0	0,0,0
651	0.17	0.30	0.0	76,74,0	0.0	0.0	0.0	0,0,0
652	0.13	0.23	0.0	76,74,0	0.0	0.0	0.0	0,0,0
653	0.11	0.19	0.0	74,74,0	0.0	0.0	0.0	0,0,0
654	0.10	0.16	0.0	74,74,0	0.0	0.0	0.0	0,0,0
655	0.08	0.12	0.0	74,74,0	0.0	0.0	0.0	0,0,0
656	0.10	0.17	0.0	74,74,0	0.0	0.0	0.0	0,0,0
657	0.10	0.27	0.0	76,74,0	0.0	0.0	0.0	0,0,0
660	0.35	0.63	0.0	76,74,0	0.15	0.0	0.0	74,0,0
661	0.19	0.33	0.0	76,76,0	0.0	0.0	0.0	0,0,0
662	0.19	0.34	0.0	76,76,0	0.0	0.0	0.0	0,0,0
663	0.35	0.66	0.0	74,76,0	0.15	0.0	0.0	76,0,0
668	0.25	0.46	0.0	76,74,0	0.0	0.0	0.0	0,0,0
669	0.14	0.25	0.0	76,74,0	0.0	0.0	0.0	0,0,0
670	0.11	0.19	0.0	74,74,0	0.0	0.0	0.0	0,0,0
671	0.10	0.17	0.0	74,74,0	0.0	0.0	0.0	0,0,0
672	0.08	0.13	0.0	74,74,0	0.0	0.0	0.0	0,0,0
673	0.09	0.14	0.0	74,74,0	0.0	0.0	0.0	0,0,0
674	0.04	0.29	0.0	74,74,0	0.0	0.0	0.0	0,0,0
677	0.14	0.22	0.0	76,74,0	0.0	0.0	0.0	0,0,0
678	0.13	0.21	0.0	76,74,0	0.0	0.0	0.0	0,0,0
679	0.13	0.22	0.0	76,76,0	0.0	0.0	0.0	0,0,0
680	0.16	0.26	0.0	76,76,0	0.0	0.0	0.0	0,0,0
685	0.13	0.22	0.0	74,74,0	0.0	0.0	0.0	0,0,0
686	0.12	0.20	0.0	74,74,0	0.0	0.0	0.0	0,0,0
687	0.10	0.17	0.0	74,74,0	0.0	0.0	0.0	0,0,0
688	0.09	0.15	0.0	74,74,0	0.0	0.0	0.0	0,0,0
689	0.08	0.13	0.0	74,74,0	0.0	0.0	0.0	0,0,0
690	0.09	0.16	0.0	74,74,0	0.0	0.0	0.0	0,0,0
692	0.03	0.25	0.0	74,74,0	0.0	0.0	0.0	0,0,0
695	0.20	0.34	0.0	74,74,0	0.0	0.0	0.0	0,0,0
696	0.09	0.13	0.0	74,74,0	0.0	0.0	0.0	0,0,0
697	0.10	0.16	0.0	74,74,0	0.0	0.0	0.0	0,0,0
698	0.23	0.38	0.0	74,74,0	0.0	0.0	0.0	0,0,0
702	0.22	0.40	0.0	74,74,0	0.0	0.0	0.0	0,0,0
703	0.15	0.29	0.0	74,74,0	0.0	0.0	0.0	0,0,0
704	0.14	0.27	0.0	74,74,0	0.0	0.0	0.0	0,0,0
705	0.13	0.23	0.0	74,74,0	0.0	0.0	0.0	0,0,0
706	0.08	0.14	0.0	74,74,0	0.0	0.0	0.0	0,0,0
707	0.09	0.16	0.0	74,74,0	0.0	0.0	0.0	0,0,0
710	0.01	0.07	0.0	76,74,0	0.0	0.0	0.0	0,0,0
711	0.28	0.50	0.0	74,74,0	0.0	0.0	0.0	0,0,0
712	0.03	0.04	0.0	74,74,0	0.0	0.0	0.0	0,0,0
713	0.10	0.17	0.0	74,74,0	0.0	0.0	0.0	0,0,0
714	0.16	0.29	0.0	74,74,0	0.0	0.0	0.0	0,0,0
715	0.13	0.23	0.0	74,74,0	0.0	0.0	0.0	0,0,0
716	0.15	0.26	0.0	74,74,0	0.0	0.0	0.0	0,0,0
717	0.18	0.29	0.0	74,74,0	0.0	0.0	0.0	0,0,0
718	0.16	0.29	0.0	74,76,0	0.0	0.0	0.0	0,0,0
719	0.14	0.38	0.0	76,74,0	0.0	0.0	0.0	0,0,0
720	0.09	0.24	0.0	74,74,0	0.0	0.0	0.0	0,0,0
721	0.17	0.29	0.0	74,74,0	0.0	0.0	0.0	0,0,0
722	0.19	0.35	0.0	74,74,0	0.0	0.0	0.0	0,0,0
723	0.19	0.37	0.0	74,74,0	0.0	0.0	0.0	0,0,0
724	0.20	0.38	0.0	74,74,0	0.0	0.0	0.0	0,0,0
725	0.19	0.37	0.0	74,74,0	0.0	0.0	0.0	0,0,0
726	0.08	0.13	0.0	74,76,0	0.0	0.0	0.0	0,0,0
727	0.08	0.15	0.0	76,76,0	0.0	0.0	0.0	0,0,0
728	0.12	0.36	0.0	74,74,0	0.0	0.0	0.0	0,0,0
729	0.10	0.20	0.0	74,74,0	0.0	0.0	0.0	0,0,0
730	0.08	0.17	0.0	74,74,0	0.0	0.0	0.0	0,0,0

REALIZZAZIONE DI OPERE A COMPLETAMENTO DELLA RETE FOGNARIA NEL COMUNE DI NOCERA INFERIORE – 1° LOTTO

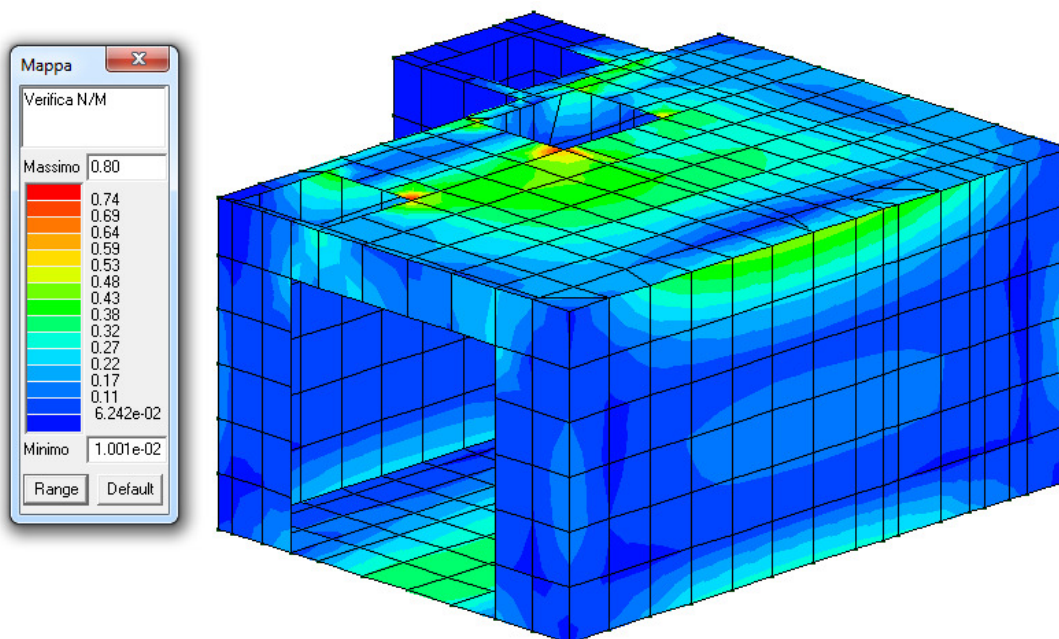
SCARICATORE IN VIA PUCCI

731	0.14	0.30	0.0	74,74,0	0.0	0.0	0.0	0,0,0
732	0.15	0.30	0.0	74,74,0	0.0	0.0	0.0	0,0,0
733	0.14	0.28	0.0	74,74,0	0.0	0.0	0.0	0,0,0
735	0.12	0.28	0.0	74,74,0	0.0	0.0	0.0	0,0,0
738	0.19	0.39	0.0	74,74,0	0.0	0.0	0.0	0,0,0
739	0.11	0.22	0.0	74,74,0	0.0	0.0	0.0	0,0,0
740	0.01	0.06	0.0	74,74,0	0.0	0.0	0.0	0,0,0
743	0.03	0.05	0.0	74,74,0	0.0	0.0	0.0	0,0,0
744	0.01	0.02	0.0	74,74,0	0.0	0.0	0.0	0,0,0
745	0.01	0.02	0.0	74,74,0	0.0	0.0	0.0	0,0,0
746	0.02	0.04	0.0	74,76,0	0.0	0.0	0.0	0,0,0
747	0.01	0.03	0.0	76,75,0	0.0	0.0	0.0	0,0,0
748	0.02	0.02	0.0	74,75,0	0.0	0.0	0.0	0,0,0
749	0.01	0.02	0.0	74,75,0	0.0	0.0	0.0	0,0,0
Guscio	rRfck	rRfyk	rPfck		wR	wF	wP	
	0.35	0.66	0.0		0.15	0.0	0.0	

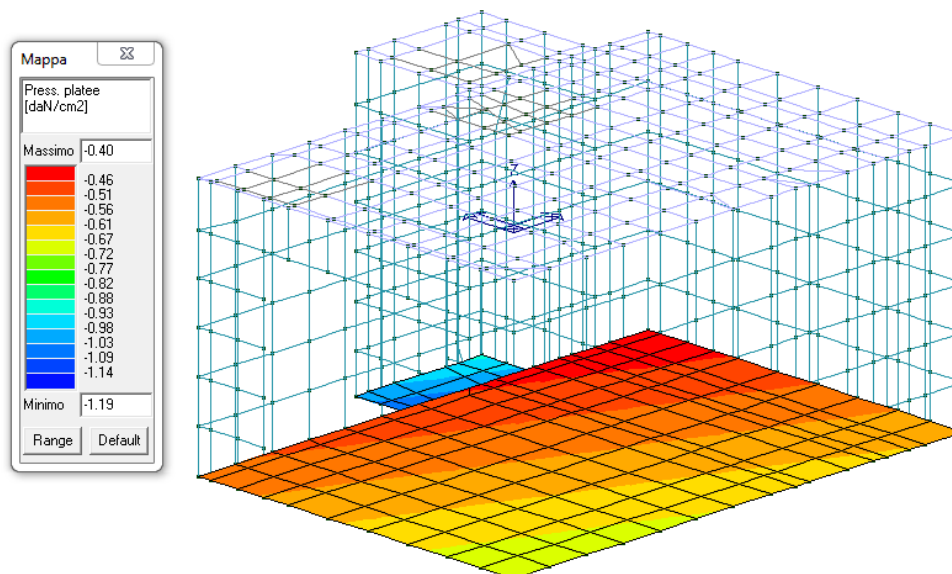
SINTESI GRAFICA DEI RISULTATI OTTENUTI

Azioni su elementi D3

- Verifica N/M



- Pressioni allo SLU - Platea



Il Progettista strutturale